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# Round-Robin Study of Methods for Trace Metal Analysis

Graphite Furnace Atomic Absorption Spectroscopy-  
Cadmium, Arsenic, and Chromium

**TR-108989**

Final Report, November 1997

Prepared by  
TRW INC.  
Space & Technology Division  
Redondo Beach, CA

Project Manager  
J.W. Scott

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Authors  
R.F. Maddalone  
J.W. Scott  
N.T. Whiddon

Prepared for  
**Electric Power Research Institute**  
3412 Hillview Avenue  
Palo Alto, California 94304

EPRI Project Manager  
B. Nott  
Generation Group

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# REPORT SUMMARY

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Eighteen utility laboratories evaluated graphite furnace atomic absorption spectroscopy (GFAAS) methods for measuring cadmium, arsenic, and chromium in a variety of utility aqueous streams. This EPRI Tailored Collaboration Project, part of the ongoing Analytical Methods Qualification (AMQ) program, will help utilities define reasonable pollutant discharge limits and effluent monitoring requirements.

## BACKGROUND

Federal and state permits are requiring electric utilities to monitor power plant effluents for increasingly low concentrations of trace metals, in some cases at levels that preclude reliable measurement. A central source of verified data on the standard deviation, recovery, and quantification levels for various methods would help utilities define reasonable effluent guidelines and monitoring requirements. It would also aid in the selection of appropriate analytical methods. EPRI sponsored this work to evaluate EPA GFAAS methods 213.2 (cadmium), 206.2 (arsenic), and 218.2 (chromium).

## OBJECTIVE

To verify the standard deviation, recovery, and Alternative Minimum Level (AML) for measurement of specific trace metals in typical utility aqueous samples.

## APPROACH

Investigators developed a test program based on ASTM D2777-96 protocols. At utility test sites, they collected several types of water samples (Midwest groundwater, acid mine drainage, and estuarine), they then injected cadmium, arsenic, and chromium into them. Eighteen utility laboratories conducted round-robin tests on these samples using EPA analytical methods. Based on the test results, the investigators developed single-operator (one laboratory) and multiple-operator (overall) standard deviation data for each element and sample matrix combination. They derived estimates of the Interlaboratory Critical Level ( $L_{CL}$ ), Interlaboratory Detection Level ( $L_{DL}$ ) and AML for each element in each matrix. They compared these values with concentrations specified by EPA and with federal Water Quality Criteria (WQC).

## **RESULTS**

The  $L_{CI}$ ,  $L_{DI}$  and AML were calculated for each trace element in each water type. Only three of the 12 element/matrix combinations had AMLs lower than the lowest freshwater EPA WQC: arsenic in reagent grade water, groundwater, and estuarine. No cases were found in which the Interlaboratory Detection Level ( $L_{DI}$ ) or the AML was lower than the EPA Detection Limit (DL) quoted in the analytical method.

## **EPRI PERSPECTIVE**

This report is the fifth (AMQ-IV, Round 2) in a series of comprehensive, round-robin evaluations to verify methods for chemical analysis. EPRI report CS-5910, Volumes 1- 3, and TR-105910 contain details of four similar round-robin studies of atomic absorption methods for 18 elements. EPRI report TR-106220 discussed in detail the development of the Alternative Minimum Level, presented AML values calculated from the data collected in all of the previous AMQ round-robin studies, and included a program on diskette to calculate AMLs. EPRI, in conjunction with the Utility Water Act Group, continues to work with the Inter-Industry Analytical Group (IIAG), a broad coalition of industry groups, ASTM, and EPA to achieve consensus on detection and quantification limits appropriate for NPDES permit compliance monitoring.

## **TR-108989**

### **Interest Categories**

Waste & Water Management  
Environmental Compliance Planning

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Chemical Analysis  
Measurement/Accuracy  
Trace Metals  
Compliance Monitoring  
Detection/Orientation

## ABSTRACT

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The objective of the Analytical Methods Qualification (AMQ) phase of the RP1851 project is to develop validated standard deviation and bias statements of analytical methods for selected elements in utility matrices. During AMQ-IV, Round 2, three elements (cadmium, arsenic and chromium) were validated in four matrices (reagent grade water, midwest groundwater, acid mine drainage, and estuarine water). The graphite furnace methods validated were Method 213.2 (cadmium), Method 206.2 (arsenic) and Method 218.2 (chromium) from the Metals - Atomic Absorption Methods in EPA 600/4-79-020 Methods for Chemical Analysis of Water and Wastes (March 1983 Revision). Eighteen laboratories completed the study.

Statements of standard deviation and bias for each element and matrix were produced using STATCALC, a statistical analysis program developed by EPRI based on ASTM D2777. The standard deviation data were used to calculate the Interlaboratory Critical Level ( $L_{CI}$ ), Interlaboratory Detection Level ( $L_{DI}$ ) and Alternative Minimum Level (AML) for each element by matrix. The Interlaboratory Critical Level is the lowest concentration that is distinct from zero to a specific level of confidence. The Interlaboratory Detection Level is the concentration at which a given analytical procedure may be relied upon to lead to detection. The Alternative Minimum Level, which is an estimate of quantification, is a factor of 10 times the interlaboratory standard deviation at the  $L_{CI}$  corrected to true concentration units with the appropriate prediction interval. In comparing the AMLs calculated from this study with the lowest EPA water quality criteria (WQC) listed for freshwater, the AMLs were higher in 9 of the 12 cases.



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### EPRI RESEARCH PROJECT RP1851 PROJECT ADVISORY COMMITTEE

Angie Grooms  
Duke Power Company

Sam Pellerite  
Pennsylvania Power & Light Company

Donna Hill  
Southern Company Services, Inc.

James K. Rice  
Consultant

Lyman Howe  
Tennessee Valley Authority

Dan Salvito  
Public Service Electric & Gas Company

John Moffet  
Kentucky Utilities Company

James F. Stine  
Baltimore Gas & Electric

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# 1

## INTRODUCTION

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### 1.1 Background And Objectives Of The Analytical Methods Qualification Project

#### 1.1.1 *Regulatory Environment*

The utility industry is required under the Clean Water Act (Federal Water Pollution Control Act) as amended to monitor their discharges for numerous chemical substances. The discharge limits vary with each pollutant. Where limits are set below levels at which quantification is possible, compliance in many states is gauged exclusively on the basis of monitoring results at or above the quantification level. An exception applies to limits expressed in terms of "no detectable discharge," where the detection limit often is used to gauge compliance. Concerns have arisen within the industry because the detection limits published in the USEPA MCAW (Methods for Chemical Analysis of Water and Wastes, EPA 600/4-79-020, Revised March 1983) are based on signal-to-noise ratios rather than detection limits that take into account all sources of interferences that are present when the test method is used in practice. If compliance standards, such as NPDES permit limitations, are set at levels at which it is not possible to make reliable measurements, permittees may be subjected to harsh civil and criminal enforcement consequences entirely as a result of analytical variability, as opposed to an unacceptable concentration of pollutants in their effluents. That is because compliance is gauged solely on the basis of the analytical results of a permittee's effluent, not on the pollution control measures employed. Unless appropriate detection and quantification levels are developed and applied, permittees may experience compliance problems, notwithstanding their best efforts to select and apply effective pollution control measures.

#### 1.1.2 *AMQ Design and Objectives*

EPRI Project RP1851, "Utility Aqueous Discharge Monitoring - Analytical Methods Qualification," (AMQ) was initiated in 1981 to improve the industry's ability to monitor plant wastewater streams. The project was divided into two phases - a literature review and a series of field studies. The goal of the first phase was to identify pollutants of concern to the electric utility industry and to document state-of-the-art analytical methods used to monitor the pollutants. Of special interest were regulated pollutants for which little analytical data had been collected. The literature study revealed that the EPA analytical method validation data were often obtained for matrices and

concentrations not representative of the steam electric industry. These findings prompted a field study program to validate the analytical methods used for discharge monitoring.

The primary objective of the AMQ project is to collect precision (standard deviation) and bias (observed value minus true value) data for methods used to determine selected parameters and elements in utility discharge streams. The field study was comprised of round-robin collaborative testing using representative utility laboratories and actual utility discharge streams. A round-robin study consists of distributing identical whole volume samples to individual laboratories for analysis according to a specified method. The analytical methods validated were from the USEPA MCAW (Methods for Chemical Analysis of Water and Wastes, EPA 600/4-79-020, Revised March 1983), which are approved by EPA for compliance testing under 40 CFR Part 136. The studies followed the experimental design recommended by the American Society for Testing and Materials' "Standard Practice for Determination of Precision and Bias of Applicable Methods of Committee D-19 on Water," D2777, for interlaboratory round-robin studies.

Table 1-1 provides an overview of the entire AMQ project, which was divided into four parts in order to facilitate participation by industry laboratories and to permit modification of the test design to reflect changing environmental issues or regulatory requirements. The elements and parameters in each part were selected on the basis of their importance to the utility industry and regulatory interest. All work up through AMQ-IV Round 1 was funded under Research Project RP1851. The current project, a Tailored Collaboration effort, was funded under Work Order WO3569-01.

### **1.1.3 Use of Validation Data**

One of the primary objectives of the AMQ project is to establish estimates of detection and quantification for use in compliance monitoring. A number of definitions of detection and quantification limits/levels have been published over the years, and the definitions have continued to evolve. The pioneering work of Currie (1) forms the basis of most, if not all, of the various approaches. For the reports published for AMQ-I, -II, -III and -IV, AMQ researchers evaluated the various definitions available and selected ones that had a strong technical justification and that incorporated the use of interlaboratory data. A discussion of the various definitions examined, the rationale for selection of the ones used and the values calculated using the definitions can be found in the EPRI reports cited in Table 1-1.

During the summer of 1995, EPRI along with the Inter-Industry Analytical Group (IIAG), an industry coalition, conducted an extensive review of available detection and quantification level definitions (2). This evaluation produced two major outputs:

- A list of properties and performance standards to evaluate detection and quantification level definitions, and

- A consensus agreement on an Alternative Minimum Level (AML) to estimate a method's quantification level.

EPRI worked within the industry coalition to develop a definition called the Alternative Minimum Level (AML). The AML, which is an estimate of the quantification level, is defined as 10 times the interlaboratory standard deviation at the lowest concentration that is differentiable from zero, the Interlaboratory Critical Level ( $L_{CI}$ ). The Interlaboratory Detection Level ( $L_{DI}$ ) is defined as the point at which a given analytical procedure may be relied upon to lead to a detection. The development of these definitions, and the computational approach for the  $L_{CI}$ ,  $L_{DI}$  and the AML are discussed in Section 8. The standard deviation data obtained by this study were used to calculate for each element by matrix the values for  $L_{CI}$ ,  $L_{DI}$  and AML that are found in Section 9. These values provide a realistic estimate of the capabilities of EPA-approved analytical methods in the compliance monitoring situation in utility aqueous matrices tested.

**Table 1-1**  
**Utility Aqueous Discharge Monitoring - Analytical Methods Qualification**  
**(AMQ) Program Overview**

Project Title	Part	Round	Parameters	Method	EPRI Report
Sampling and Analysis of Utility Pollutants	*		---	---	CS-3741
Analytical Methods Qualification	I	1	As, Se	GFAAS**	CS-5910
		2	Cr, Cu, Ni, Pb	GFAAS	Vol. 1
Analytical Methods Qualification	II		Hg	CVAAS	CS-5910
			Fe, Zn	Flame AAS	Vol. 2
			Cd	GFAAS	
Analytical Methods Qualification	III		Al, Ba, Be, B, Cd, Cr, Cu, Fe, Pb, Mn, Mo, Ni, V, Zn	ICP-AES	CS-5910
					Vol. 3
Analytical Methods Qualification	IV	1	Al, Be, Tl	GFAAS	TR-105910
		2***	Cd, As, Cr	GFAAS	<b>This Report</b>

\* Initial effort under EPRI Project RP1851 which involved collection and analysis of data on discharge rates and data on the analytical precision and bias for utility discharge species.

\*\* Several seawater laboratories determined As and Se by GHAAS.

\*\*\* Tailored Collaboration effort funded under WO3569-01.

GFAAS = Graphite Furnace Atomic Absorption Spectroscopy

GHAAS = Gaseous Hydride AAS

CVAAS = Cold Vapor AAS

ICP-AES = Inductively Coupled Plasma - Atomic Emission Spectroscopy



## 1.2 Overview of AMQ-IV Round 2

The AMQ project is based on the premise that a method qualification project should use matrices representative of those encountered by the analyst in routine work. Furthermore, since the shipment and storage of samples is part of the normal analysis procedure at most laboratories and comparison of the results from different laboratories on split samples is often encountered in compliance monitoring, the test program should include spiking the matrices and sending aliquots to each participant.

The AMQ test matrices were selected to be of interest to the utility industry. Descriptions of the matrices selected and the reasons for selecting those matrices are found in Section 2. The elements selected for validation in AMQ-IV Round 2 were cadmium, arsenic and chromium. The EPA Graphite Furnace Atomic Absorption Spectroscopy methods for each element were selected for validation.

## 1.3 Objectives Of This Report

The objective of this report is to provide the utility personnel with validated standard deviation and bias data for cadmium, arsenic and chromium by the EPA-approved GFAAS methods for cadmium (213.2), arsenic (206.2) and chromium (218.2) contained in the USEPA MCAW. In addition, we have provided estimates of the method's Interlaboratory Critical Level ( $L_{CL}$ ) and Alternative Minimum Level (AML) for each element in each matrix based on the data collected.

## 1.4 Use Of This Report

When an analyst produces a result that falls below the Alternative Minimum Level (AML), the EPRI quantification level definition, the result needs to be evaluated carefully in terms of its use. It is important that the use of such data in a regulatory setting be coupled with a thorough understanding of the analytical variability associated with the data. The intent of this report is to provide utilities with detection and quantification levels based on measurements made in qualified laboratories using utility matrices. The  $L_{CL}$ s,  $L_{DL}$ s and AMLs derived from this interlaboratory data provide a framework for evaluating data to be used in permit negotiation and compliance monitoring situations.

## 1.5 Organization of this Report

The methodology used in selecting parameters for testing is discussed in Section 2. Section 3 describes the solicitation process used to enlist the volunteer laboratories. Also included in this section is a list of the participants. The sample collection, spiking, and disbursement procedures are described in Section 4, along with the laboratory

reporting requirements. Section 5 summarizes the quality assurance approach and the results of analyses performed to verify sample integrity. In Section 6, a discussion of the statistical methods applied to the data is presented. The complete data evaluation process is described in Section 7, and in Section 8 the development of detection and quantification definitions for compliance monitoring are discussed. Section 9 contains the Alternative Minimum Levels calculated from the AMQ-IV Round 2 data. The report's conclusions are given in Section 10. The appendices contain the instructions given to the laboratories, operating data reported by the laboratories and the analytical results summarized by element in tabular form.

## 1.6 References

1. Currie, L.A (1968). Limits for Qualitative Detection and Quantitative Determination: Application to Radiochemistry. Analytical Chemistry, 40, 586-593.
2. Koorse, S. J., "Industry Presentation for EPA's Meeting on the Draft 'National Guidance for the Permitting, Monitoring, and Enforcement of Water Quality-based Effluent Limitations Set Below Analytical Detection/Quantitation Levels'", submitted to the EPA on June 21, 1995 on behalf of a coalition of American Industries by law firm of Hunton & Williams.

# 2

## SELECTION OF PARAMETERS FOR VALIDATION TESTING

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The methodology used in selecting elements, methods, test concentrations and matrices is discussed in the following sections.

### 2.1 Selection of Elements

For the AMQ project, only metals were considered since data gathered for the Sampling and Analysis of Utility Pollutants (EPRI Report CS-3741) project showed that organics are rarely found in steam electric power plant discharges. As indicated in Table 1-1, a number of metals were investigated in earlier AMQ studies. For the most part, the elements selected were included for regulatory interest, direct importance as a discharged pollutant, potential importance in the groundwater monitoring programs and lack of previous AMQ validation.

A survey was conducted among members of the RP1851 Project Advisory Committee to solicit information on the elements and matrices of interest to electric utilities. Table 2-1 summarizes the level of interest of various metals, listed in order from highest interest to lowest. Based on discussion with the Project Advisory Committee, cadmium, arsenic and chromium were selected for validation by GFAAS in this round.

**Table 2-1**  
**Survey Results -Level of Interest in Elements**

<b>Element</b>	<b>Level of Interest</b>
Hg	High
Cd	High
As	High
Se	High
Pb	High

**Table 2-1**  
**Survey Results -Level of Interest in Elements**

<b>Element</b>	<b>Level of Interest</b>
Ag	Medium
Ni	Medium
Mn	Medium
Cr <sup>+3</sup>	Medium
Ba	Medium
Sb	Medium
Cr <sup>+6</sup>	Medium
Mg	Medium
B	Low
V	Low
Cu	Low

## **2.2 Selection of Test Methods and Procedures**

The GFAAS methods selected for validation in AMQ-IV Round 2 were Method 213.2 (cadmium), Method 206.2 (arsenic) and Method 218.2 (chromium) for "Atomic Absorption, Furnace Technique" from the Metals - Atomic Absorption Methods in EPA 600/4-79-020 Methods for Chemical Analysis of Water and Wastes (March 1983 revision). The digestion procedure listed in Method 206.2 specifies that hydrogen peroxide and nitric acid be used in the digestion of samples for arsenic analysis. The cadmium and chromium methods require only nitric acid. Using two different digestion procedures would significantly increase the participants' workload and the volume of sample that each laboratory would require. TRW conducted a digestion comparison to determine the necessity of digesting the samples with hydrogen peroxide for arsenic analysis. An aliquot of river water from a previous AMQ study was spiked with arsenic, cadmium and chromium and split. Duplicate samples were digested using only nitric acid and both nitric acid and hydrogen peroxide. Unspiked duplicate blanks were digested in the same manner. The digested samples were split and analyzed by Inductively Coupled Plasma - Mass Spectrometry. As Table 2-2 shows, no differences in recoveries were noted.

**Table 2-2**  
**Comparison of Recoveries for Nitric Acid Digestion and**  
**Hydrogen Peroxide Digestion for Arsenic, Cadmium and**  
**Chromium in Spiked River Water**

<b>Sample</b>	<b>Measured, Blank µg/L</b>	<b>Measured, Spiked µg/L</b>	<b>Added Spike, µg/L</b>	<b>Recovery</b>
As, HNO <sub>3</sub> Digestion	1.0	89.2	82.2	107%
As, H <sub>2</sub> O <sub>2</sub> /HNO <sub>3</sub> Digestion	1.1	88.9	82.2	107%
Cd, HNO <sub>3</sub> Digestion	0.1	7.4	6.8	107%
Cd, H <sub>2</sub> O <sub>2</sub> /HNO <sub>3</sub> Digestion	0.1	7.6	6.8	110%
Cr, HNO <sub>3</sub> Digestion	0.3	60.5	56.9	106%
Cr, H <sub>2</sub> O <sub>2</sub> /HNO <sub>3</sub> Digestion	0.2	59.9	56.9	105%

The participants were instructed to digest all samples according to Section 4.1.4 for "total recoverable metals." Hydrochloric acid is omitted for GFAAS analysis. A slight modification was made to the digestion procedure. Instead of filtering all samples at their reduced volume to remove precipitates as directed in the method, the analysts were instructed to redilute the samples back to their original volumes and filter only those that still contained precipitates. Some matrices have solids that may precipitate at the reduced volume but redissolve on dilution. This modification was noted in the instructions to the participants and also noted directly on the copy of the EPA Metals Method that was sent to each laboratory.

The AMQ-IV Round 2 study employed Youden paired samples (1) instead of replicate samples like those used in most of the previous AMQ studies. Results from replicate studies are sometimes considered suspect because of the potential for repeated analysis by analysts intent on obtaining results in close agreement. For this reason, the Youden pair study is preferred. A Youden pair consists of two closely matched samples of the same matrix with similar concentrations of the test element. Each sample is treated as a completely independent sample. This approach still allows for the calculation of intralaboratory precision statistics but removes the analyst's opportunity to bias the data.

## 2.3 Selection of Test Matrices

The AMQ-IV Round 2 matrices are shown in Table 2-3. Respondents to the survey discussed in Section 2.1 indicated a high level of interest in groundwater matrices. A low TDS groundwater from the midwest, acid mine drainage, and estuarine matrices were selected for this study. Reagent grade water matrix was selected to provide an estimate of the variability due to preparation and analysis when no significant interferences are present.

**Table 2-3**  
**Selected Test Matrices for AMQ-IV Round 2**

<b>Matrix</b>	<b>Reason for Selection</b>
Midwest Groundwater	Low TDS groundwater sample with few interferences
Acid Mine Drainage (groundwater)	Complex matrix which has significant analysis problems
Estuarine	Major water source for coastal plants; complex matrix
Reagent Grade Water	Baseline matrix for comparison of stability and matrix effects

Members of the RP-1851 Project Advisory Committee provided the groundwater and estuarine matrices. Since the salinity of the estuarine sample varies seasonally, the salinity of the estuarine site was monitored weekly during the spring until the chloride content was at a relatively high level before the sample was collected. Prior to the preparation of validation samples, TRW determined the background concentration of each test element by ICP-MS using standard addition techniques. These values are included in the test concentration summaries presented in Section 2.4. For further matrix characterization, the background elements were determined by ICP-MS and the anion concentrations were measured by ion chromatography. Total dissolved solids and conductivity were also measured. The results of those analyses are found in Section 4.3.

In order to obtain sufficient data for the study, the participating laboratories were asked to analyze as many of the matrices as possible. All of the participants analyzed the midwest groundwater and reagent grade water samples. Most of the laboratories analyzed the estuarine and acid mine drainage samples.

## 2.4 Selection of Test Concentrations

The selection of test concentrations addressed the needs to:

- Challenge the analytical method at or near its detection limit.
- Stay within the published (EPA MCAW) estimate of the optimum analytical range if possible.
- Maximize the number of different test concentrations over the analytical range of each element.
- Overlap the intake and discharge spike concentrations for the freshwater and seawater matrices.
- Provide for dilution of the more complex matrices

ASTM recommends a minimum of three test levels (2). The AMQ-IV Round 2 program used four pairs of spiked samples plus a pair of unspiked background samples for each matrix, resulting in a total of ten samples per matrix.

The EPA (49FR 43430 Friday, October 26, 1984) has recommended an approach to calculating the Method Detection Limit (MDL). The analyte of interest is spiked into the matrix to obtain a concentration within a factor of 1 to 5 times the estimated limit of detection (1 to 10 times for reagent grade water.) Table 2-4 contains the detection limits estimated by the EPA (MCAW, EPA 600/4-79-020, Revised March 1983), the optimum range suggested by the EPA (MCAW), the non-cooling water discharge values obtained in Phase I of this project, and the Water Quality Criteria for the AMQ-IV Round 2 elements. Based on the data in Table 2-4, the initial spike concentrations for the freshwater (midwest groundwater) and reagent grade water, were targeted to satisfy the EPA requirements for the calculation of the MDL. The eighth and final spike concentration was at the upper limit of the optimum use range when background levels permitted. The spikes for the estuarine and acid mine drainage samples were a factor of 10 higher to permit dilution of these high dissolved solids matrices.

Tables 2-5 through 2-8 contain the total targeted concentrations for the AMQ-IV Round 2 validation effort based on the analysis of the unspiked samples. Prior to the test, each matrix was analyzed at TRW by ICP-MS to determine the background concentrations of the test elements. The amount of each element to be added to each matrix was calculated to reach the targeted concentrations. It should be noted that the true concentrations reported in Section 7 and the Appendix are computed from the mean value reported by the participants for the lowest concentrations. Tables 2-5 through 2-8 represent only TRW's estimate of the background and show the planned spike concentrations.

TRW conducted a series of tests to assess the compatibility of the three spiking solutions with each other and with the test matrices. A solution containing volumes of 1000 ppm

single element ICP standards in the ration of 1:2:2 Cd:As:Cr was prepared and monitored. No evidence of precipitation was seen. Portions of this mixture were spiked into reagent grade water both immediately after preparation and 24 hours after preparation. The samples were then analyzed by ICP-MS. Recoveries were within ten percent of the spiked values. It was concluded that these standards could be combined in beakers for the short time necessary during the spiking activity without danger of precipitation of test elements.

**Table 2-4**  
**AMQ-IV Round 2 Background Information**

<b>Element</b>	<b>EPA GFAAS DL µg/L (1)</b>	<b>NCWD µg/L (2)</b>	<b>WQC µg/L (3)</b>	<b>EPA MCAW Optimum Range µg/L (1)</b>
As	1	41	190	5-100
Cd	0.1	4.6	1.0	0.5-10
Cr	1	19	10 (hex)	5-100

(1) From EPA MCAW, Methods for Chemical Analysis of Water and Wastes, EPA 600/4-29/040, Revised March 1983

(2) Non-Cooling Water Discharge average concentration in Aggregate Ashpond Overflow (Source: EPRI CS-3741, November 1984)

(3) Freshwater Criteria Continuous Concentration expressed as dissolved (60 FR 22236, May 4, 1995), 100 mg/L hardness where applicable



**Table 2-5**  
**EPRI AMQ-IV Round 2 Target Spiked Concentrations for Reagent Grade Water**

Element	EPA DL µg/L	Optimum Range µg/L	BKG	1	2	3	4	5	6	7	8
As	1	5-100	0	5	7	22	28	50	58	90	100
Cd	0.1	0.5-10	0	0.5	1.1	2.2	3.1	3.5	6	8.2	9.3
Cr	1	5-100	0	5	8	15	21	46	52	80	92

**Table 2-6**  
**EPRI AMQ-IV Round 2 Target Spiked Concentrations for Midwest Groundwater**

Element	EPA DL µg/L	Optimum Range µg/L	BKG	1	2	3	4	5	6	7	8
As	1	5-100	0.8	5	9	18	23	40	48	86	92
Cd	0.1	0.5-10	<0.1	0.5	1.2	3.1	3.9	5.5	7	9	10
Cr	1	5-100	0.4	5	8	20	25	55	63	88	100

**Table 2-7**  
**EPRI AMQ-IV Round 2 Target Spiked Concentrations for Estuarine Water \***

Element	EPA DL µg/L	Optimum Range µg/L	BKG	1	2	3	4	5	6	7	8
As	1	5-100	3.7	50	60	230	280	550	600	800	850
Cd	0.1	0.5-10	0.7	10	16	32	41	50	62	88	97
Cr	1	5-100	4	60	80	300	380	650	720	850	980

\* Spiked to be within range when diluted 1:10

**Table 2-8**  
**EPRI AMQ-IV, Round 2 Target Spiked Concentrations for Acid Mine Drainage\***

Element	EPA DL µg/L	Optimum Range µg/L	BKG	1	2	3	4	5	6	7	8
As	1	5-100	5.6	70	100	330	410	700	770	870	940
Cd	0.1	0.5-10	4	20	28	40	48	62	71	85	93
Cr	1	5-100	4	50	70	220	290	450	520	910	1000

\* Spiked to be within range when diluted 1:10

To test for compatibility of the test elements with the study matrices, aliquots of the concentrated spiking solutions were spiked into samples of the matrices near the highest target spike concentrations and allowed to sit for approximately three weeks. The samples were then analyzed in duplicate by ICP-MS. No stability problems were noted. Tables 2-9 through 2-12 summarize the results of the stability testing.

**Table 2-9**  
**AMQ-IV Round 2 Pre-Test Stability of Concentrated Spiking Standards**

Element	Spike	Bkg	Result 1	Result 2	Recovery
As	4000	0	4070	3950	100%
Cd	2000	0	1970	2000	99%
Cr	4000	0	4110	4120	103%

**Table 2-10**  
**AMQ-IV Round 2 Pre-Test Stability of Analytes in Midwest Groundwater**

Element	Spike µg/L	Bkg µg/L	Result 1 µg/L	Result 2 µg/L	Recovery
As	90	0.8	94	95	104%
Cd	10	0	9.7	9.6	97%
Cr	80	0.4	82	81	101%

**Table 2-11**  
**AMQ-IV Round 2 Pre-Test Stability of Analytes in Acid Mine Drainage**

<b>Element</b>	<b>Spike μg/L</b>	<b>Bkg μg/L</b>	<b>Result 1 μg/L</b>	<b>Result 2 μg/L</b>	<b>Recovery</b>
As	850	5.6	934	945	110%
Cd	90	4	97	95	102%
Cr	900	4.5	945	969	106%

**Table 2-12**  
**AMQ-IV Round 2 Pre-Test Stability of Analytes in Estuarine Water**

<b>Element</b>	<b>Spike μg/L</b>	<b>Bkg μg/L</b>	<b>Result 1 μg/L</b>	<b>Result 2 μg/L</b>	<b>Recovery</b>
As	900	3.7	913	910	101%
Cd	80	0.7	79	78	97%
Cr	800	4	852	854	106%

## 2.5 References

1. W.J. Youden and E.H. Steiner, Statistical Manual of the Association of Official Analytical Chemists, 1975.
2. American Society for Testing and Materials, "Standard Practice for Determination of Precision and Bias of Applicable Methods of Committee D-19 on Water," D2777-96, *Annual Book of ASTM Standards*, 1997.



# 3

## LABORATORY SELECTION FOR AMQ-IV ROUND 2

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A comprehensive solicitation campaign consisting of phone calls to potential participants was conducted by TRW. A total of 26 laboratories was eventually enlisted for AMQ-IV Round 2, with 18 completing the analyses.

### 3.1 Solicitation Process

Starting with the list of participants culled from the AMQ-I, -II, -III and -IV Round 1 efforts, TRW initiated a telephone survey to determine whether the potential participants were interested in joining the AMQ-IV Round 2 effort and whether they had the requisite equipment.

### 3.2 Laboratory Selection Process

A key contact was identified and contacted by TRW personnel. A profile on the laboratory capabilities was developed using the Laboratory Contact Worksheet (Appendix B).

The following criteria were applied to the respondents:

- Experience with methods selected for qualification.
- Commitment/capability to do all or most of the AMQ-IV Round 2 elements.

After intensive solicitation effort, 26 laboratories were found to meet these criteria, 18 of which completed the study. Since few laboratories routinely analyze the elements of interest in acid mine drainage and estuarine samples, laboratories with experience analyzing complex matrices were solicited to analyze these samples. Table 3-1 lists the laboratories completing AMQ-IV Round 2. All participants analyzed the reagent grade water and midwest groundwater samples. Fifteen of the laboratories analyzed the estuarine samples and seventeen of the laboratories analyzed the acid mine drainage samples.

**Table 3-1**  
**Laboratories Completing AMQ-IV Round 2**

Laboratory	Matrices				Elements		
	GW	RGW	EST	AMD	As	Cd	Cr
Alabama Power	X	X	X	X	X	X	X
BC Analytical - Glendale	X	X	X	X	X	X	X
CDS Laboratories	X	X	X	X	X	X	X
Centerior Services	X	X	X	X	X	X	X
Duke Power	X	X	X		X	X	
Duquesne Light	X	X	X	X	X	X	X
Florida Power	X	X	X	X	X	X	X
Kentucky Utilities Company	X	X	X	X	X	X	X
Micro Methods	X	X	X	X	X	X	X
New York State Electric & Gas Corporation	X	X	X	X	X	X	X
Pennsylvania Power & Light Company	X	X		X		X	X
Public Service Company of Colorado	X	X	X	X	X	X	X
San Diego Gas & Electric	X	X	X	X	X	X	X
Savannah Laboratories - Mobile, AL	X	X	X	X	X	X	X
South Carolina Gas & Electric Co.	X	X	X	X	X	X	X
Tampa Electric Company	X	X	X	X	X		X
Wisconsin Public Service Corp.	X	X		X	X	X	X
Wisconsin Electric Power Company	X	X		X	X	X	X

GW = Midwest Groundwater

RGW = Reagent Grade Water

EST = Estuarine

AMD = Acid Mine Drainage

# 4

## AMQ-IV ROUND 2 SAMPLE PREPARATION AND DISBURSEMENT

The activities associated with sample preparation and disbursement included hardware checkout, sample acquisition, sample spiking, and development of participant instructions and reporting forms. Details of these activities are presented in the following sections.

### 4.1 Spiking Hardware Checkout and Equipment Calibration

AMQ-IV Round 2 employed the same churn splitters used in all of the AMQ studies. Figure 4-1 shows one of the four all-polyethylene 120-L churn splitters used in AMQ-IV Round 2. A separate churn splitter was used for each matrix to avoid cross contamination between the sample matrices.

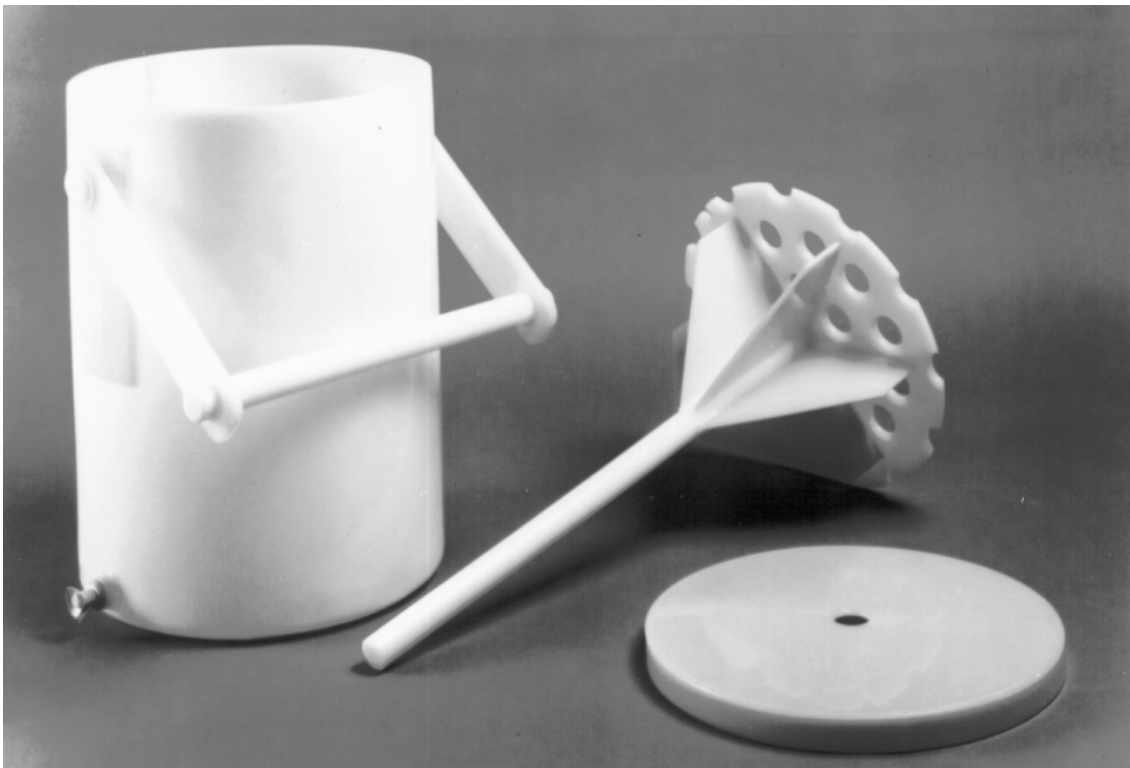


Figure 4-1 Photograph of Churn Splitter Used during AMQ-IV Round 2 Effort

As part of the AMQ-I study, a test was conducted to determine the time necessary for thorough sample mixing. After the churn splitter was filled with a known volume of deionized water, a manganese spiking solution was prepared so that thorough mixing with the water in the splitter would result in a manganese solution of exactly 5.0 ppm. After the spiking solution was added to the top layer of the water in the splitter, the churn handle was moved at a rate of 7 inches/second (18 cm/sec) and samples were withdrawn through the spigot at the bottom at specified time intervals. Manganese concentrations were determined by Flame AAS. The plot of manganese concentrations versus time (Figure 4-2) shows that top-to-bottom liquid movement was very rapid and that thorough mixing was achieved in less than three minutes. For the AMQ-IV Round 2 samples a five-minute mix period followed each spike addition.

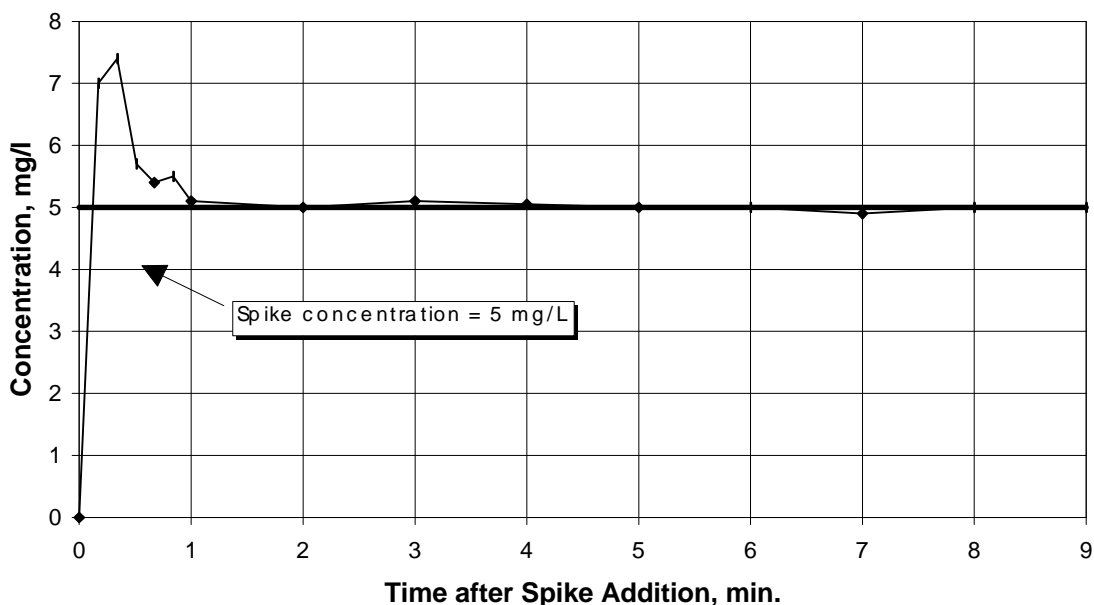


Figure 4-2 Plot of Manganese Concentrations with Time in the Churn Splitter

To calculate the amount of spiking solution required to prepare the test samples, the total solution volume in the churn splitter had to be known. A digital platform scale with 200 kg capacity was used to weigh the splitters and liquid contents to the nearest 0.05 kg. Whenever a volume measurement was needed, triplicate 50-mL aliquots of solutions were withdrawn for determination of solution density. The volume of solution in the churn splitter was then calculated from its weight and density. The scale was calibrated immediately prior to the spiking activity.



## **4.2 Sample Collection/Stabilization**

Collection of the AMQ-IV Round 2 test matrices is described in the following sections. Since the AMQ program emphasized matrix effects rather than the absolute trace element concentrations of the matrices, no nitric acid was added to the field samples prior to their arrival at TRW. Upon receipt, and after aliquots were removed for pH, anion, and TDS analysis, samples were stabilized with Ultrex® grade nitric acid to pH<2. The amount of acid added and pH readings were recorded on an Acid Stabilization Worksheet (Figure 4-3). The stabilized samples were checked again in several hours and again on the day of spiking to verify that the pH remained below 2.

### **4.2.1 Groundwater Sample Collection**

The midwest groundwater and acid mine drainage samples were collected by utility personnel at each utility's groundwater sampling site for the respective source. For each matrix, a total of 100 L was collected in four 25 L carboys. The carboys were cleaned by the procedure in Table 4-1 prior to shipment to the utility.

A complete set of sampling requirements and procedures was transmitted to the utility providing the samples prior to the collection. Approximately one gallon (4L) of sample was used to rinse each carboy and discarded. After rinsing, each container was filled with fresh sample to within two inches (5 cm) of the top and capped. Labels were then affixed with strapping tape. The filled carboys were repackaged in their original shipping crates and secured by padlocks. Federal Express 2-day service was used for transport to TRW.

### **4.2.2 Estuarine Sample Collection**

A sample was collected weekly at the estuarine sampling site in order to monitor the arsenic, chromium and chloride concentrations. Once the concentrations of these analytes reached a level that the plant considered to be suitable, the matrix sample was collected. A total of 100 L of was collected in four 25 L carboys. The carboys were cleaned by the procedure in Table 4-1 prior to shipment to the utility.

Prior to the collection, a complete set of sampling requirements and procedures, the same as those for collecting the groundwater samples, was transmitted to the utility providing the samples.

## ACID STABILIZATION OF AMQ SAMPLES

Matrix: \_\_\_\_\_

Date Stabilized: \_\_\_\_\_

pH	Volume of Acid Added
1.	
2.	
3.	
4.	
5.	
6.	
7.	
8.	
9.	
10.	

Figure 4-3 Acid Stabilization Worksheet

**Table 4-1**  
**Method for Cleaning AMQ Sample Carboys, Disbursement Bottles and Churn Splitters**

Step	Activity
1	Fill with 10% (w/w) HCl (AR grade).
2	Allow to stand 48 hours.
3	Empty and rinse with ASTM Type III water.
4	Fill with 10% (w/w) HNO <sub>3</sub> (AR grade).
5	Allow to stand 48 hours.
6	Empty and rinse with ASTM Type III water.
7	Fill with ASTM Type I water.
8	Allow to stand several weeks or until needed, changing water periodically to ensure continued cleaning.

### 4.3 Test Matrix Characterization

Once the samples were in-house, they were subjected to survey elemental and anion analyses to determine whether the sample concentrations roughly fit the concentration needs of the project and to characterize the background chemical composition of the samples.

Samples for anion, conductivity and total dissolved solids (TDS) analyses were withdrawn and stored under refrigeration prior to stabilizing the matrices with nitric acid. Duplicate samples of the stabilized matrices were analyzed by Inductively Coupled Plasma - Mass Spectrometry to characterize the major constituents of the test matrices. These results are contained in Table 4-2.

The three AMQ-IV Round 2 analytes are listed first in the table, followed by other cations of interest. The background cation data along with the anion, conductivity and TDS results yield important information on the chemical make-up of the matrices. These samples were deemed suitable for the study's needs.

Participants were told that the high TDS matrices, estuarine and acid mine drainage, had high concentrations of dissolved solids. It was recommended that they dilute these

samples and the matrix spikes were selected accordingly. Most of the participants diluted these samples by a factor of ten.

**Table 4-2**  
**Background Data for AMQ-IV Round 2 Test Matrices**  
 (Results in mg/L unless otherwise noted.)

<b>Analyte</b>	<b>Groundwater</b>	<b>Estuarine</b>	<b>Acid Mine Drainage</b>
As (µg/L)	0.8	3.7	5.6
Cd (µg/L)	nd<0.1	0.7	4.0
Cr (µg/L)	0.4	4.0	4.0
Ag	nd<0.004	nd<0.004	nd<0.004
Al	0.02	0.18	51
B	0.02	0.40	0.27
Ba	0.080	0.053	0.026
Be	nd<0.01	nd<0.01	0.01
Ca	81	45	120
Co	nd<0.002	0.003	0.44
Cu	nd<0.003	0.004	0.021
Fe	0.1	0.5	652
K	1.5	55	5.9
Mg	38	130	45
Mn	0.004	0.066	17
Mo	nd<0.008	0.021	nd<0.008
Na	5.1	1085	39.9
Ni	nd<0.003	0.004	0.84

**Table 4-2**  
**Background Data for AMQ-IV Round 2 Test Matrices**  
 (Results in mg/L unless otherwise noted.)

<b>Analyte</b>	<b>Groundwater</b>	<b>Estuarine</b>	<b>Acid Mine Drainage</b>
Pb	nd<0.002	0.048	0.007
Se	nd<0.05	nd<0.05	nd<0.05
Sn	nd<0.003	0.056	nd<0.003
Sr	14	0.85	0.55
Ti	nd<0.006	nd<0.006	nd<0.006
V	nd<0.003	nd<0.003	0.025
Zn	nd<0.008	0.011	1.7
Zr	nd<0.003	nd<0.003	nd<0.003
Fluoride	<1	<1	<1
Chloride	5	1750	25
Bromide	<1	8	<1
Nitrate	<1	<1	<1
Sulfate	65	265	1900
Phosphate	<1	<1	<1
TDS	400	3800	3000
Conductivity, µmhos/cm	530	5700	2500

#### 4.4 Procedures For Sample Processing

Bottle identity was tracked by using a two-step process to separate the filling and sorting/packing steps. As a result, the number of different ongoing activities during the filling operation was minimized. This two-step process ensured bottle identity by:

- Using a two-label system as a cross check

- Having only bottles for one matrix and one spike concentration level off the storage shelf at one time

The accuracy of spike additions was controlled by:

- Use of a Spike Calculation Worksheet discussed in Section 4.4.2
- Operation of the churn handle at pre-calibrated rates to ensure complete mixing

#### **4.4.1 Sample Tracking System**

Two sets of sample labels were used. The Pre-test Labels were placed on the bottles directly before the spiking/splitting activity began. These labels were used to identify matrix, spike concentration level, and filling order and eliminated the need for any hand-labeling during the labor-intensive spiking/splitting activity. Figure 4-4 contains the Pre-test Label coding. After filling, the bottles for each spike concentration level were stored on a separate shelf until preparation of individual laboratory packages. The adhesive backed final Test Labels were affixed during the packaging of samples for shipment, thus providing a double check of sample identity and reducing the chance of sample confusion.

The Test Label contains the following information:

- Laboratory Identification Number
- Matrix Identification Code
- Spiking Concentration Level
- Bottle Filling Order

With the exception of the bottle filling order, all other identifiers were entered on the Test Label prior to sample preparation. The filling order number from the Pre-test Label was entered into the last two digits of the sample identification number on the Test Label which was affixed to the bottle. For AMQ-IV Round 2, a Youden paired study, the spiking level was not revealed to the analysts. Instead, the spike level was indicated by a code letter on the Test Label. Figure 4-5 shows the blank final Test Label. The actual sequence of events during sample preparation and processing is discussed in the following sections.

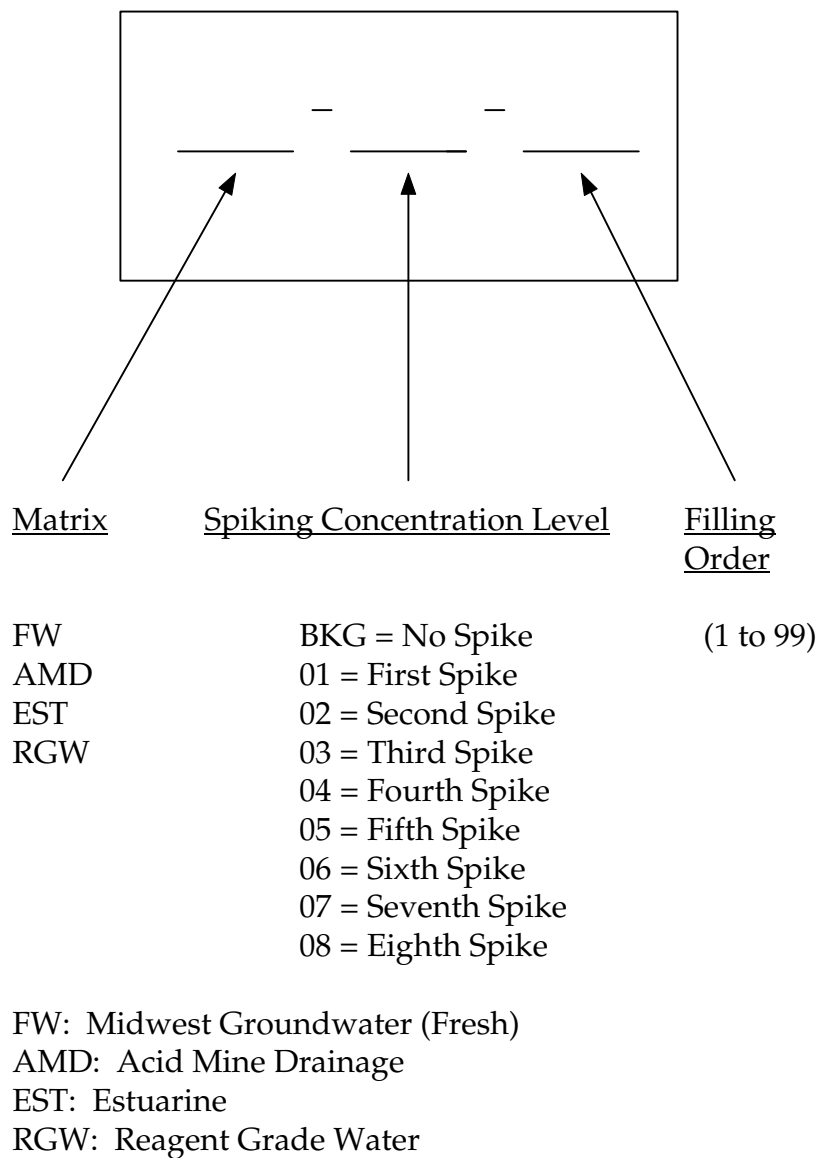


Figure 4-4 Pre-Test Label Coding

# EPRI AMQ-TC – Round 1

**AMQTC**

**Round 1**

**Sample ID:** \_\_\_\_\_ - \_\_\_\_\_ - \_\_\_\_\_ - \_\_\_\_\_

**Matrix Type:** Reagent Grade Water (05)

Freshwater (08)

Estuarine (09)

Acid Mine Drainage (10)

Figure 4-5 Test Label for Sample Bottles

## 4.4.2 Sample Filling Procedure

Figure 4-6 provides an overview of the filling procedure. The stepwise procedure follows:

- a. Place the empty churn splitter on the scale and record its tare weight on the Spike Calculation Worksheet (Figure 4-7).
- b. Empty the carboys for the current matrix into the designated churn splitter. Churn for 5 minutes to mix.
- c. Measure pH and record on the pH Verification Worksheet (Figure 4-8). Adjust pH, if necessary, to <2 by adding 5 mL increments of concentrated nitric acid (Ultrex grade, Baker Chemical).
  - Operate churn handle for 5 minutes. Check pH and adjust as needed with the acid. Record all data on the Pre-Spike pH verification Worksheet.
  - Repeat until pH is reduced to <2.
  - Operate churn handle for 30 minutes in "5 minutes on/5 minutes off" cycle. Check the pH every ten minutes. If the pH remains stable at <2, then record the pH on the pH Verification Worksheet. If the pH>2, repeat step c.
- d. Fill a tared 50 mL volumetric flask with sample. Weigh the filled flask and calculate the density by using the formula:

$$\text{Density} = \frac{\text{Weight of 50 mL of Sample in Grams}}{50 \text{ mL}} \quad (\text{eq. 1})$$



Perform in triplicate. Record all weights on the density determination portion of the pH Verification Worksheet.

- e. Move the bottles for the background portion of the current matrix to the bench top adjacent to the churn splitter.
- f. Place the Pre-Test Labels on the bottles.
- g. Empty the Type I Water from these bottles one at a time. Inspect the bottle for residual DI water. If no residual water is observed, fill the bottle as indicated in Step h. If residual water is observed, rinse the bottle with a small portion (approximately 25 mL) of the current spike concentration level sample from the churn splitter. Dump the rinse into a waste container and inspect the bottle. If a film is still found, discard the bottle. All bottles passing this inspection are filled as indicated in Step h.
- h. Operate the churn handle at 7 inches/second (18 cm/sec) for five minutes. While continuing to operate the handle, fill the bottles for the current spike level. Replace the top and wipe the outside of the bottle dry. Place the bottle on the designated shelf.
- i. After all sample bottles have been filled for a given spike concentration, record the weight of the churn splitter and sample solution on the Spike Calculation Worksheet. Calculate the spike requirements for each element.
- j. Weigh the precleaned Teflon beaker for this spike and record the values on the Spike Calculation Worksheet. The total beaker weights in the churn at the end of each spike will be added to the tare weight on the next higher spike.
- k. Using the required single element standards (Inorganic Ventures, certified), weigh out the first standard into a polystyrene disposable beaker. Transfer the solution quantitatively into a precleaned Teflon beaker. Repeat with the remaining two standards.

Place the Teflon beaker containing the standards on the churn paddle and tip the beaker over to empty the spiking solutions into the sample. Churn for 5 minutes at 7 inches/sec (18 cm/sec).

- l. Move the bottles for the current spike concentration level to the bench top adjacent to the churn splitter.
- m. Repeat steps f through l until all of the spike concentration levels have been completed.
- n. Repeat steps a through m for each subsequent matrix.

At the end of the filling effort, all sample bottles carried a Pre-Test Label and were segregated in a cabinet by matrix and spike concentration level. The next step was to package the appropriate bottles and forms into boxes for shipment to each laboratory.

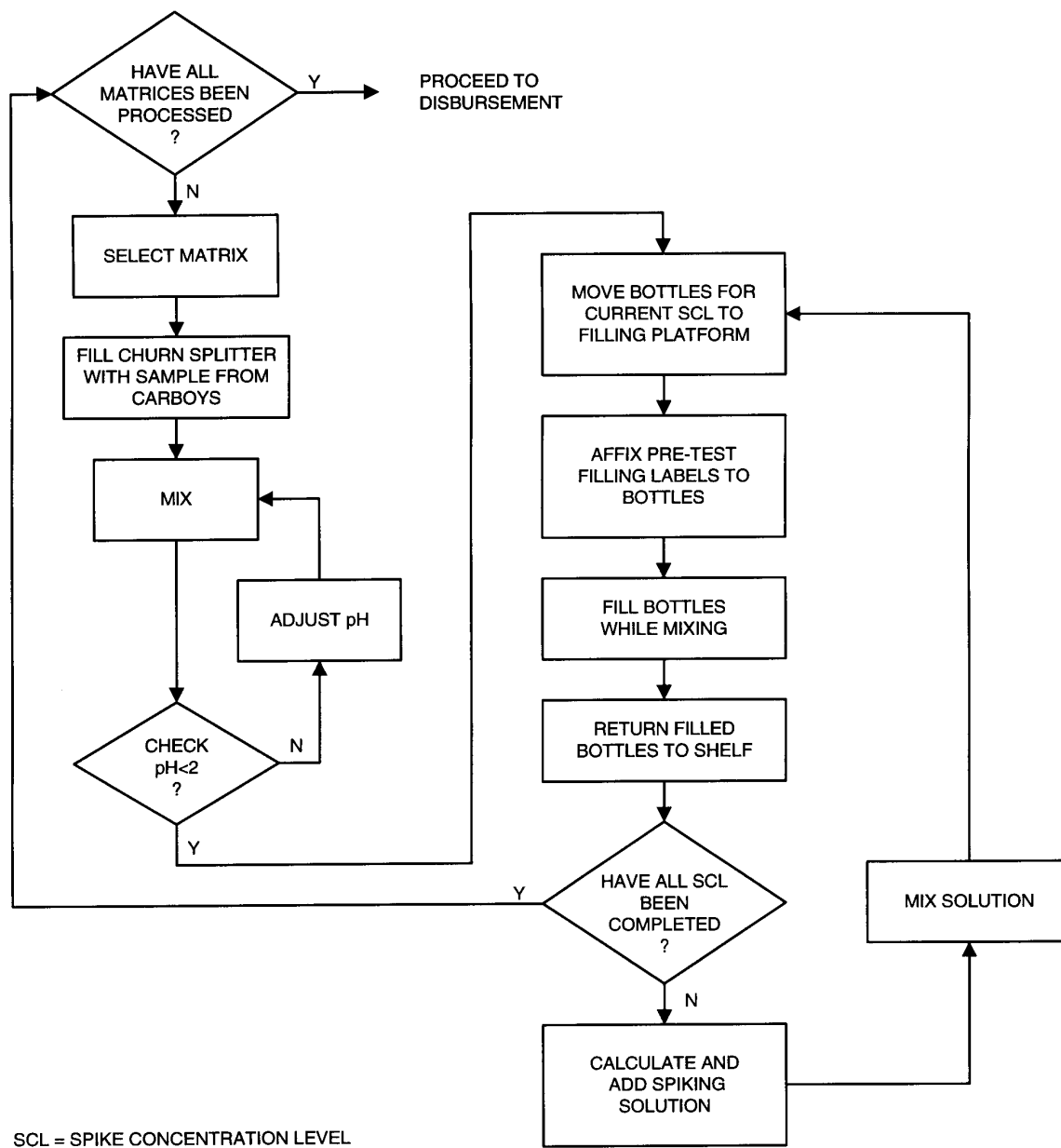


Figure 4-6 Bottle Filling Procedure

# AMQ-TC ROUND 1 SPIKE CALCULATION WORKSHEET

SPIKE LEVEL (CIRCLE PAIR)  
1 2 3 4 5 6 7 8

OPERATOR: \_\_\_\_\_

DATE: \_\_\_\_\_

MATRIX: \_\_\_\_\_

SPIKE LEVEL	SPIKE ELEMENT	(a) TOTAL WEIGHT (KG)	(b) TARE WEIGHT (KG)	(c) CALCULATED TOTAL VOLUME (L)	(d) TARGET SPIKE CONCENTRATION (PPB)	(e) CURRENT SPIKE CONCENTRATION (PPB)	(f) REQUIRED WEIGHT SPIKE SOLUTION (G)	(g) ACTUAL WEIGHT OF SPIKE SOLUTION (G)	(h) CONCENTRATION AFTER SPIKE (PPB)
LOW	As		CHURN	DENSITY					
	Cd		BEAKERS	VOLUME					
	Cr		TOTAL						
HIGH	As		CHURN	DENSITY					
	Cd		BEAKERS	VOLUME					
	Cr		TOTAL						

TEFLON BEAKERS TARE WEIGHT (G)

(a) TOTAL WEIGHT OF CHURN SPLITTER + SAMPLE AND SPIKING BEAKER(S) AND SPIKING SOLUTION

(b) TARE WEIGHT OF CHURN SPLITTER AND SPIKING BEAKERS

(c) = [(a)-(b)] ÷ DENSITY = CALCULATED TOTAL VOLUME OF SAMPLE

(d) TARGET TOTAL SPIKE CONCENTRATION

(e) = (d) FROM PREVIOUS SPIKE LEVEL

(f) = (c) x [(d) - (e)] ÷ CONCSOL

(g) THE WEIGHED QUANTITY OF SPIKING SOLUTION ACTUALLY USED

(h) = [(g) x CONCSOL ÷ (c)] + (e)

WHERE CONCSOL = CONCENTRATION OF SPIKING SOLUTION IN PPM

LOW

SPIKE 1

SPIKE 2

SPIKE 3

SPIKE 4

SPIKE 5

SPIKE 6

SPIKE 7

TOTAL (g)

+1000 (kg)

RECORD ON NEXT HIGHER LEVEL SPIKE COLUMN (i)

HIGH

SPIKE 1

SPIKE 2

SPIKE 3

SPIKE 4

SPIKE 5

SPIKE 6

SPIKE 7

TOTAL (g)

+1000 (kg)

Figure 4-7 Spike Calculation Worksheet AMQ-IV Round 2

## AMQ-IV Round 2

Pre-Spike pH Verification  
and  
Density DeterminationpH Verification

pH Reading	Estimated Acid Required to Achieve pH	Acid Added	
		Volume	Time Mixed
1.			
2.			
3.			
4.			

Acid Lot No. \_\_\_\_\_

## Density Determination

1	2	3	
_____	_____	_____	Gross Weight, g Sample + Flask
_____	_____	_____	Tare Weight, g Flask
- _____	- _____	- _____	Net Weight, g Sample
÷ 50	÷ 50	÷ 50	Divide by Flask Volume, mL
_____	_____	_____	Density, g/mL

Figure 4-8 pH Verification Worksheet

#### **4.4.3 Packaging Samples for Disbursement to Participating Laboratories**

An overview of the steps that comprise the packaging operation is presented in Figure 4-9 and details of these activities are presented in the following sections. In general:

- Filling order numbers are entered on each of three matching Identification (ID) Labels.
- Identical ID Labels are placed on a Test Label, Laboratory Data Reporting Form (LDRF) and Distribution Record.
- Test Labels are placed on the bottles.
- The sample bottles are sealed in polyethylene bags and placed in shipping cartons.
- The accompanying paperwork is placed in a large envelope in the carton.

In order to eliminate the labor intensive step of typing all of the sample Test Labels, a system employing computer generated adhesive Identification (ID) Labels was devised. The ID Labels were prepared in sets of three, containing all the information required for the Test Label except the bottle filling order. This was entered during packaging. Sets of ID Labels were prepared in the order they were to be placed on the bottles. The spiking order was identified by a letter code in order to disguise the relative spiking level. After entering the bottle filling order on each of the three ID Labels, one was placed on the Test Label, one on the LDRF and one on the Distribution Record. This accomplished the following:

- The bottle was fully identified for distribution to the participant.
- The LDRF sample ID exactly matched the bottle label.
- A record was maintained of each bottle sent to each participant.

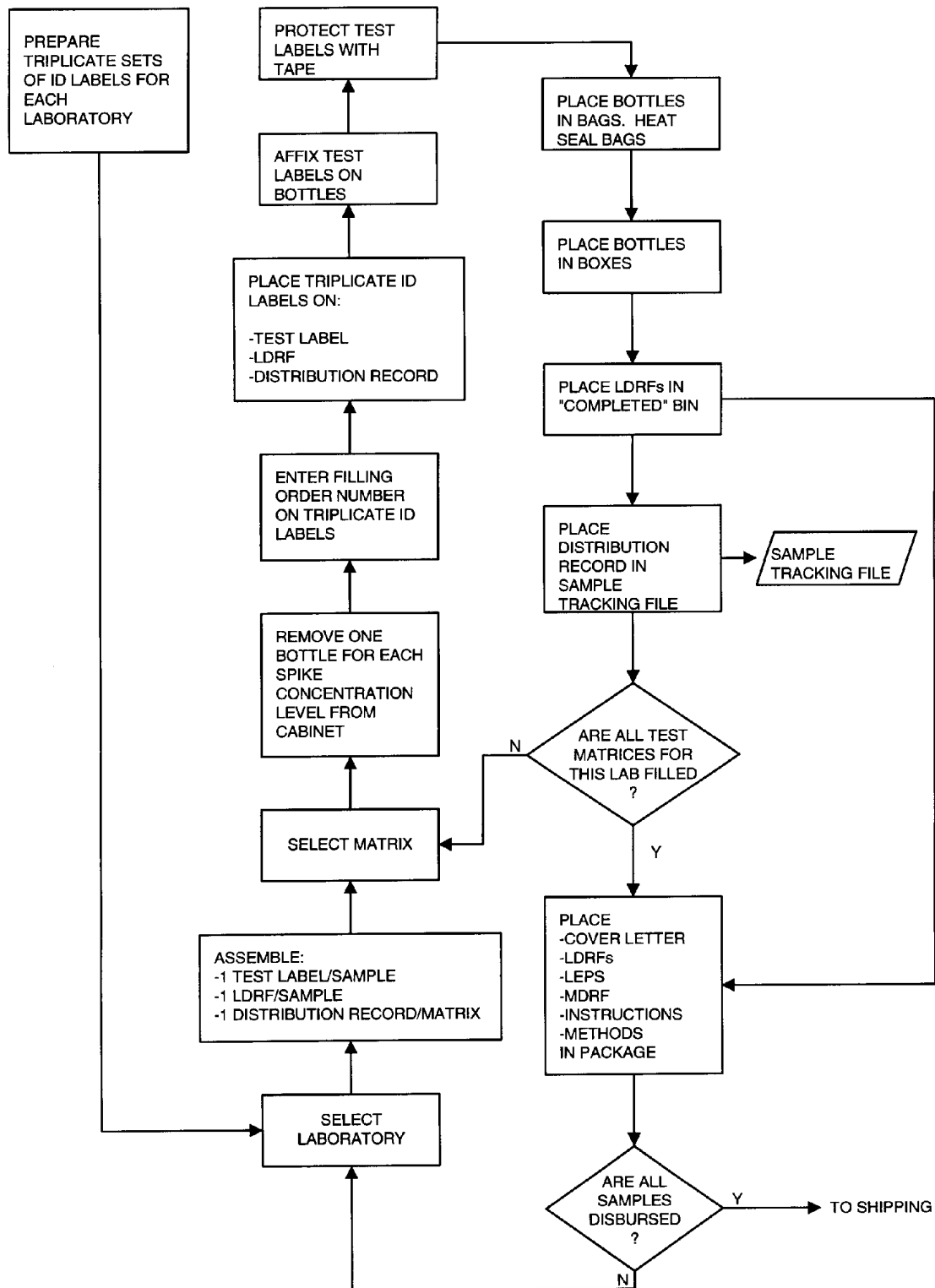


Figure 4-9 Sample Packaging Procedure

The following describes the packaging procedure:

- a. A laboratory is selected and the required number of blank forms are assembled for that laboratory:
  - Test Labels - one for each sample.
  - Lab Data Reporting Forms (LDRFs) - one for each sample.
  - Distribution Records - one for each matrix.
- b. The Spiking Level Code sheet, which translates the spiking level number on the Pre-Test Label to the spiking level letter code on the Identification Labels is placed in a prominent position for easy reference.
- c. The prepared Identification (ID) Labels are assembled in the order used (lowest to highest) for the selected laboratory and matrix. The Spiking Level Code Sheet is used to verify that the labels were in the correct order.
- d. A bottle with the first spike concentration level of the same matrix selected in Step c is removed from the shelf.
- e. A bottle with the next highest spike concentration level of the same matrix selected in Step b is removed from the shelf.
- f. Step e is repeated until all of the spike concentration levels for a given matrix have been assembled. The bottles are lined up in the sample processing area in ascending order of spiking level.
- g. The bottle with the lowest spiking level is selected.
- h. The Spiking Level Code Sheet is used to select the correct set of three ID Labels for the selected bottle.
- i. The bottle filling order on the Pre-Test Label is entered on each of the three ID Labels.
- j. After checking the three ID labels to verify that they are identical, one is placed on the Test Label, one on the LDRF and one on the Distribution Record.
- k. After double checking the Spiking Level Code Sheet to verify that the letter code is correct for the spiking level, the Test Label is placed on the bottle completely covering the Pre-Test Label.
- l. The bottle label is secured with wide transparent tape, the sample bottle is placed in a polyethylene bag, the bag is heat sealed and the sample is placed in the shipping carton. The completed LDRFs are placed in the "completed" bin.
- m. Steps g through l are repeated until all bottles for the selected matrix have been processed.
- n. Steps c through m are repeated with the remaining matrices for the selected laboratory.

- o. All of the forms for a given laboratory are collated: the cover letter, the "Instructions to the Laboratories," "Laboratory Data Reporting Forms," "Laboratory Equipment and Practices Survey," "Method Parameters Reporting Form," and the specific analytical methods to be employed. They are then placed in a large envelope, which is shipped inside the carton. Finally, the carton is sealed and the shipping label is secured to the carton.
- p. Steps a through o are then repeated for the remainder of the laboratories.

In this instance, the analytical methods included were the EPA Metals Method (Atomic Absorption), and EPA Methods 206.2, 213.2 and 218.2.

#### **4.4.4 Shipping of Samples to the Participating Laboratories**

The processed samples were shipped to the participating laboratories via two-day air express. Although the processed samples contained nitric acid, the acid concentration was below the 0.15% (wt/wt) nitric acid corrosive criterion established by the U.S. Department of Transportation in 49 CFR Part 173.

#### **4.5 Instructions To Participating Laboratories**

The instructions to participating laboratories provided information on:

- Elements and matrices to be tested
- Bottle coding
- Reporting requirements
- Preparation and analytical procedures

Appendices C through F contain a copy of the instructions, Laboratory Data Reporting Form (LDRF), Laboratory Equipment and Practices Survey (LEPS), and Method Parameters Reporting Form (MPRF) which were sent to the participating laboratories. Annotated copies of the EPA MCAW Metals Method, Method 213.2 for cadmium, Method 206.2 for arsenic and Method 218.2 for chromium were also sent to all the participants. The LEPS is designed to collate information on the equipment and laboratory practices used by the participant during sample analysis. It also asks some basic questions concerning analyst and supervisor experience and education. The MPRF solicits information on the instrument operating parameters used to analyze the samples. The data obtained from the LEPS and MPRF are discussed in Section 7. A LDRF was included for each sample. Analysts were instructed to report all analytical results, including zero and negative values, on the LDRFs.



# 5

## QUALITY ASSURANCE/QUALITY CONTROL

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Detailed procedures were prepared for the spiking, filling and shipment of samples as described in the preceding section. Besides carefully following those procedures, TRW implemented the following quality assurance measures during disbursement:

- The spiking and disbursement activity was audited by TRW personnel experienced in contamination control. Adherence to the test plan was closely monitored.
- Special single element standards made from "6 nine's" metal or primary standards were used for all spike solutions.
- Separate churn splitters were used for each matrix.
- The spiking laboratory was cleaned floor to ceiling prior to the sample spiking operation and was made off limits to all but the AMQ disbursement personnel.
- Sample concentrations were verified by analyzing the sample bottles containing the highest test concentration.
- Prior to shipment, filled sample bottles were stored in locked cabinets. Labeling protocol provided traceability with regard to order of filling.

Approximately three months after the samples were shipped to the participants, samples retained at TRW were analyzed to confirm sample stability. The EPA permits nitric acid stabilized samples to be stored for up to six months prior to the determination of most trace metals. It was decided that, since the participating laboratories would analyze the samples anywhere from one to two months after they were bottled, the stability of the samples should be confirmed. During the test round, duplicate samples from the lowest and highest test concentration bottles from each matrix were analyzed for the test elements approximately three months after filling. The spike recovery was computed and compared to the amount actually added to the test samples.

The results of the verification and stability check analyses are described in the following sections.

### 5.1 Analyses to Verify AMQ-IV Round 2 Sample Concentrations

During the AMQ-IV Round 2 test program, verification of the test concentrations was accomplished by indirect and direct methods. The indirect methods included auditing the spiking procedure, calibrating the scale used to weigh the churn splitter, and

auditing the spike log books. Besides these indirect practices, the highest test concentration sample from each matrix was analyzed for each element before the samples were disbursed to the participants. If an error occurred in any one of the spiking steps, it would show up in the highest test concentration. The results of these analyses are found in Table 5-1 and Figures 5-1 through 5-3. The samples were analyzed by TRW personnel using Inductively Coupled Plasma - Mass Spectrometry (ICP-MS). These analyses did not indicate any significant differences between the calculated and measured concentrations. All measured element concentrations were within +/-10 % of the calculated values. All of the test elements were within the analytical precision expected at the test concentrations.

## **5.2 Analyses to Confirm Stability in AMQ-IV Round 2**

The highest and lowest concentration test samples from each matrix were analyzed for the three test elements approximately three months after spiking. Analyses were performed in duplicate by TRW using ICP-MS. Figures 5-1 through 5-3 summarize the results of the stability analyses for the highest concentration samples. The actual analysis data are found in Table 5-1. Recoveries were calculated by ratioing the difference between the measured concentration of the highest and lowest samples for a given matrix to the added spike. The recoveries ranged from a low of 99% (arsenic in estuarine) to a high of 108% (chromium in reagent grade water). The results confirmed that there had been little or no change in the test samples with time.

**Table 5-1**  
**Summary of Verification and Stability Analyses for AMQ-IV Round 2**

Matrix	Arsenic			Cadmium			Chromium		
	CV	Verify	Stability	CV	Verify	Stability	CV	Verify	Stability
	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L
RGW-1	5.0	-----	4.9	0.5	-----	0.6	5.2	-----	5.3
RGW-8	100	100	106	9.5	9.6	10.0	91.1	97.3	98.5
Recovery		100%	106%		101%	104%		107%	108%
FW-1	5.0	-----	5.0	0.4	-----	0.5	5.2	-----	4.6
FW-8	91.9	92.2	93.0	10.4	10.0	10.5	100	102	102
Recovery		100%	101%		96%	100%		102%	103%
AMD-1	69.4	-----	72.3	20	-----	20.1	49.9	-----	51.2
AMD-8	941	970	968	93.3	92.4	94.5	999	1045	1000
Recovery		103%	103%		99%	102%		105%	100%
EST-1	48.6	-----	54.0	9.9	-----	9.5	60.1	-----	58.1
EST-8	857	836	854	97.6	94.0	97.5	957	985	980
Recovery		98%	99%		96%	100%		103%	103%

RGW = Reagent Grade Water

AMD = Acid Mine Drainage

FW = Midwest Groundwater (freshwater)

EST = Estuarine

CV = Calculated Value. Based on original TRW background analysis plus added spikes.

Verify = Results of TRW verification analysis of highest concentration samples prior to shipment.

Stability = Results of TRW stability analysis 3 months after sample preparation.

Recovery: Verify = Ratio of measured concentration to CV

Recovery: Stability = Ratio of difference between the measured concentrations of highest and lowest samples from the stability analysis to the CV

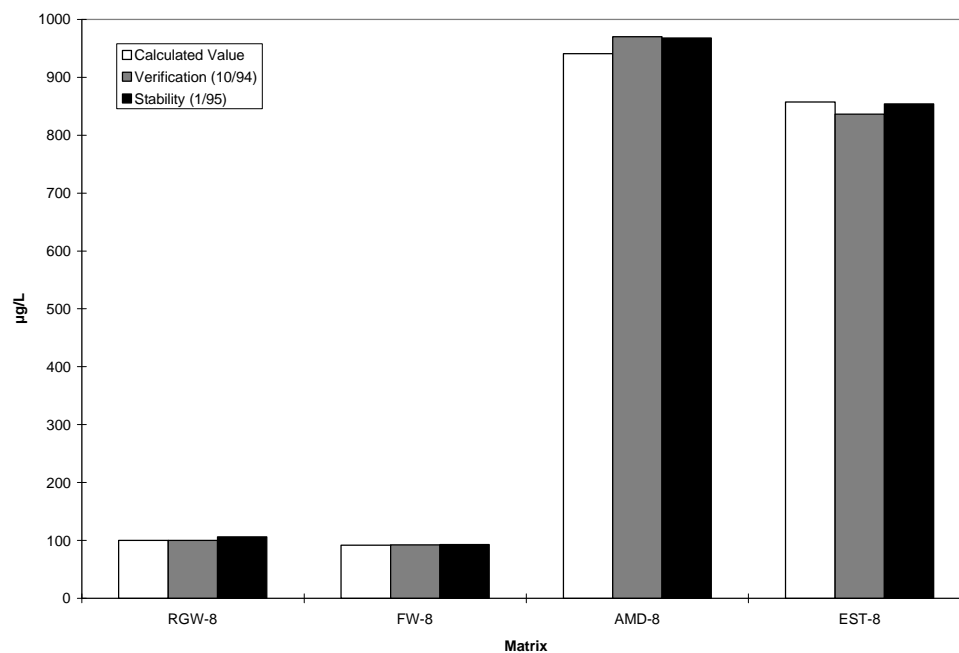


Figure 5-1 QA/QC Analysis of Highest Concentration Samples for As

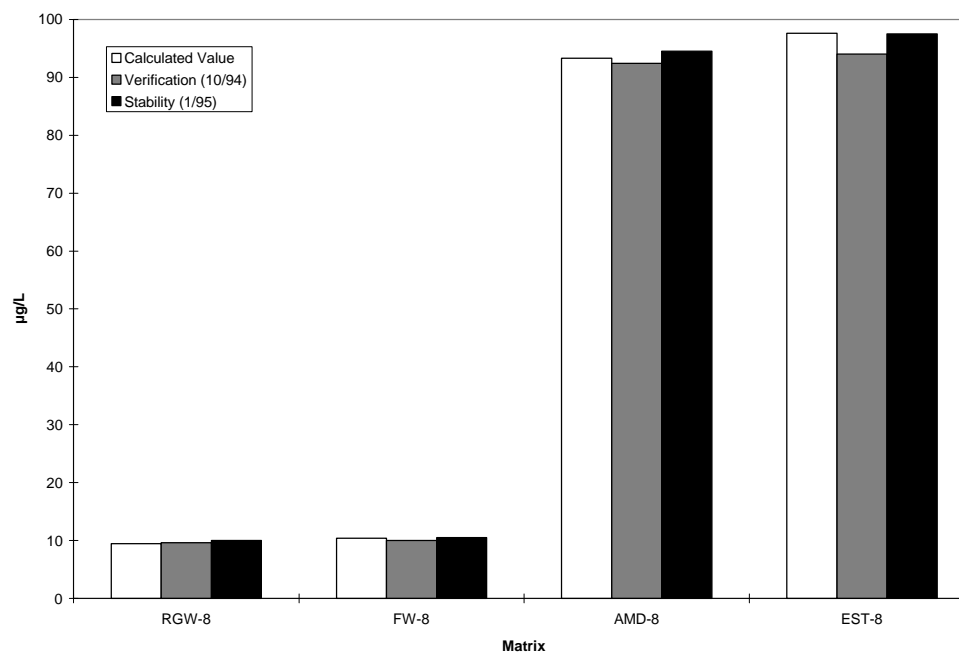


Figure 5-2 QA/QC Analysis of Highest Concentration Samples for Cd

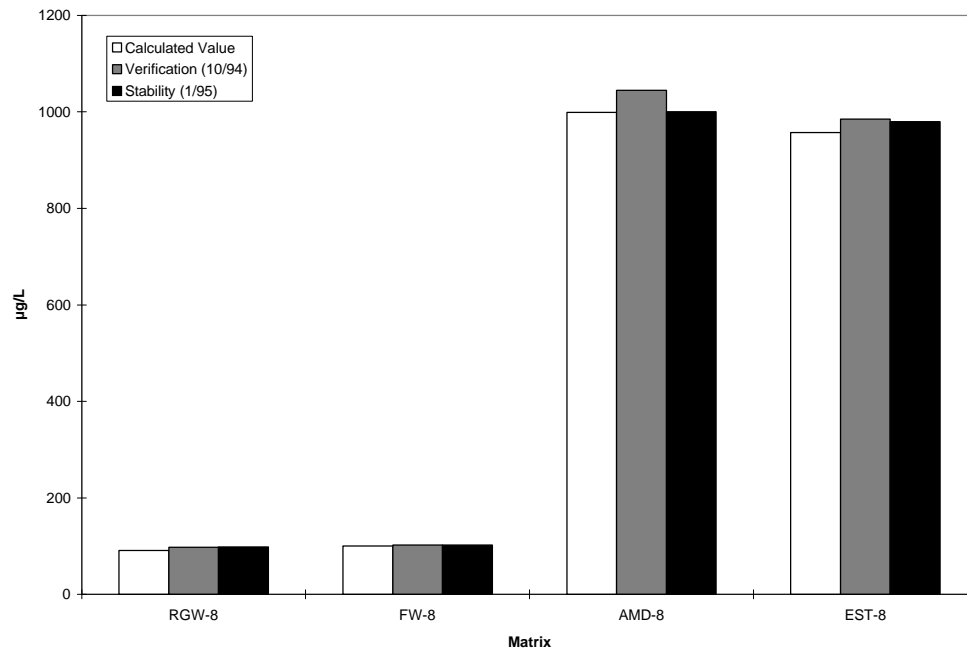


Figure 5-3 QA/QC Analysis of Highest Concentration Samples for Cr



# 6

## AMQ STATISTICAL ANALYSIS PROGRAM

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Data for this method performance study were analyzed by STATCALC, a data preparation and statistical analysis program developed by EPRI which provides computer processing according to the ASTM D2777 method. Figures 6-1, 6-2 and 6-3 provide an overview of the program.

### 6.1 STATCALC Collaborative Statistical Analysis Program

STATCALC is a set of software programs designed to operate in the personal or desktop computer environment, commonly known as an "IBM-PC". STATCALC was designed to analyze data resulting from collaborative analytical method validation studies. Such studies are conducted, both by government regulatory bodies and by private industry, to assess the precision and bias of analytical methods. The program uses procedures based on and developed using sound scientific principles, procedures that have been demonstrated and verified with actual field studies.

STATCALC was conceived and developed as a computer-assisted implementation of the preparatory and statistical information processing required by a well-known and successful standard for collaborative laboratory studies, ASTM D2777-86 (1). This standard, while very detailed with examples for collaborative studies with replicate experimental design, also provides for the studies based upon Youden pairs. The experimental design for this method performance study uses the processing subprogram "YODENPR", which has a capacity of 100 laboratories with five Youden pair observations per laboratory for each analyte and matrix.

Over the course of the AMQ study, the STATCALC program was modified to conform to the latest version of ASTM D2777. The version used to reduce the data for the AMQ-IV Round 2 study was compliant with ASTM D2777-96 (2).

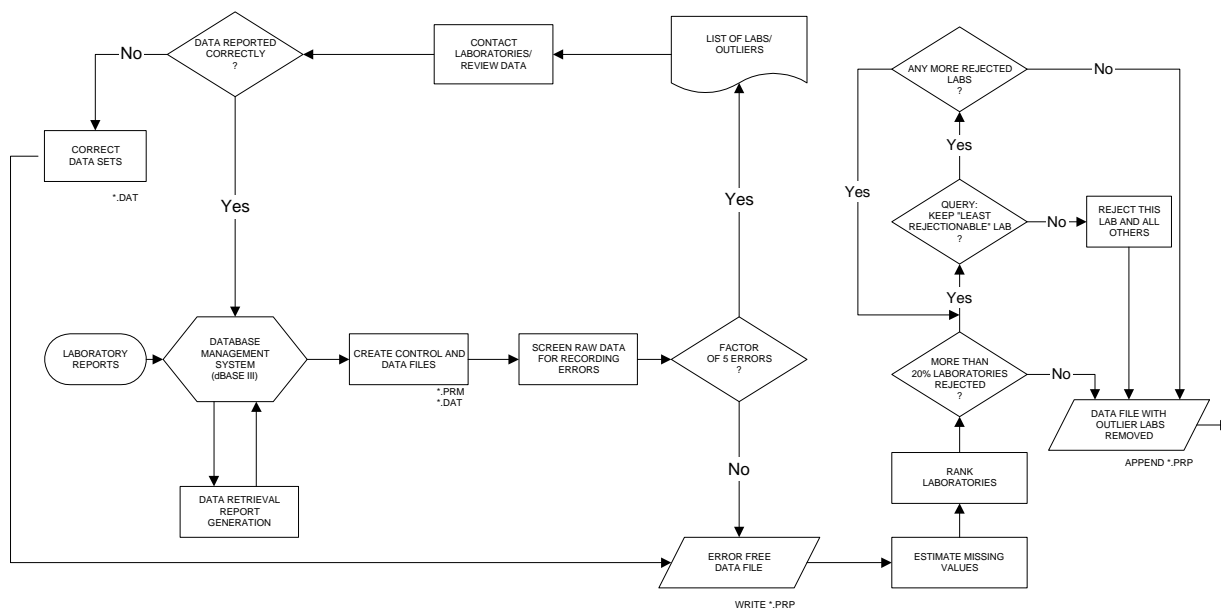


Figure 6-1 STATCALC Data Screening/Lab Ranking

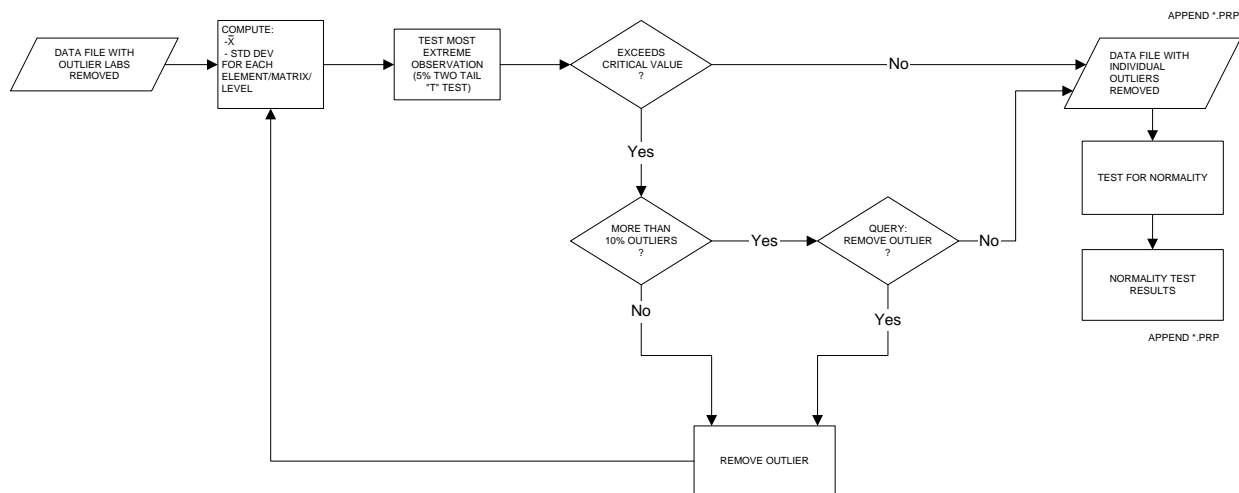


Figure 6-2 STATCALC Outlier Testing



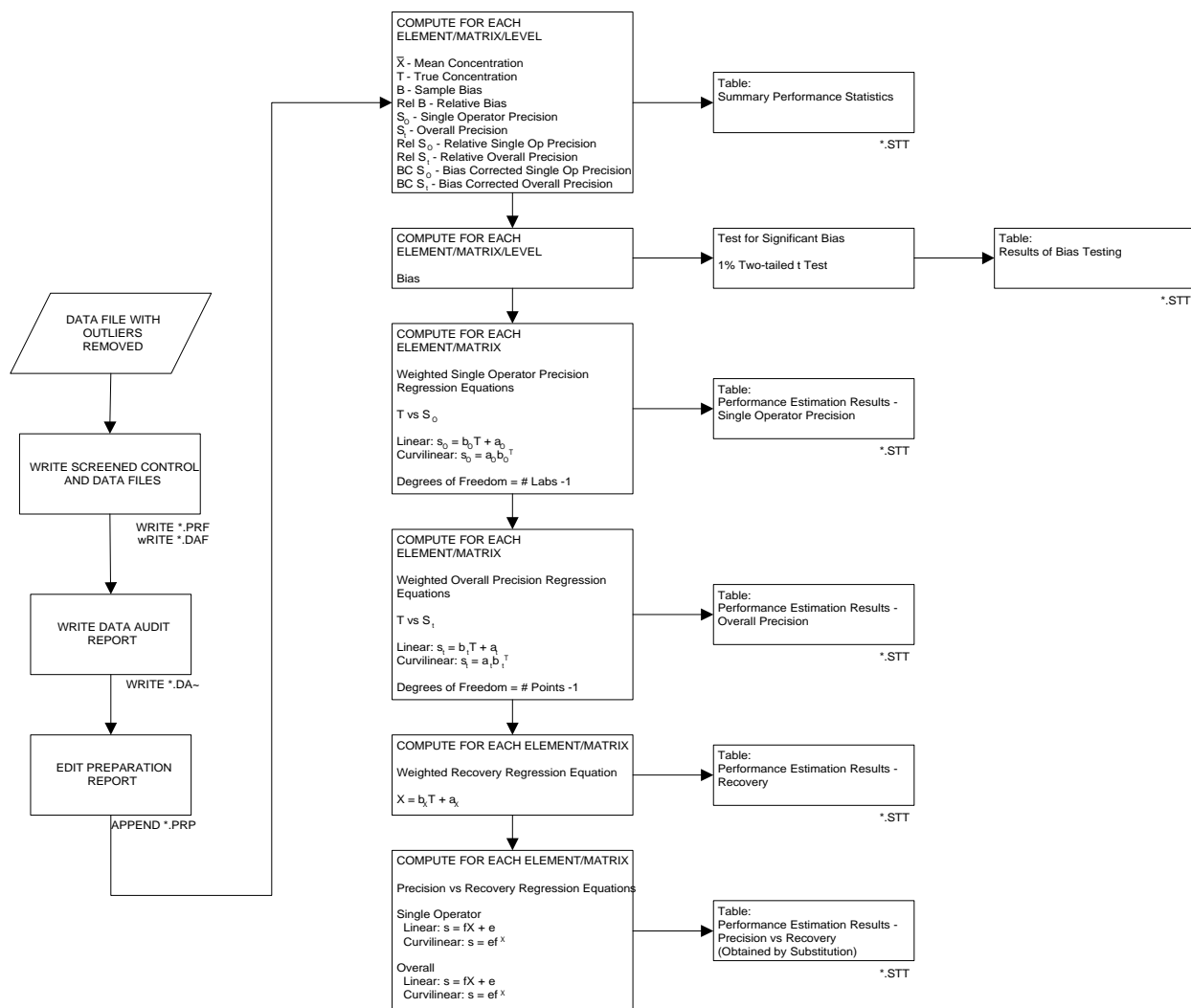


Figure 6-3 STATCALC Statistical Processing

## Program Capacities:

Number of Elements	1
Number of Laboratories	100
Number of Youden Pairs	5
Number of Replicate Concentration Levels	9
Number of Replicates per Level	7
Number of Matrixes per Run	1
Number of Data Sets	1

**6.1.1 Notation for STATCALC**

Users may freely specify, under the limitations of the Personal Computer operating system, a file name "root" of up to eight characters which precedes the "." which separates the file name root from its three letter "extension." STATCALC uses this user specified root, referred to as "\*" in the following discussions, to systematically name all of the intermediate and final input and output files created during processing with this same root name. The following files, with the exception of the data (\*.DAT) and parameter (\*.PRM) files which the user must create for each analyte/matrix, are created during STATCALC data processing. They are discussed in more detail in the following sections.

*.PRM	Of the two files that STATCALC must have, the first is a control file called the parameter (*.PRM) file. This file contains information about the type of analyte under study, the analytical method being used, the name of the matrix, the spike levels, units of measurement, and so forth.
*.DAT	The second file is the data (*.DAT) file which contains the laboratories' reported results and associated identification indexes for the analyte/matrix described in the parameter file.

*.DA~	Data that are read initially from the *.DAT file are echoed to an intermediate file (*.DA~), which provides an audit record of the actual data the program analyzes.
*.PRF	This file is a copy of the parameter file used for actual final processing, and amounts to a reconciliation of the *.PRM and *.DAT files.
*.DAF	After all checking has been accomplished, a file containing only non-rejected data is created (*.DAF). This file represents the final data set. It is used in the performance evaluation section of the program where precision and bias are estimated and reported.
*.PRP	The data preparation file, *.PRP, tracks the data preparation steps. After reading the *.PRM and *.DAT files, STATCALC first screens the data and reports possible transcription or calculation errors in the raw data file, *.DAT. Results of the lab ranking test as well as results of individual outlier testing are reported in the *.PRP file. The individual outlier test assumes that the underlying statistical population follows a normal probability model, and the results of normality testing are recorded in this file.
*.STT	The results of the summary statistic calculations are written in the statistical processing output file, *.STT, as are results of bias testing, estimation and performance regressions.
*.RGC	A file of regression coefficients is produced for use as input to other programs.
*.MEF *.MDT	Matrix effects testing (optional for pairs of matrices) produces two files, *.MEF for results of the test, and *.MDT for internal program use.

### 6.1.2 Data Notation

An observation (also called a result, recovery, measurement, observed value, data value, or data point) is the actual numerical value of the analyte concentration as reported by the laboratory. The letter "X" is used as generic notation for these reported values.

When appropriate, or necessary, the subscript "a" will be used to denote measurements for different analytes, the subscript "m" for different matrixes, the subscript "c" for different concentration levels, the subscript "l" for different laboratories, the subscript "r" for different replicates. In all cases, unless noted otherwise, the lower limits are 1 and the upper limits are the corresponding upper case letters of the respective categories of subscripts, that is:

Observation Hierarchy
Analyte: (a = 1,2,...,A)
Matrix: (m = 1,2,...,M)
Concentration Level: (c = 1,2,...,C)
Laboratory: (l = 1,2,...,L)
Replicates: (r = 1,2,...,R)
Youden Pairs: r=1

The notation for a completely specified observation would be:

Observation (Recovery)
$X_{amclr}$

The letter "T" is used as generic notation for the true concentration of the analyte. Since there are "C" different concentration levels, the set of concentration levels (T) and incremental spikes ( $\Delta T_c$ ) would be denoted:

True Analyte Spikes and Concentrations
Error! Objects cannot be created from editing field codes., $c=1,2,\dots,C$
$T_c, c=1,2,\dots,C$

Subscripts used in the text following are suppressed when not needed, as in ( $X_{cl}$ ). This is usually sufficient since with one analyte,  $a$  and  $A$  equal 1, and with a single matrix,  $m$  and  $M$  equal 1.

## 6.2 Data Validation

Data are screened and examined in various ways before being placed in a data bank and used for estimating population parameters or making decisions. To this end, data that are read initially from the DAT file are echoed to an intermediate file (\*.DA~) and, optionally, to the screen. This operation provides an audit record of the actual data the program analyzed. It also serves to isolate the user provided data file (\*.DAT) from program alteration and provide data to the next step in the analysis.

### 6.2.1 "Zero" Data

"Zero" data are not noted by the program as unusual and are treated in the same way as other nonzero measurements.

### 6.2.2 Censored or "Less Than" Data

Measurements which were reported as "less than" a particular value are handled by STATCALC as follows. A single character "flag field" is provided in the \*.DAT (input data) file for each reported value. The program checks for a "<" symbol in the flag field and, optionally, ignores the flag (treats the value as if it were measured at the censoring level) or substitutes a 0.0, depending on the result of a query to the user. The program, as written, treats such values as being reported at the upper limit or lower limit (0.0) of the possible range.

### 6.2.3 "Negative" Data

"Negative" observations are values reported as negative by a laboratory. They are handled by the program as valid data values. That is to say, the program does not preclude processing negative reported values.

## 6.3 "Factor of 5" Data Screening

Mistranscriptions of data such as transposition errors, misplaced decimal points, or inadvertently misreported units will interfere with the statistical estimates of precision and bias produced by STATCALC. To guard against this, the data are initially screened for patently obvious inconsistencies. STATCALC does not remove any data during this screening procedure but flags it for the user's review.

### 6.3.1 The Screening Procedure

After reading the \*.PRM (processing control file) and \*.DAT files, the program screens each measurement of a given analyte in a given matrix for possible transcription or clerical errors by two methods. If a value is more than five times the mean result of values from all laboratories at that concentration level, or less than one-fifth that mean, it is reported as a questionable observation.

Since the above method will not work with data sets having negative values, the program also computes the Mean Absolute Deviation, *MAD*, for each level, i.e.,

$$MAD = \frac{\sum |X - \bar{X}|}{N} \quad (\text{eq. 2})$$

where  $\bar{X}$  is the sample mean of all N results at a given level. It then calculates the individual deviation

$$|X - \bar{X}| \quad (\text{eq. 3})$$

for each value and checks if

$$\frac{|X - \bar{X}|}{MAD} \quad (\text{eq. 4})$$

is greater than 5.0.

The program reports all questionable observations and their associated identification information to the user in the data preparation result file, \*.PRP. If no such observations are encountered, that fact is also recorded in the data preparation result file. No data are removed by the screening tests. The user must evaluate each questionable observation and correct any errors in the data in the \*.DAT file. If any such corrections are necessary, the data processing must be initiated again using the corrected \*.DAT file. After all individual values have been screened, processing of the data in the \*.DAT file proceeds to the lab ranking routine.

## **6.4 Lab Ranking**

After the data set is screened initially for transcription errors and the like, it is subjected to a statistical procedure designed to detect laboratories whose results as a whole are either so consistently high or so consistently low, compared to the other laboratories, as to be considered unreasonable. Results from such a laboratory should be rejected for a given analyte and matrix. If the laboratory's data are allowed to remain in the analysis, it will materially affect the precision and bias estimates, and the results of the analysis will not be representative.

### **6.4.1 Rationale for the Test**

If a particular laboratory is producing exceedingly biased results that are consistently lower or higher than the other laboratories, and if the results from that laboratory are ranked among the other laboratories' results, the suspect laboratory will tend to get either consistently high or consistently low ranks. The measurements for a laboratory which has no such large systematic bias should rank randomly among the other laboratories' results, receiving some high ranks and some low ones. The statistical procedure which is used to test for outlying laboratories uses the sums of the several laboratories' ranks over several concentrations as the test statistic. If any given laboratory's sum is too large or too small, that laboratory may be excluded from the analysis.

STATCALC operates with a limit of no more than 20 percent of the laboratories removed by laboratory ranking. If the program detects that more than 20 percent of the laboratories need to be considered for rejection from the study, the operator is given a choice to keep the data from a laboratory that has failed the laboratory ranking test.

### **6.4.2 Discussion of the Test**

The results of each laboratory at each concentration level are ranked in ascending order with the lowest value assigned "1" and the highest value the rank of "L". If one or more observations are tied, each laboratory is given the average of the sum of the ranks of the equal observations. Rank sums are computed by summing across all

concentrations for each laboratory. If the minimum rank sum is less than the lower critical value, or the maximum rank sum is larger than the upper critical value, then laboratories with those extreme sums are rejected. If no more than 20 percent of the laboratories are rejected, and if the operator does not retain data from a laboratory that failed the laboratory ranking test, their data are excluded. Their data are not used in any further analysis and are flagged with an "r" in the data validation file (\*.DA~). The quantities needed for the lab ranking test and the test's results are reported in \*.PRP in the laboratory ranking section of the file.

As a general rule, to perform the laboratory ranking procedure, the analyst must have a complete set of data. That is, every laboratory must have at least one observation at each concentration level for replicate data or both members of each pair for the Youden pair analytical design. In the case of missing data, an estimation procedure is used. If there are measurements reported for at least three different concentration levels (one member of each of three pairs for Youden paired data) for a given laboratory, the ranking subroutine fits a simple linear regression to the actual values reported for that laboratory. The estimation procedure returns estimated recoveries from its regression line to be used in place of the missing observations. Values substituted for missing observations are used only in the laboratory ranking routine are discarded before subsequent data processing.

If there are fewer than 15 laboratories involved, the critical values for the rank sums are those found in ASTM D 2777-86 (1). If there are more than 15 laboratories, the critical values for the laboratory rank sums are computed using an approximating uniform probability distribution to calculate the quantity  $Q$  below. The data for a laboratory are rejected and not used in subsequent calculations if the laboratory's rank sum satisfies either of the inequalities below:

$$\text{Rank Sum} < C + Q \quad (\text{eq. 5})$$

or

$$\text{Rank Sum} < C \times L - Q \quad (\text{eq. 6})$$

where

$C$  = Number of Concentration Levels in the study

$L$  = Number of Laboratories

and



$$Q = L \left( \frac{aC!}{2L} \right)^{1/c} - \left( \frac{C+1}{2} \right) \quad (\text{eq. 7})$$

where

$\alpha$  = Significance Level of the Test = 0.05 (Default)

#### 6.4.3 Justification for Use of the Test

This laboratory ranking procedure is the standard in general use for evaluating data from interlaboratory studies presented in ASTM Standard D2777.

### 6.5 Testing for Outliers

The next step in the data analysis is to check those data remaining following rejection of laboratories for individual outlying observations, that is, individual recoveries for a given concentration that differ markedly from the other observations for that concentration, i.e., by an amount that cannot be explained solely by sampling variability. Such observations occur when a major disturbance (such as a radical deviation from standard procedure or an error in calculation or recording of the value) impacts the measuring process so as to grossly affect the accuracy of the measurement. These observations should be excluded from the subsequent analysis provided that either a) it is known that a substantial departure from prescribed experimental procedure has occurred, or b) a valid statistical criterion shows them to be outlying.

Because the program may exclude too many values from small data sets, a limit of 10 percent is imposed on the number of the values automatically excluded by this test. After 10 percent of the outliers have been removed, the operator is queried for the choice of retaining or discarding data that failed the outlier test.

#### 6.5.1 Rationale for the Test

It is reasonable to expect variability from one measurement to another for a given concentration because of a certain amount of imprecision in the measurement process. However, when a major discrepancy between measurements occurs, the extreme value is no longer representative of the regular measurement process and should be eliminated from the collaborative analysis. The judgment as to whether a given observed recovery is so disturbed is based on determining how far that result lies from the average of all measured results for that concentration. A two-sided T test is used to determine whether the measurement lies too far from the average and should be rejected.

### 6.5.2 Discussion of the Test

As mentioned above, the statistical procedure which is used in STATCALC for individual outlier testing is based on comparing each individual recovery to the average of all laboratories' recoveries at a given concentration level in a given matrix.

#### Individual Outlier Detection Procedure

Step 1 - The distance of each individual recovery from the overall average is compared to the average distance of all recoveries as measured by the overall (also called "total", or "multiple laboratory operational") standard deviation,  $s_t$ .

For a given concentration level, with L laboratories and one replicate (for Youden pairs, the test is done for each pair level), the average recovery is computed as

$$\bar{X} = \frac{\sum_{l=1}^L X_l}{L} \quad (\text{eq. 8})$$

and the overall standard deviation as

$$s_t = \sqrt{\frac{SS_t}{L-1}} \quad (\text{eq. 9})$$

where

$$SS_t = \sum_{l=1}^L X_l^2 - \frac{\left(\sum_{l=1}^L X_l\right)^2}{L} \quad (\text{eq. 10})$$

Step 2 - To run the test, the distance of the most extreme observation from the overall average is computed, and divided by the overall standard deviation. The test statistic is

$$T = \max_l \frac{|X_l - \bar{X}|}{s_t} \quad (\text{eq. 11})$$

and the value associated with this maximum is discarded if T exceeds the critical value of T for a given level of significance alpha, (Default:5%) and number of observations equal to the current number of retained data for the given concentration level and

matrix. Whenever such a rejection takes place, the pertinent information is recorded in \*.PRP.

Step 3 - The test is conducted in the same manner for each and every concentration level, until all the data have been examined. The results of the outlier testing procedure are reported in \*.PRP, in the outlier testing section of the file. After all checking has been accomplished, a file containing only nonrejected data is created (\*.DAF). This file represents the final data set. It is used in the performance evaluation section of the program where precision and bias are estimated and reported. In all there are four files created by STATCALC's data preparation phase:

*.PRP	Results of Data Preparation
*.DA~	Data Echo File for Audit Trail
*.DAF	Final Data for Analysis
*.PRF	Parameter File for Final Processing

### 6.5.3 Justification for the Procedure

The outlier detection method described above and employed in STATCALC is the standard in general use for such purposes. It is presented in ASTM Standard D2777-96, Section 10.4, (2) The procedure also appears in Grubbs (3), along with a general and informative discussion of the subject of statistical determination of outliers.

## 6.6 Testing for Normality

The test for individual outliers assumes that the underlying statistical population, that is, the population from which the observed measurements are drawn, follows a normal probability model. Much of the regression analysis performed later in the program also assumes normality (at least approximate) as well. The YODENPR subprogram checks this assumption for each set of data consisting of all nonrejected measurements of all labs within each analyte, matrix, concentration level. To check the assumption, one of two test procedures is used, depending on the sample size. If there are 50 or fewer observations remaining within an analyte, matrix, concentration level, the data are checked using the Shapiro-Wilk (W) test (4, 5). When more than 50 observations remain, D'Agostino's (D) test (6, 7) is used.

In both cases, the statistical procedure tests the null hypothesis that all data in the sample come from the same normally distributed population versus the alternative hypothesis that the population's probability distribution is not normal. While a decision not to reject the null hypothesis lends credence to the assumption that the underlying distribution is normal, it cannot be viewed as proof.

### 6.6.1 The Shapiro-Wilk (W) Test (Sample Size $\leq 50$ )

The theory used in the development of the Shapiro-Wilk test is complex, and the test statistic does not lend itself easily to intuitive interpretation. A complete technical discussion of the theory and development of the test is given in Shapiro and Wilk (4).

Discussion of the Test. The computation of the test statistic for the W test is accomplished in several stages.

Shapiro-Wilk Test Procedure -

Step 1 - First the number of observations to be tested is determined. There must be at least 3 observations in the data set in order for the test to be run.

Step 2 - Next, when N is 50 or less, the data for the analyte-matrix-concentration under analysis is sorted into ascending order using a Shell-Metzner sort routine. The "sum of squares" (sum of squared deviations from the mean) of the data set being tested is then computed from the formulas below. Let  $R_l, l=1,2,\dots,L$  be the number of retained values for the L laboratories, for the selected analyte-matrix-concentration level. Then renumber the observations

$$X_{(i)}, i = 1, 2, \dots, N \quad (\text{eq. 12})$$

where the use of parentheses (1), (2), ... indicates that the array has been sorted into ascending order (so that  $X_{(1)}$  is the smallest observation,  $X_{(2)}$  the second smallest, ...), and

$$N = \sum_{l=1}^L R_l \quad (\text{eq. 13})$$

The sum of squares,  $SS_{XX}$ , is, then,

$$SS_{XX} = \sum_{i=1}^N (X_{(i)} - \bar{X})^2 = \sum_{i=1}^N X_{(i)}^2 - \frac{\left( \sum_{i=1}^N X_{(i)} \right)^2}{N} \quad (\text{eq. 14})$$

Step 3 - Next the appropriate set of k coefficients,

$$a_1, a_2, \dots, a_k$$

are taken from Shapiro and Wilk (4), where

$$k = \begin{cases} \frac{N}{2} \\ \frac{N-1}{2} \end{cases} \quad (\text{eq. 15})$$

Step 4 - Then the test statistic, W, is computed from the above quantities,

$SS_{XX}$ ,  $a_1, a_2, \dots, a_k$ , and the ordered X values,  $X_{(1)}, X_{(2)}, \dots, X_{(N)}$

from the formula

$$W = \frac{1}{SS_{XX}} \left[ \sum_{i=1}^k a_i (X_{(N-i+1)} - X_{(i)}) \right]^2 \quad (\text{eq. 16})$$

Step 5 - The test is run at the 5% significance level. It rejects the normality assumption if the value of W is too small, that is, less than the critical value for N data points.

Step 6 - The results of the normality test ("A" = Accept normality, the data pass the test; "R" = Reject normality, the data do not pass the test.) are reported to the normality testing section of the \*.PRP output file.

Justification for the Procedure. The Shapiro-Wilk procedure is a standard method of testing for departures from normality. It is one of the most powerful methods available for such purposes. The original development work for the test was done by S. S. Shapiro and M B. Wilk, (4).

### 6.6.2 D'Agostino's (D) Test (Sample Size > 50)

For larger samples, when there are more than 50 data points involved, tables for the critical values of the Shapiro-Wilk statistic are not generally available. In that case, a test developed by R. B. D'Agostino (6, 7) is used. The program is currently restricted to no more than 500 data points for a single element-matrix-concentration level.

Discussion of the Test. The preliminaries in the calculation of D, the test statistic for D'Agostino's test, are similar to those for Shapiro-Wilk.

## D'Agostino's Test Procedure -

Step 1 - The data are sorted into ascending order as with the Shapiro-Wilk test.

Step 2 - Next the maximum likelihood estimate of the standard deviation,  $s$ , of the data set is computed from the formulas below. (Note: The "maximum likelihood estimate of the standard deviation" is similar to the "sample standard deviation", the difference being that where the latter divides by  $(N-1)$  the former divides by  $N$ .) Let  $R_l$ ,  $l = 1, 2, \dots, L$  be the number of retained results for the  $L$  laboratories, for the selected analyte-matrix-concentration level. Then renumber the observations, as with the Shapiro-Wilk test,

$$X_{(i)}, i = 1, 2, \dots, N \quad (\text{eq. 17})$$

where the use of parentheses (1), (2), ... indicates that the array has been sorted into ascending order (so that  $X_{(1)}$  is the smallest observation,  $X_{(2)}$  the second smallest, ...), and

$$N = \sum_{l=1}^L R_l \quad (\text{eq. 18})$$

As before, the sum of squares,  $SS_{xx}$ , is,

$$SS_{xx} = \sum_{i=1}^N (X_{(i)} - \bar{X})^2 \quad (\text{eq. 19})$$

$$SS_{xx} = \sum X_{(i)}^2 - \frac{(\sum X_i)^2}{N} \quad (\text{eq. 20})$$

Where  $\bar{X}$  is the sample mean

$$\bar{X} = \frac{\sum_{i=1}^N X_{(i)}}{N} \quad (\text{eq. 21})$$

The maximum likelihood estimate of the standard deviation is then,

$$s' = \sqrt{\frac{SS_{xx}}{N}} \quad (\text{eq. 22})$$

Step 3 - Next, D, the preliminary form of the test statistic is computed:

$$D = \frac{N \sum_{i=1} \left[ i - \frac{(N-1)}{2} \right] X_{(i)}}{N^2 s'} \quad (\text{eq. 23})$$

Step 4 - Then the actual test statistic, Y, is computed from the formula

$$Y = \frac{D - 0.28909479}{0.02998598 / \sqrt{N}} \quad (\text{eq. 24})$$

Step 5 - The test is run at the 5% significance level, it rejects the normality assumption if the value of Y is too small, i.e., less than the 2.5 percentage point, or if Y is too large, greater than the 97.5 percentage point.

Step 6 - The results of the normality test ("A" = accept normality, the data pass the normality test", "R" = Reject normality, the data do not pass the normality test.) are reported to the normality testing section of \*.PRP.

Justification for the Procedure. D'Agostino's development of the test for normality can be found in D'Agostino, (7).

## 6.7 Calculation of Analytical Method Performance Statistics

In the next step of the analysis, STATCALC calculates the sample summary statistics for precision, recovery, and bias as specified by D2777.

In addition, because they will be used in subsequent analyses, the program calculates bias-corrected, i.e., statistically unbiased, estimates of single operator and overall precision and includes these estimates in the output.

At this point in the analysis, the final data set consists of observations:

$$X_{cl}, = 1, 2, \dots, C; l = 1, 2, \dots, L \quad (\text{eq. 25})$$

where

$X_{cl}$  = measurement for the  $l^{\text{th}}$  laboratory, at the  $c^{\text{th}}$  concentration level

$L$  = the number of retained laboratories after lab ranking

$C$  = the number of concentration levels

$R_{cl}$  = the number of retained measurements for laboratory  $l$ , at level  $c$

These values are used in the calculations.

### 6.7.1 Calculation of Method Mean Recovery and Bias

Statistics are calculated for average recovery and bias.

Recovery. The mean recovery,  $\bar{X}_c$ , which is calculated for each concentration level, is found by averaging over the  $L$  sets of laboratory measurements at that level, i.e.,

$$\bar{X}_c = \frac{\sum_{l=1}^L X_{cl}}{N_{tc}} \quad (\text{eq. 26})$$

where

$$N_{tc} = \sum_{l=1}^L R_{cl} \quad (\text{eq. 27})$$

$N_{tc}$  is the total number of retained observations among the  $L$  laboratories at concentration level  $c$ . With Youden pairs,  $R_{cl}$  is either 0 or 1. The notation "tc" is used here to be consistent with later notation requirements.

True Concentration. To calculate the true concentrations, the program accumulates the incremental spikes,  $\Delta T_c$ ,  $c = 1, 2, \dots, C$ , given in the \*.PRF file.

The value of the true concentration,  $T_c$ , for level  $c$  is given by

$$T_c = \sum_{i=1}^C \Delta T_i \quad (\text{eq. 28})$$

Bias. The sample bias,  $B_c$ , for concentration level  $c$  is defined as the difference between the true concentration and the mean recovery (D2777), i.e.,

$$B_c = (\bar{X}_c - T_c) \quad (\text{eq. 29})$$



The relative bias is then given by

$$(Relative\ Bias)_c = \frac{(\bar{X}_c - T_c)}{T_c} \times 100\% \quad (\text{eq. 30})$$

$$(Relative\ Bias)_c = \frac{B_c}{T_c} \times 100\% \quad (\text{eq. 31})$$

### 6.7.2 Calculation of Method Precision Statistics (Standard Deviations)

STATCALC computes estimates of the parameters of regression relating operator precision ( $s_o$ ), overall precision ( $s_t$ ), and method recovery (result), ( $X$ ) to true concentration, ( $T$ ). These regressions are:

Single Operator Precision regressions:

$$s_o = b_o T + a_o \quad (\text{eq. 32})$$

Overall Precision regressions:

$$s_t = b_t T + a_t \quad (\text{eq. 33})$$

Recovery regressions:

$$X = b_x T + a_x \quad (\text{eq. 34})$$

Single Operator Precision with Youden Pairs. The objective of the Youden pair design is to produce within laboratory measurements which are free from the analyst's tendency to make known replicates match. By selecting two concentrations that are nearly, but not exactly the same, and observing the difference between the uncorrelated measurements at the two concentration levels, the variance of this difference should be twice the variance of the individual measurements, i.e. twice the single operator precision which the analyst is attempting to estimate. If one assumes that single operator precision is equal for all laboratories, then the information (differences) for the several laboratories may be pooled to give a single operator precision estimate for each pair of observations.

Observations for the  $l^{\text{th}}$  laboratory (in a given data set, i.e., a given matrix/analyte combination) for the  $P$  pairs are

$$X_{lp1}, X_{lp2}; \quad p = 1, \dots, P \quad (\text{eq. 35})$$

and the differences between the observations within pairs are

$$D_{lp} = (X_{lp1} - X_{lp2}); \quad p = 1, \dots, P \quad (\text{eq. 36})$$

The estimate of the variance of  $D_{lp}$  is

$$\hat{s}_p^2 = \frac{\sum_{l=1}^{L_p} (D_{lp} - \bar{D}_p)^2}{(L_p - 1)} \quad (\text{eq. 37})$$

where

$$\bar{D}_p = \frac{\left( \sum_{l=1}^{L_p} D_{lp} \right)}{L_p} \quad (\text{eq. 38})$$

and  $L_p$  is the number of retained laboratories with both observations present (i.e. no outliers or missing values) for concentrations of pair  $p$ .  $D_{lp}$  is the difference between two observations, its variance is twice the single operator variance (assuming that the two observations in the pair are independent) so that the estimate of the single operator standard deviation for the  $p^{\text{th}}$  pair is

$$s_{op} = \sqrt{\frac{\sum_{l=1}^{L_p} (D_{lp} - \bar{D}_p)^2}{2(L_p - 1)}} \quad (\text{eq. 39})$$

**Overall (Total) Precision for Youden Pairs.** Overall precision ( $S_{tc}$ ) represents the total combined variability, i.e., both within and between laboratories. Let  $N_{tc}$  be the total number of retained observations among the  $L$  laboratories at concentration level  $c$ . Then

$$s_{tc} = \sqrt{\frac{\sum_{l=1}^{N_{tc}} (X_{cl} - \bar{X}_c)^2}{N_{tc} - 1}} \quad (\text{eq. 40})$$

Weights for the Precision Regressions. The STATCALC program uses explicitly weighted linear regression techniques which incorporate weights based upon 1) the number of retained data at a given concentration level and 2) the change in precision with concentration. The selected weights compensate for changing precision and rejected data to give approximately constant variances for the dependent variable at each concentration. The weights also compensate for "statistical bias" in the sample standard deviation,  $s$ , as an estimate of the true standard deviation.

Bias Factor (bf). Although a sample variance,  $s^2$ , is statistically unbiased for a true "population" single operator variance,  $s^2$ , its square root,  $s$ , is well known to be biased for  $s$  and can be corrected for bias with a multiplicative constant dependent upon sample size. To correct for this bias, each  $s$  is multiplied by a bias factor to give corrected estimates,  $s^*$ , of true precision,

$$s^* = (bf) \cdot s \quad (\text{eq. 41})$$

where

$$bf = \frac{1}{c_4} \quad (\text{eq. 42})$$

and

$$C_4 = \frac{\sqrt{\frac{2}{n}} \left( \frac{n-1}{2} \right)!}{\left( \frac{n-1}{2} \right)!} \quad (\text{eq. 43})$$

where  $n$  is the number of degrees of freedom with which the sample standard deviation is computed.

Standard Error Factor (sef). In addition, the standard error of the sample standard deviation,  $s$ , at a given concentration level,  $T$ , is also a function of the constant  $c_4$ .

$$s_{s|T} = \sqrt{1 - c_4^2} \cdot s_{X|T} \quad (\text{eq. 44})$$

so that the standard error of  $s^*$  is

$$s_{s^*|T} = s_{(bf) \cdot s|T} \quad (\text{eq. 45})$$

$$= (bf) \cdot \sqrt{1 - c_4^2} \cdot s_{x|T} \quad (\text{eq. 46})$$

$$= (bf) \cdot (sef) \cdot s_{x|T} \quad (\text{eq. 47})$$

which is a function of sample size and the true value of  $s_{x|T}$ .

Need for Weights. Since regression analysis requires homogeneity of variances for the dependent variable, weighted least squares estimates must be used to fit the regression model to the values of  $s$ . The weights used must be proportional to the variances of the  $s$  values for the different concentration levels. The appropriate weights are

$$w = \frac{1}{(bf)^2 \cdot (sef)^2 \cdot s_{x|T}^2} \quad (\text{eq. 48})$$

The true value of  $s_{x|T}^2$  is not known, however, so it must be estimated.

Preliminary Weights. There is a practical difficulty here since the values of  $b$  and  $a$  are not determined until the regression line has been fit, yet their values are needed to determine weights used to fit the regression line. To overcome this difficulty, an initial rough estimate of the precision regression line is obtained by assuming that the true values of  $s_{x|T}^2$  are constant, for which appropriate weights would be

$$w = \frac{1}{(bf)^2 \cdot (sef)^2} \quad (\text{eq. 49})$$

and weighted linear regression with these weights gives initial estimates,  $b_{init}$  and  $a_{init}$ , of the slope and intercept, respectively, of the regression of  $s^*$  on  $T$ .

$$s^* = b_{init} T + a_{init} \quad (\text{eq. 50})$$

Preliminary estimates of the method variance at each concentration level are now calculated using the values of  $b_{init}$  and  $a_{init}$ , above. This calculation gives approximate weights

$$w = \frac{1}{(bf)^2 \cdot (sef)^2 \cdot (b_{init} T + a_{init})^2} \quad (\text{eq. 51})$$

which are then normalized, i.e. they are divided by their sum to give normalized weights,  $w_c$

$$w_c \rightarrow \frac{w_c}{\sum_{c=1}^C w_c} \quad (\text{eq. 52})$$

As before, the bias and standard error factors are determined for the number of degrees of freedom with which the standard deviation is computed.

Refined estimates of the precision regression equation are now obtained using the preliminary weights above to perform a second weighted linear regression for the precision model using the weighted regression formulas in the next section with  $Y = s^*$ ,  $X = T$  to give

$$\hat{s}^* = bT + a \quad (\text{eq. 53})$$

Weighted Linear Regression Formulas. The formulas for computing weighted least squares regression estimates are similar to those for unweighted least squares. Suppose one has  $C$  observations on variables  $U$  (dependent) and  $V$  (independent), i.e.,

$$(V_c, U_c); \quad c = 1, 2, \dots, C \quad (\text{eq. 54})$$

Then the weighted least squares estimates, given normalized weights

$$w_c; \quad c = 1, 2, \dots, C \quad \left( \sum w_c = 1.0 \right) \quad (\text{eq. 55})$$

and letting

$$WSS_{VU} = \sum w(V - \bar{V})(U - \bar{U}) = \sum wUV - \left( \sum wV \right) \left( \sum wU \right) \quad (\text{eq. 56})$$

$$WSS_{VV} = \sum w(V - \bar{V})^2 = \sum wV^2 - \left( \sum wV \right)^2 \quad (\text{eq. 57})$$

are

$$b = \frac{WSS_{VU}}{WSS_{VV}} \quad (\text{eq. 58})$$

and

$$a = \bar{U} - b\bar{V} \quad (\text{eq. 59})$$

where

$$\bar{V} = \sum wV \quad (\text{eq. 60})$$

and

$$\bar{U} = \sum wU \quad (\text{eq. 61})$$

and all sums are taken from 1 to C.

Precision Estimates by Weighted Curvilinear Regression. The STATCALC program uses essentially the same techniques described for the linear models described above to fit a curvilinear regression mode. To accomplish the curvilinear fit, the logarithms of the precisions are used, rather than the precisions themselves. The logarithmic form of the curvilinear precision equation is

$$\ln \hat{s}^* = bT + a \quad (\text{eq. 62})$$

After the fitting is done, the logarithmic model is converted back so that it is expressed in the original (nonlogarithmic) units. Use of the curvilinear model assumes that operator precision changes at a constant relative rate.

The nonlogarithmic form of the model is

$$\hat{s}^* = a'(b')^T \quad (\text{eq. 63})$$

where

$$b' = e^b \quad (\text{eq. 64})$$

and

$$a' = e^a \quad (\text{eq. 65})$$

General. For the curvilinear single operator regressions, the dependent variable is the logarithm of the bias corrected precision, i.e.,

$$\ln \hat{s}_{oc}^*; \quad c = 1, 2, \dots, C \quad (\text{eq. 66})$$

and the true concentration is the independent variables, i.e.,

$$T_c; \quad c = 1, 2, \dots, C \quad (\text{eq. 67})$$

Weighted linear regression is used, but, since the standard deviation of  $s^*$  is proportional to the standard deviation of  $\sigma_{X|T}$ , the logarithmic transformation stabilizes the variance. The regression weights depend only on the number of retained data. In general, they are

$$w = \frac{1}{(bf)^2 \cdot (sef)^2} \quad (\text{eq. 68})$$

Recovery Estimates by Weighted Linear Regression. Recoveries are the measured amounts,  $X$ , reported by the laboratories. In fitting the regression models, it is assumed that, at a given concentration, the expected recovery is the same for all laboratories. STATCALC estimates the parameters of a linear model which relates recovery to true concentration.

$$\hat{X} = bT + a \quad (\text{eq. 69})$$

For estimating the recovery regression equation, STATCALC uses weighted regression techniques for the same reasons already discussed for precision regression, that is, to compensate for decreasing precision and rejected data to give approximately constant standard errors for recovery at each concentration.

The recovery regressions are performed with recovery as the dependent variable and true concentration as the independent variable. The actual calculations are performed on the  $C$  mean recovery-true concentration pairs, i.e.,

$$(T_c, \bar{X}_c); \quad c = 1, 2, \dots, C \quad (\text{eq. 70})$$

Weighted linear regression is used with (normalized) weights

$$w_c; \quad c = 1, 2, \dots, C \quad (\text{eq. 71})$$

Calculation of these weights differ from those for precision. To achieve the required homogeneity of variances the weights used must be proportional to the variances of the X values for the different concentration levels. The appropriate weights are

$$w = \frac{1}{N_T \cdot s_{X|T}^2} \quad (\text{eq. 72})$$

where  $N_T$  is the total number of retained observations from which the mean recovery is computed and  $\sigma_{X|T}^2$  is the true overall precision. The true value of  $\sigma_{X|T}^2$  is not known, however, so it must be estimated using  $\hat{s}_T^*$  from the previous precision regression analysis.

The weights are

$$w_c = \frac{N_c}{\hat{s}_c^*} \quad (\text{eq. 73})$$

where  $\hat{s}_c^*$  is the appropriate regression equation evaluated at  $T_c$ .

Weighted least squares with  $U = \bar{X}$ ,  $V = T$  is used to obtain the recovery regression equation.

Precision Versus Recovery. A regression relationship between precision and recovery may be obtained by substituting the recovery regression results into the precision regression formulas.

Linear Models. The formulas output by the program for linear precision and linear recovery versus true concentration are:

- Single Operator Precision

$$\hat{s}_o^* = b_o T + a_o \quad (\text{eq. 74})$$

- Overall Precision

$$\hat{s}_t^* = b_t T + a_t \quad (\text{eq. 75})$$

- Recovery

$$\hat{X} = b_X T + a_X \quad (\text{eq. 76})$$



Solving for T in the recovery equation gives

$$T = \frac{(\hat{X} - a_x)}{b_x} \quad (\text{eq. 77})$$

which is substituted into the precision equations to obtain

$$\hat{s}^* = a_o + b_o \frac{(\hat{X} - a_x)}{b_x} \quad (\text{eq. 78})$$

$$= \left( a_o - \frac{a_x}{b_x} \right) + \frac{b_o}{b_x} \hat{X} \quad (\text{eq. 79})$$

$$= e_o + f_o \hat{X} \quad (\text{eq. 80})$$

where

$$e_o = a_o - \frac{a_x}{b_x} \quad (\text{eq. 81})$$

$$f_o = \frac{b_o}{b_x} \quad (\text{eq. 82})$$

In a like manner, for the overall precision,

$$\hat{s}_t^* = e_t + f_t \hat{X} \quad (\text{eq. 83})$$

where

$$e_t = a_t - \frac{a_x}{b_x} \quad (\text{eq. 84})$$

$$f_t = \frac{b_t}{b_x} \quad (\text{eq. 85})$$

Curvilinear Models. The formulas output by the program for curvilinear precision and linear recovery versus true concentration are:

- Single Operator Precision

$$\hat{s}_o^* = a_o(b_o)^T \quad (\text{eq. 86})$$

- Overall Precision

$$\hat{s}_t^* = a_t(b_t)^T \quad (\text{eq. 87})$$

- Recovery

$$\hat{X} = b_X T + a_X \quad (\text{eq. 88})$$

Solving for T in the recovery equation gives

$$T = \frac{(\hat{X} - a_X)}{b_X} \quad (\text{eq. 89})$$

which is substituted into the single operator precision equation to obtain

$$\hat{s}_o^* = a_o(b_o)^{\frac{(\hat{X} - a_X)}{b_X}} \quad (\text{eq. 90})$$

$$\hat{s}_o^* = a_o(b_o)^{\left(-\frac{a_X}{b_X}\right)} (b_o)^{\left(\frac{\hat{X}}{b_X}\right)} \quad (\text{eq. 91})$$

$$\hat{s}_o^* = e_o(f_o)^{\hat{X}} \quad (\text{eq. 92})$$

where

$$e_o = a_o(b_o)^{\left(-\frac{a_X}{b_X}\right)} (b_o)^{\left(\frac{\hat{X}}{b_X}\right)} \quad (\text{eq. 93})$$

$$f_o = (b_o)^{(1/b_x)} \quad (\text{eq. 94})$$

In a like manner for the overall precision,

$$\hat{s}_t^* = e_t(f_t)^{\hat{x}} \quad (\text{eq. 95})$$

## 6.8 Testing for Significant Bias

The program next performs the necessary calculations and tests to determine whether the observed bias values for each level are statistically significant.

### 6.8.1 General

The statistical procedure tests the null hypothesis that the true method bias at each concentration is zero, versus the alternative that it is nonzero, assuming the underlying distribution is normal. While a decision not to reject the null hypothesis is not proof that the method bias is zero, it lends credence to such a conclusion.

### 6.8.2 Rationale for the Procedure

If there is no method bias for a given level of concentration, then one would expect that the true and measured amounts of analyte should be the same, on average. A Student's t test procedure is used to judge, as prescribed by ASTM D2777, whether the bias (difference between true and average measured concentrations) for the sample data at each concentration level is within the realm of acceptable variability, taking overall method precision into account. First, the program adjusts the overall precision (standard deviation) to reflect the number of observations over which recovery was averaged at the given concentration level. The adjusted value is called the standard deviation of the mean. Then, the program calculates the number of standard deviations (of the mean) by which the true and average recovered values differ. Finally, this latter figure is tested for acceptability under Student's t distribution.

### 6.8.3 Outline of the Calculations

The basic steps in the calculations at each concentration level are given below.

Student's t Test for Bias -

Step 1 - Calculate the bias:

$$B_c = \bar{X}_c - T_c \quad (\text{eq. 96})$$

Step 2 - Calculate the standard deviation of the mean (recovery):

$$s_{\bar{X}} = \frac{s_{tc}}{\sqrt{N_{tc}}} \quad (\text{eq. 97})$$

When the average of the Level 1 concentration recoveries is used as the true background concentration, an adjustment must be made in this calculation. The bias is then identically 0.0 for level 1 and for c greater than 1 it is

$$\bar{X}_c - T_c = \bar{X}_c - \bar{X}_1 - \sum_{i=2}^c \Delta T_i \quad (\text{eq. 98})$$

for which the standard deviation is estimated as

$$s_{\bar{X}_c - \bar{X}_1} = \sqrt{\frac{s_{tc}^2}{N_{tc}} + \frac{s_{t1}^2}{N_{t1}}} \quad (\text{eq. 99})$$

Step 3 - Calculate the observed t-value:

$$t_c = \frac{|\bar{X}_c - T_c|}{\frac{s_{tc}}{\sqrt{N_{tc}}}} \quad (\text{eq. 100})$$

Step 4 - Determine the critical value,  $t_{.005}$ , for a 1% (two-tailed) significance level for Student's t test with  $N_{tc} - 1$  degrees of freedom, and compare t from Step 3 to the critical value. The null hypothesis is rejected (concluding there is significant bias) if

$$t_c > t_{.005} \quad (\text{eq. 101})$$

Step 5 - The results of the bias testing ("Yes" = "Yes, the bias is significant." or "No" = "No, the bias is not significant.") are reported to \*.STT.

## 6.9 Use of STATCALC Output

The STATCALC output files, particularly the data preparation files (\*.PRP) and statistical processing files (\*.STT) provide all of the information necessary for the user to

compile the tables and graphs required in ASTM D2777. Copies of the data, data preparation and statistical processing files for all of the AMQ-IV Round 2 data are contained in Appendix H. The precision and recovery regression equations are used to calculate the  $L_{ci}$  and AML discussed in Section 8. Section 9 contains the values calculated from the AMQ-IV Round 2 data.

## 6.10 References

1. American Society for Testing and Materials, "Standard Practice for Determination of Precision and Bias of Applicable Methods of Committee D-19 on Water", D2777-86, *Annual Book of ASTM Standards*, 1996.
2. American Society for Testing and Materials, "Standard Practice for Determination of Precision and Bias of Applicable Methods of Committee D-19 on Water", D2777-96, *Annual Book of ASTM Standards*, 1997.
3. F.E. Grubbs, "Procedures for Detecting Outlying Observations in Samples", *Technometrics*, 2, No. 1, February, 1969.
4. S.S. Shapiro and M. B. Wilk, "An Analysis of Variance Test for Normality", *Biometrika*, Vol 52, 1965, pp. 519-611.
5. S.S. Shapiro, M.B. Wilk and H.J. Chen, "A Comparative Study of Various Tests of Normality", *Journal of the American Statistical Association*, 63, 324, December 1968, pp. 1343-1372.
6. R.B. D'Agostino, "An Omnibus Test of Normality for Moderate and Large Samples", *Biometrika*, 58, 1971, pp. 341-348.
7. R.B. D'Agostino, "Small Sample Probability Points for the D Test of Normality", *Biometrika*, 59, 1972, pp. 219-221.



# 7

## DATA EVALUATION

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The AMQ-IV Round 2 validation effort was part of a comprehensive data collection and evaluation effort to provide a complete profile of the personnel, procedures, and methods used by utility laboratories for trace metal analysis. This section discusses the operation procedures employed by the participants and presents the results of the validation effort. The validation results are discussed by element and matrix.

### 7.1 Operating Data

During the AMQ-IV Round 2 test program, all the participants were sent a questionnaire concerning:

- Operator experience
- Analytical instrumentation
- Laboratory standards and sample handling
- Sample preparation and analysis

A copy of that form with highlights of the AMQ-IV Round 2 results from the eighteen participating laboratories summarized can be found in Appendix E.

From these documents, a profile of the personnel and procedures employed on the AMQ-IV Round 2 validation effort was constructed.

#### 7.1.1 Personnel Experience Levels

Figure 7-1 shows the percentage of respondents having a given number of years of GFAAS experience. Thirty-eight percent had 1 to 5 years of GFAAS experience, twenty-eight percent had between 5 and 10 years of GFAAS experience and twenty-two percent had more than 10 years GFAAS experience. Only twelve percent of the operators had less than 1 year of GFAAS experience. Sixty percent of the analysts had attended GFAAS training classes for the specific instrument they used in AMQ-IV Round 2.

Figure 7-2 illustrates the education level of the analysts and supervisors. Seventy-two percent of the analysts had a BA/BS degree in chemistry, biology or a related field of study. One analyst had a MA/MS degree in chemistry. Eighty-nine percent of the supervisors had BA/BS degrees, 63% in chemistry with the remainder in biology,

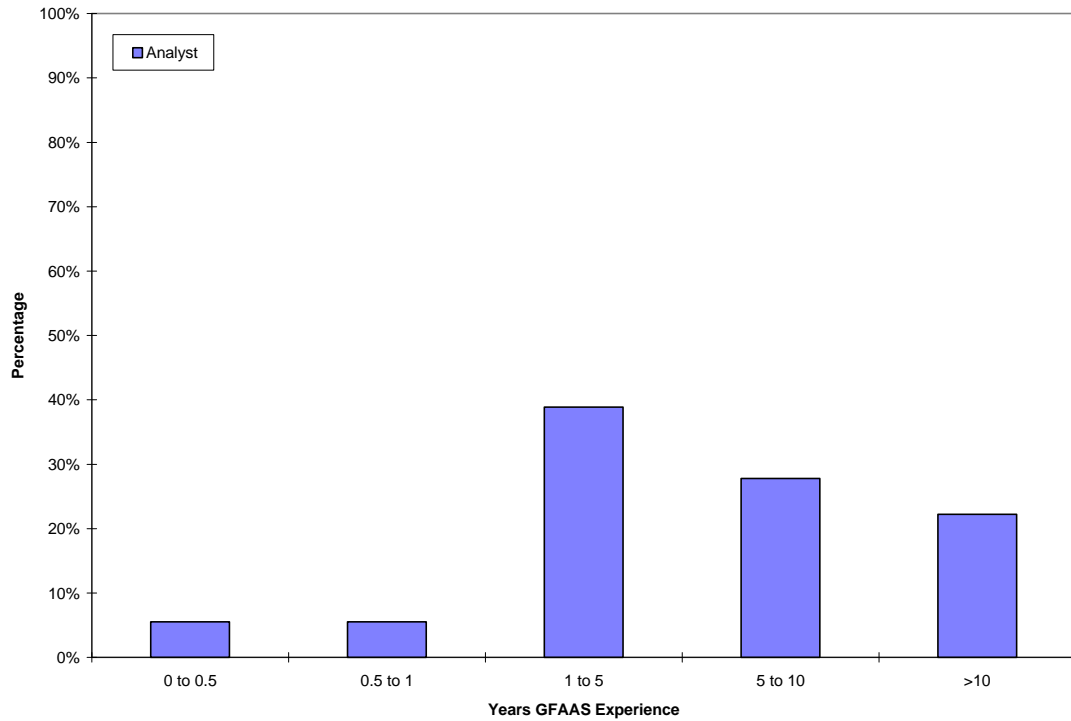


Figure 7-1 Operator GFAAS Experience

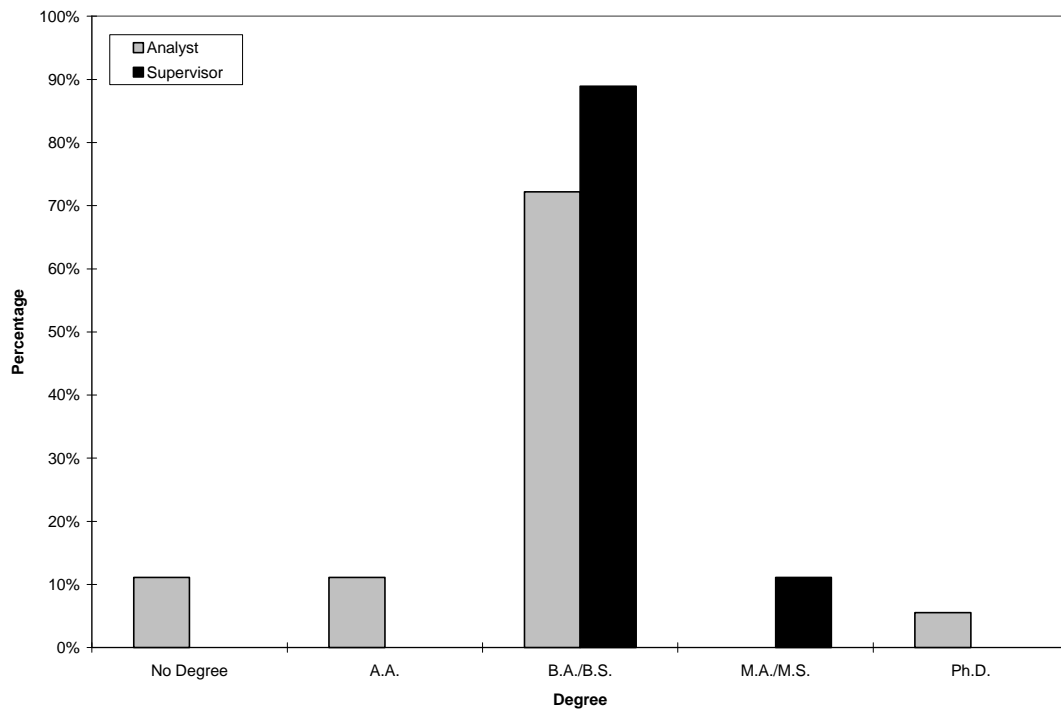


Figure 7-2 Comparison of Education: Analyst and Supervisor



biochemistry, microbiology, and environmental science. Eleven percent of the supervisors had MA/MS degrees in chemistry. Seventy-seven percent of the supervisors had more than 10 years experience. Only 11% had fewer than 5 years experience.

### 7.1.2 Analytical Instrumentation

Twenty-two instruments were used by the eighteen laboratories participating in AMQ-IV Round 2. Ninety percent employed autosamplers for sample introduction. The majority of the laboratories performed data reduction by comparison to a linear (52%) or non-linear (24%) calibration curve. One laboratory reported they used a least squares program for data analysis, two used a quadratic function, and one used "best fit".

Seventy-two percent of the laboratories analyzed all analytes using platform graphite furnace. Eleven percent of the laboratories used tube graphite furnace for all analytes. Seventeen percent used tube graphite furnace for some analytes and platform graphite furnace for others. Figure 7-3 illustrates the type of graphite furnace used by the participants.

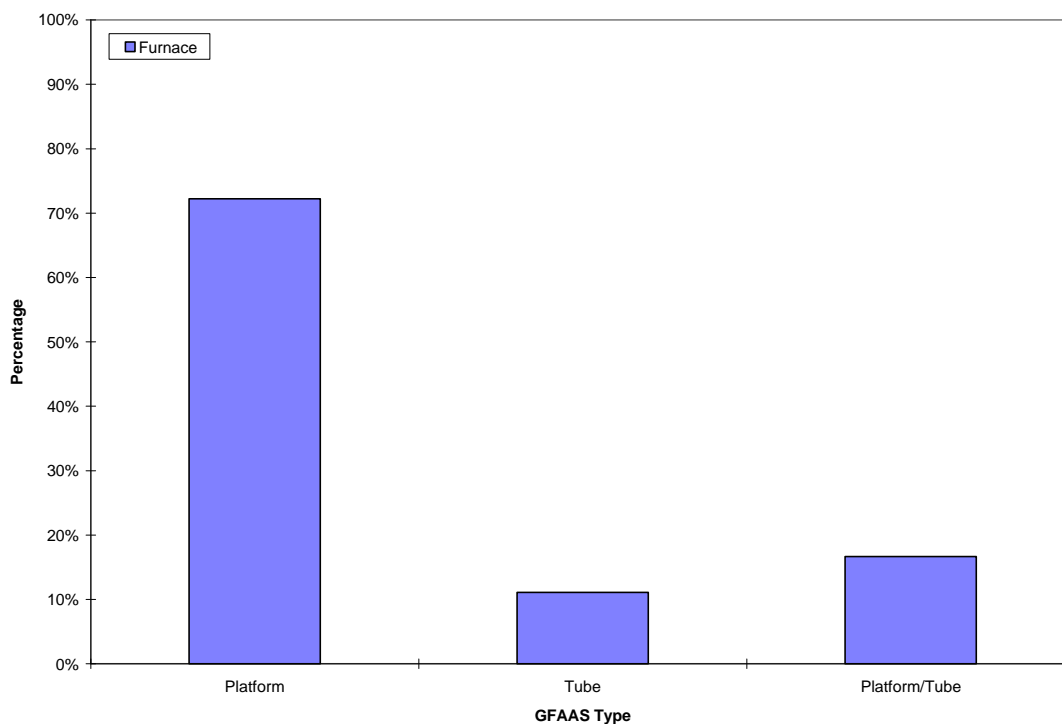


Figure 7-3 Comparison of Type of Graphite Furnace Used in AMQ-IV Round 2

### **7.1.3 Laboratory Standards and Sample Handling**

All of the participants used commercially prepared standard reference materials for calibration.

### **7.1.4 Sample Preparation and Analysis**

Only one laboratory noted the presence of precipitates in any of the sample aliquots after digestion and redilution. The laboratory observed precipitates in some of the estuarine and acid mine drainage samples. The samples were allowed to settle and the supernatant was used. Another laboratory noted that they vacuum filtered samples in the study, although they did not indicate that they had observed any precipitates.

One-third of the analysts added matrix modifiers other than those listed in the test procedure during sample analysis. These included magnesium nitrate, palladium/magnesium nitrate, and ammonium phosphate.

## **7.2 Raw Data Analysis**

As noted in Section 6, the results from each laboratory were input to a dBase III® data base from the AMQ-IV Round 2 reporting forms. Once the data were proofed for typographical errors, the appropriate ASCII files were generated for use by the STATCALC statistical program.

The following sections discuss the make-up of the data before and after processing.

### **7.2.1 Raw Data**

A complete printout of the raw data by element is contained in Appendix G. The data were sorted by element, laboratory, matrix, and concentration level.

### **7.2.2 Outlier Removal Results**

The AMQ statistical program, STATCALC, performs the two outlier removal activities described in ASTM D2777 (1): lab ranking and individual outlier removal. These are described in detail in Section 6. When a lab is ranked out, all of its data are removed for a particular element and matrix. Up to 20% of the laboratories may be removed by lab ranking.

The individual outlier test is performed on the remaining data by element, matrix and concentration level. A maximum of 10% of the data points may be removed by element, matrix and concentration level. For small data sets with fewer than 10

laboratories surviving the lab ranking test, a maximum of one outlier data point per concentration level may be removed.

Table 7-1 summarizes the total number of data points (summed over all concentration levels) remaining after outlier removal activities. The largest percentage of outliers was removed by the laboratory ranking test. Only a small percentage was removed by the outlier procedure.

**Table 7-1**  
**Data Points Remaining after Outlier Removal**  
 (Percentages based on Total Data Points Received)

Element	Matrix	Points as Received	After Lab Ranking		After 1% t-Test	
			Points	%	Points	%
As	RGW	136	112	82.4	110	80.9
As	GW	170	140	82.4	134	78.8
As	EST	150	120	80.0	115	76.7
As	AMD	160	150	93.8	143	89.4
Cd	RGW	170	140	82.4	133	78.2
Cd	GW	170	140	82.4	136	80.0
Cd	EST	140	120	85.7	118	84.3
Cd	AMD	160	130	81.3	129	80.6
Cr	RGW	170	160	94.1	153	90.0
Cr	GW	170	150	88.2	145	85.3
Cr	EST	140	120	85.7	118	84.3
Cr	AMD	170	140	82.4	137	80.6

RGW = Reagent Grade Water

GW = Groundwater

EST = Estuarine

AMD = Acid Mine Drainage

### 7.2.3 Normality Testing

The statistical program, STATCALC, tested each of the data sets for normality using either the Shapiro/Wilk (sample size <50) or D'Agostino's (sample size > 50) normality test. These tests are discussed in detail in Section 6. The test for individual outliers and much of the regression analysis assumes at least approximate normality. The results of the normality tests are either A (accept normality, the data passes the normality test) or R (reject normality, the data does not pass the normality test). Table 7-2 summarizes the results of the normality tests. A total of 96 of the 118 data sets tested normal (81%).

**Table 7-2**  
**Data Distribution after Outlier Removal**

Element	Matrix	B1	B2	1	2	3	4	5	6	7	8
As	RGW	-	-	A	R	A	A	A	A	A	A
As	GW	A	A	A	A	R	A	A	A	A	A
As	EST	A	A	A	A	A	A	A	A	A	A
As	AMD	R	R	A	A	A	R	A	A	A	A
Cd	RGW	A	A	A	R	A	A	R	R	A	A
Cd	GW	A	R	A	R	A	R	A	A	R	A
Cd	EST	R	R	R	A	R	A	A	A	A	A
Cd	AMD	A	A	A	A	A	A	A	A	A	A
Cr	RGW	A	A	A	A	A	R	R	A	R	A
Cr	GW	R	A	R	A	A	A	A	A	A	A
Cr	EST	A	R	A	A	A	A	A	A	A	A
Cr	AMD	A	A	A	A	A	A	A	A	A	A

RGW = Reagent Grade Water

GW = Groundwater

EST = Estuarine

AMD = Acid Mine Drainage

### 7.3 Reduced AMQ-IV Round 2 Data

The results of the statistical analysis of the AMQ-IV Round 2 data are contained in Appendix H. For each element, sorted by matrix, the following tables are present:

- Data File (.DAT) - Displays original raw data submitted by each laboratory.
- Data Validation File (.DA~) - Audit record documenting the fate of each original data point. Includes information on values removed by lab ranking and outlier testing.
- Final Data File (.DAF) - Final data set submitted for statistical processing after removal of outliers.
- Data Preparation File (.PRP) - Displays the results of the factor of 5 screening, laboratory ranking, individual outlier removal, and normality testing.
- Summary Statistics (.STT) - Contains recovery, single operator standard deviation, and overall standard deviation results at each concentration; results of bias testing; linear and curvilinear equations for single operator and overall standard deviation; linear regression equations for recovery; and linear regression equations for both single operator and overall standard deviation versus recovery (obtained by substitution).

These data were summarized and plotted for each element. The following plots are presented and discussed by element in this section:

- Single operator standard deviation versus true concentration (true concentration equals the mean of the lowest concentration plus the added spikes)
- Overall standard deviation versus true concentration
- Single operator relative standard deviation versus mean concentration
- Overall relative standard deviation versus mean concentration
- Mean result versus true concentration for all matrices. The 100% recovery line is plotted along with  $\pm 10\%$  lines.
- Mean result versus true concentration for each matrix. The linear regression through the data is plotted to illustrate linearity of the recovery.

#### 7.3.1 Arsenic

The reduced data for arsenic are found in Appendix H.

Arsenic Standard Deviation. Figure 7-4 and 7-5 show the single operator and overall standard deviation data for arsenic. A Rocke-Lorenzato curve fit (see Section 8.3) across the concentration range analyzed is plotted for all data sets except the overall data for groundwater, which was best fit with an exponential curve. The low TDS matrices,

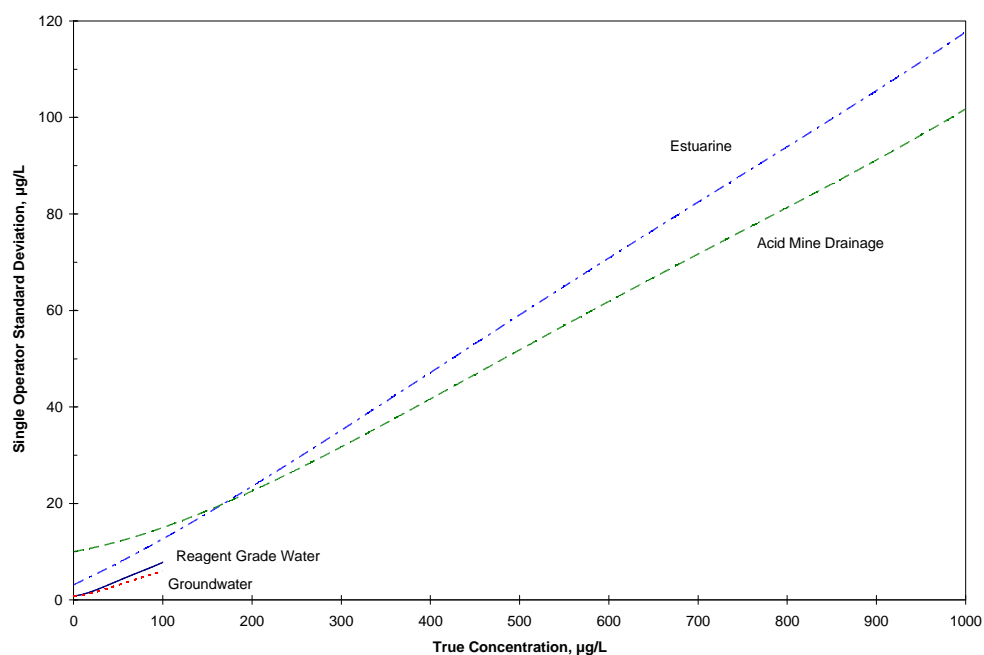


Figure 7-4 Plot of the single operator standard deviation versus the true concentration for arsenic by GFAAS

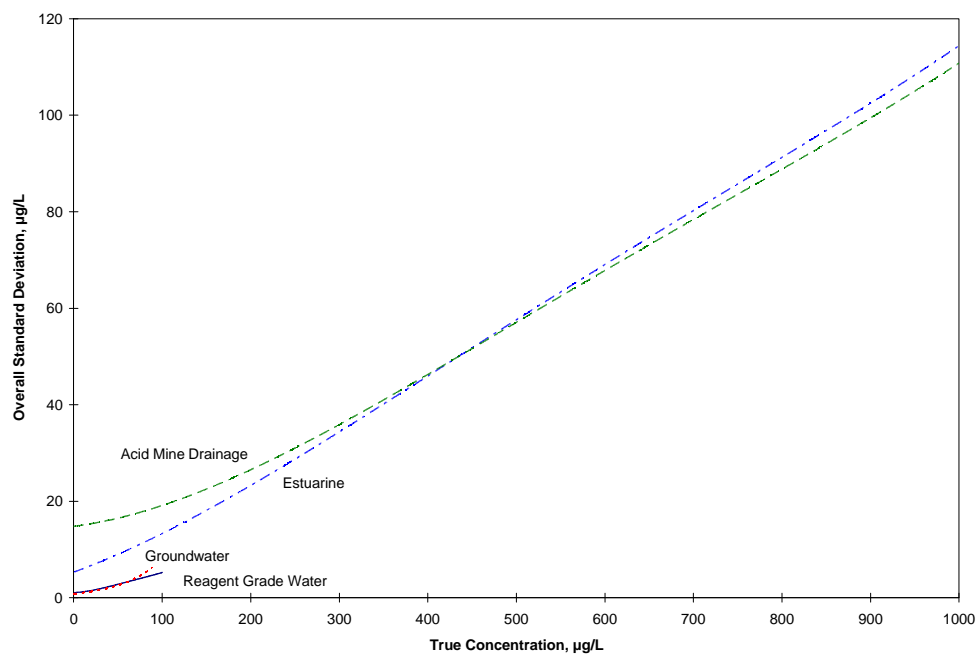


Figure 7-5 Plot of the overall standard deviation versus the true concentration for arsenic by GFAAS

reagent grade water and groundwater, exhibited similar trends in absolute standard deviation versus concentration. The high TDS matrices, estuarine and acid mine drainage, had higher standard deviations. The acid mine drainage matrix had the highest single operator standard deviation at low concentrations, but the estuarine matrix had the highest standard deviation above about 180 µg/L arsenic. The same pattern was observed in the overall standard deviation plot, with the crossover concentration at approximately 450 µg/L arsenic.

Figures 7-6 and 7-7 plot the single operator and overall relative standard deviation (RSD) against mean concentration for arsenic in all matrices. Note the log/log scale. As expected, the highest RSDs were obtained at the lowest concentrations. Single operator RSDs leveled off to generally less than 15% as concentration increased. Overall RSDs tended to be higher, particularly for the estuarine and acid mine drainage samples. For all matrices, overall RSDs were generally less than 20% at the higher concentrations.

Arsenic Recovery. The recovery data (mean result versus true concentration) for arsenic in all matrices are shown in Figure 7-8. The 100% recovery (solid line) and  $\pm 10\%$  recoveries (dotted line) are shown for reference. By definition, recovery for the lowest concentration is 100% (reported mean = lowest true concentration). Recoveries for all matrices were within  $\pm 10\%$ . Plots of the individual recoveries by matrix are found in Figures 7-9 through 7-12. The weighted linear regression through the data is shown. Arsenic recoveries were quite good for all matrices and concentrations.

### 7.3.2 Cadmium

The reduced data for cadmium are found in Appendix H.

Cadmium Standard Deviation. The single operator and overall standard deviation plots for cadmium are found in Figures 7-13 and 7-14. Reagent grade water exhibited the lowest absolute standard deviation across the concentration range studied. The standard deviation for groundwater was similar to that of reagent grade water at lower concentrations, but trended upward at higher concentrations. Single operator standard deviations for the estuarine and acid mine drainage samples were similar at the lowest concentrations, but estuarine standard deviations trended higher at higher concentrations. The overall standard deviation for the estuarine samples was lower than that of acid mine drainage at low concentrations, but was higher for estuarine samples above about 15 µg/L.

Single operator and overall RSDs for cadmium are shown in Figures 7-15 and 7-16. RSDs generally trended lower at higher concentrations. The overall RSDs exhibited a clustering of data at the higher concentrations with estuarine having the highest RSDs, followed by acid mine drainage, groundwater and then reagent grade water.

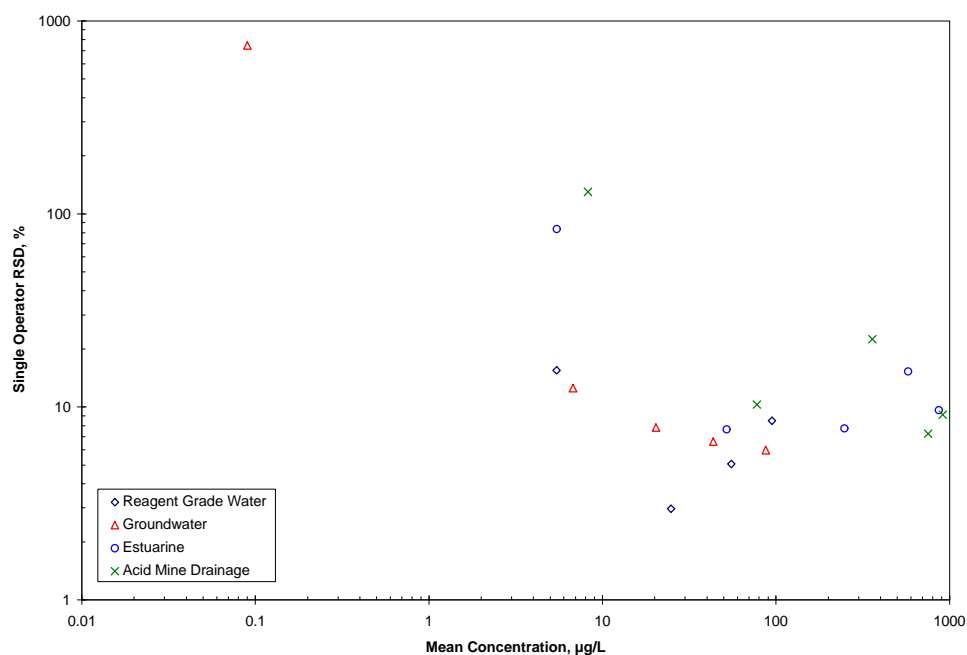


Figure 7-6 Plot of the single operator relative standard deviation versus the mean concentration for arsenic by GFAAS

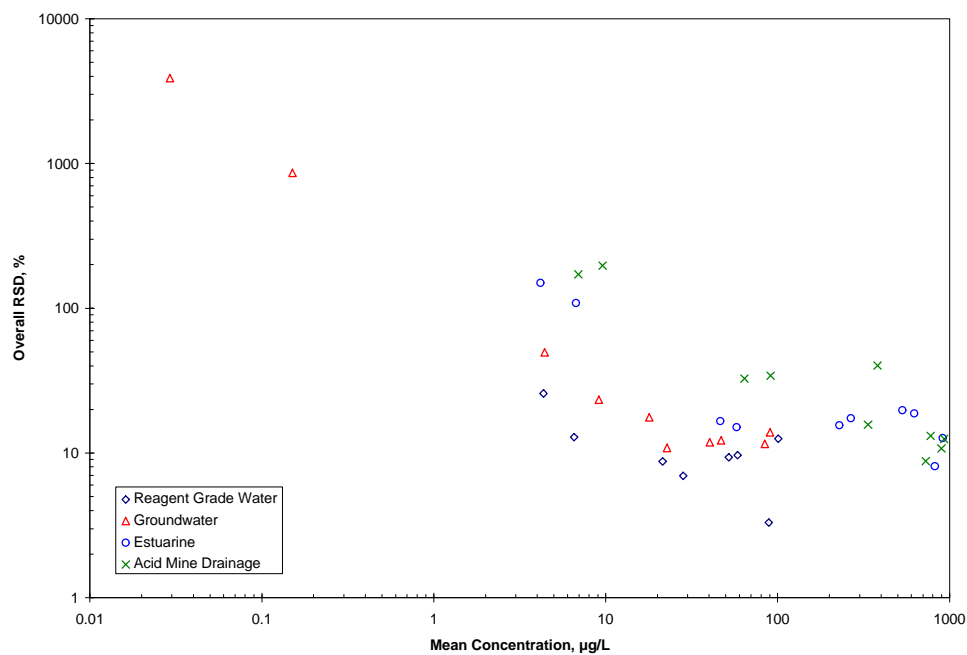


Figure 7-7 Plot of the overall relative standard deviation versus the mean concentration for arsenic by GFAAS



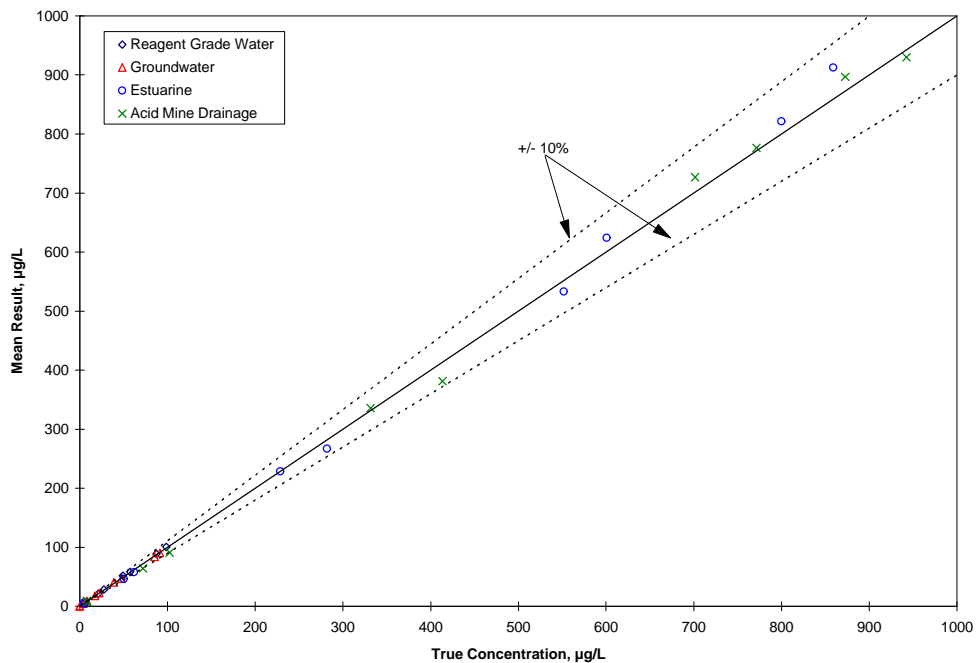


Figure 7-8 Plot of the mean result versus the true concentration for arsenic in all matrices by GFAAS

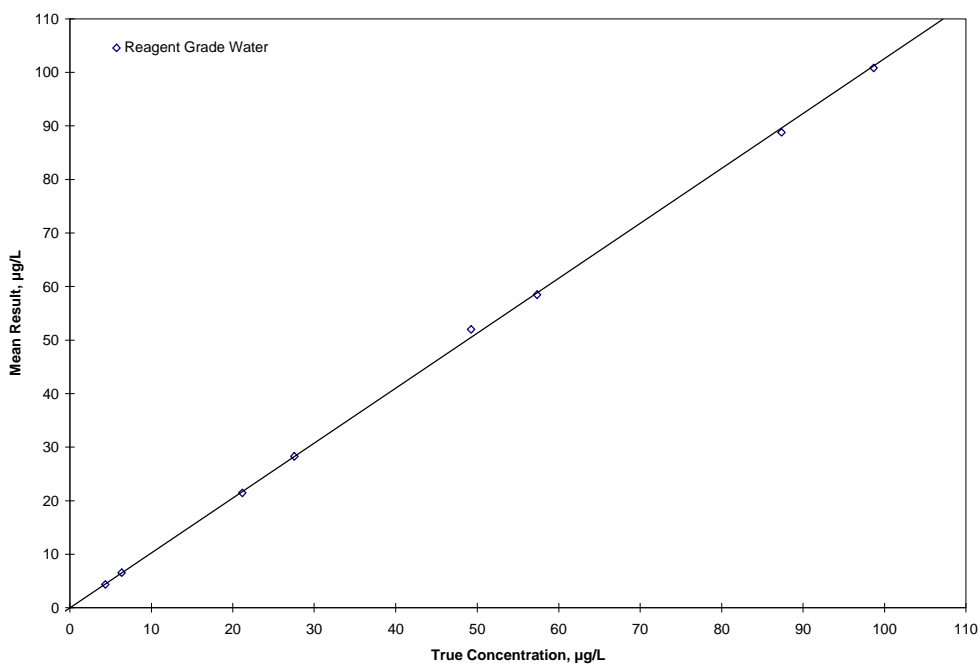


Figure 7-9 Plot of the mean result versus the true concentration for arsenic in reagent grade water by GFAAS

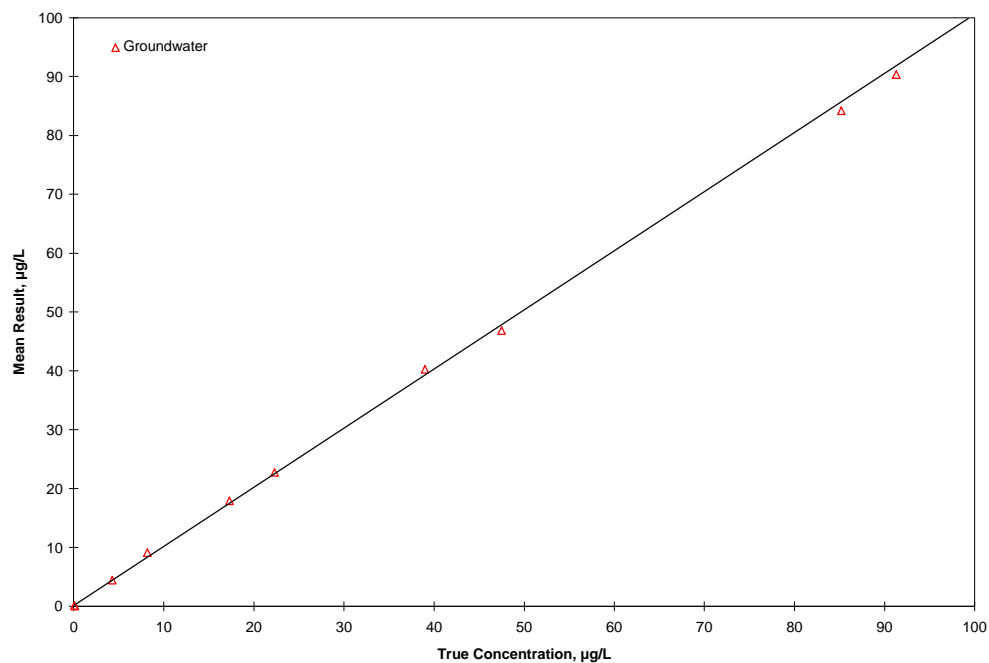


Figure 7-10 Plot of the mean result versus the true concentration for arsenic in groundwater by GFAAS

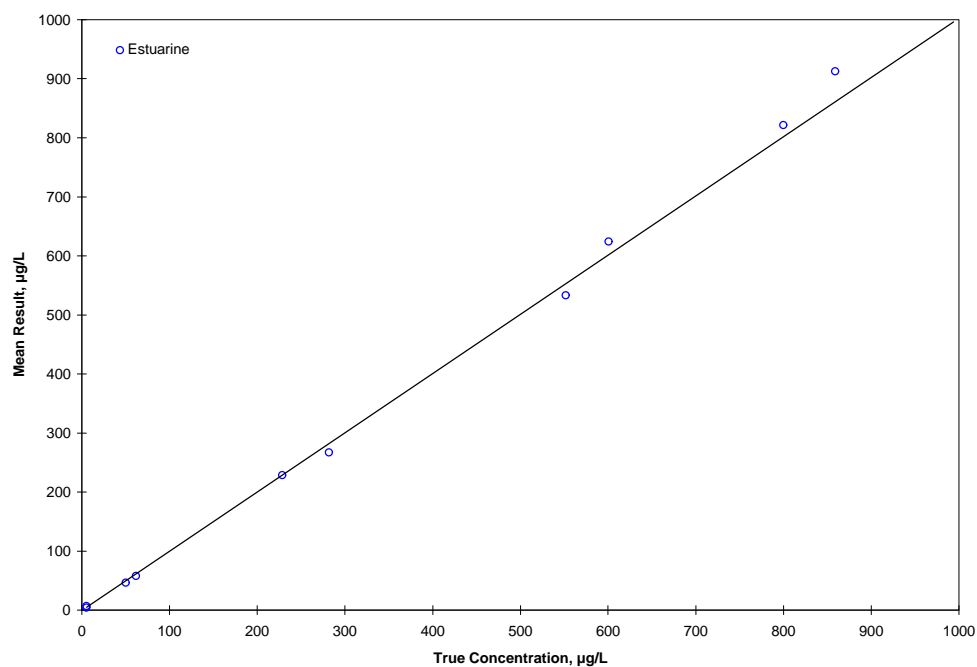


Figure 7-11 Plot of the mean result versus the true concentration for arsenic in estuarine water by GFAAS

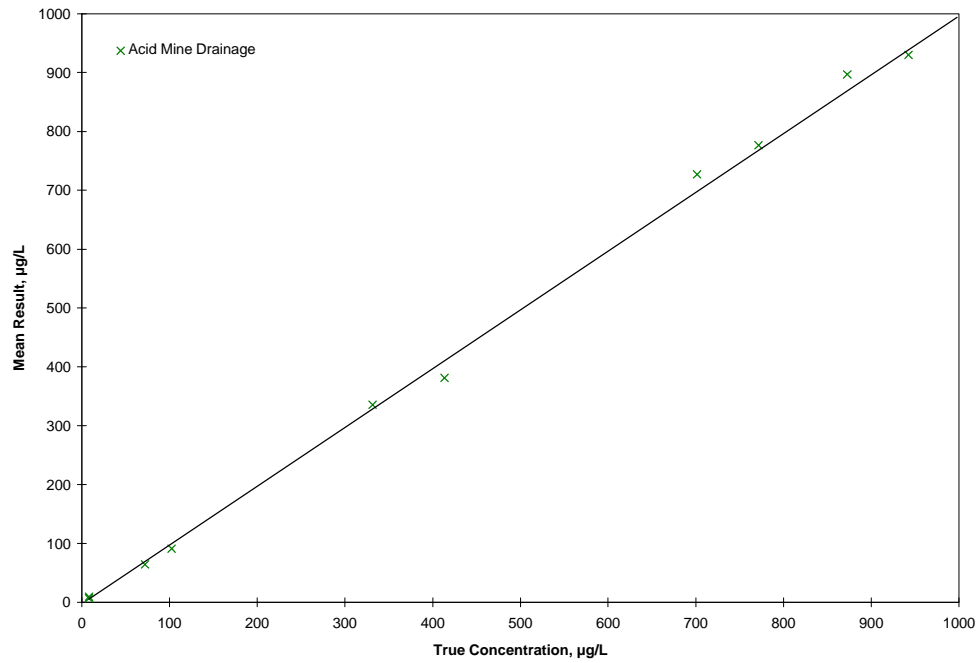


Figure 7-12 Plot of the mean result versus the true concentration for arsenic in acid mine drainage by GFAAS

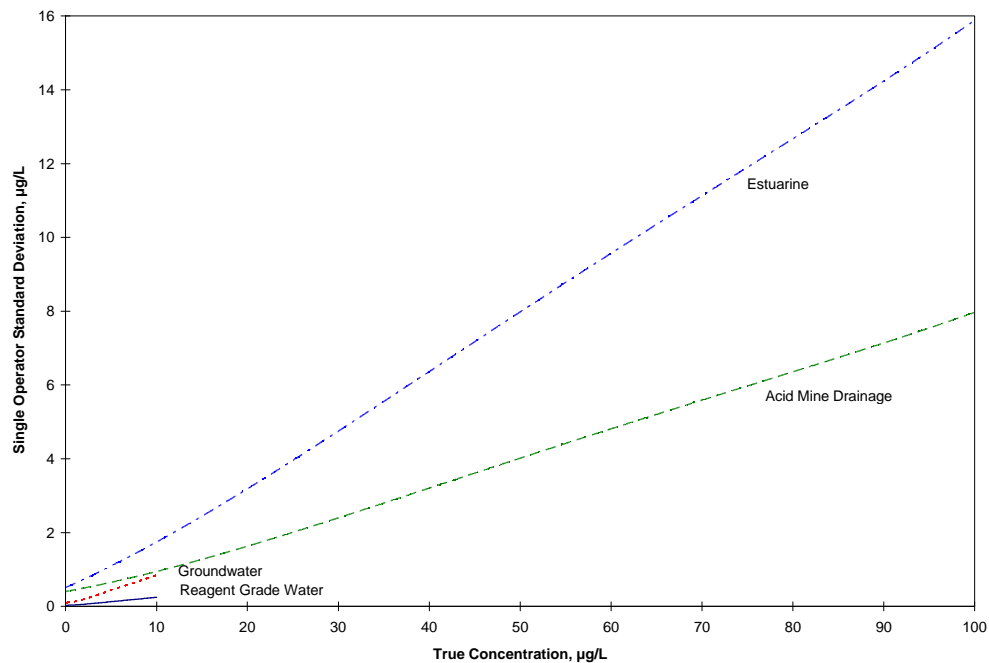


Figure 7-13 Plot of the single operator standard deviation versus the true concentration for cadmium by GFAAS

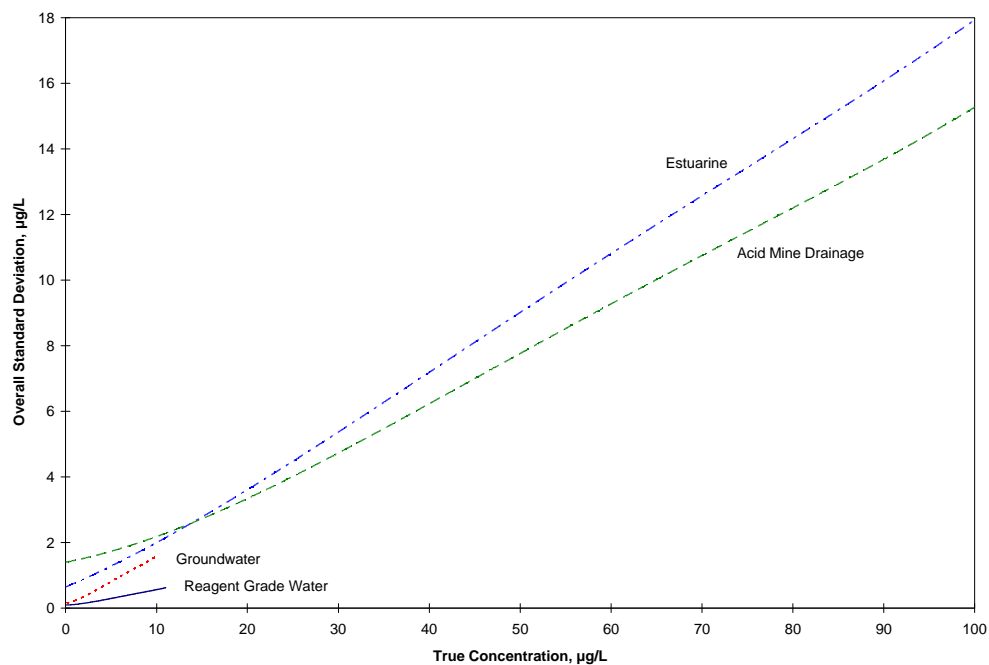


Figure 7-14 Plot of the overall standard deviation versus the true concentration for cadmium by GFAAS

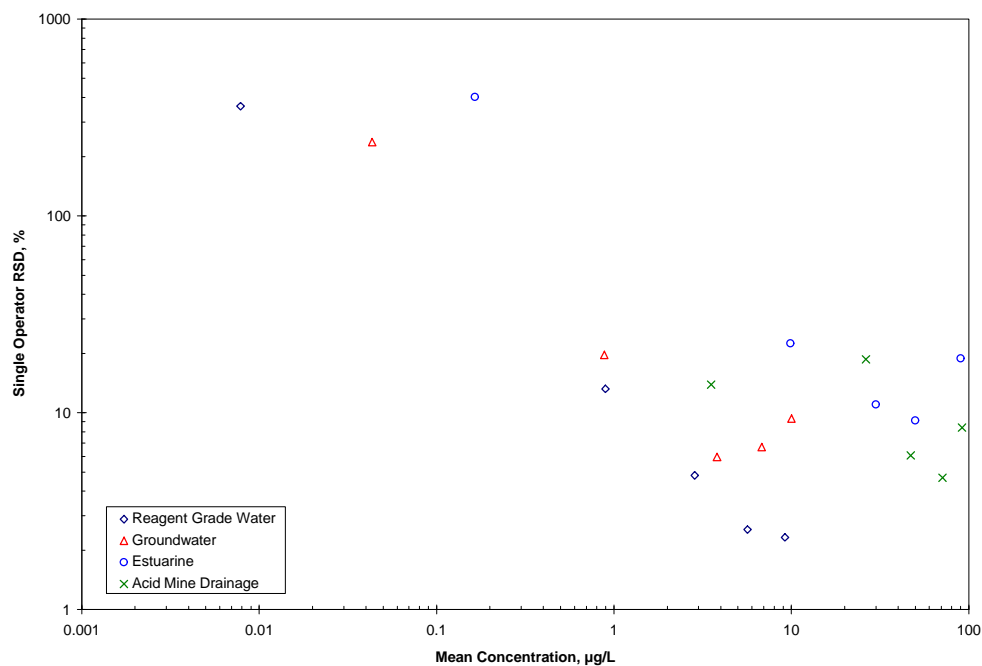


Figure 7-15 Plot of the single operator relative standard deviation versus the mean concentration for cadmium by GFAAS

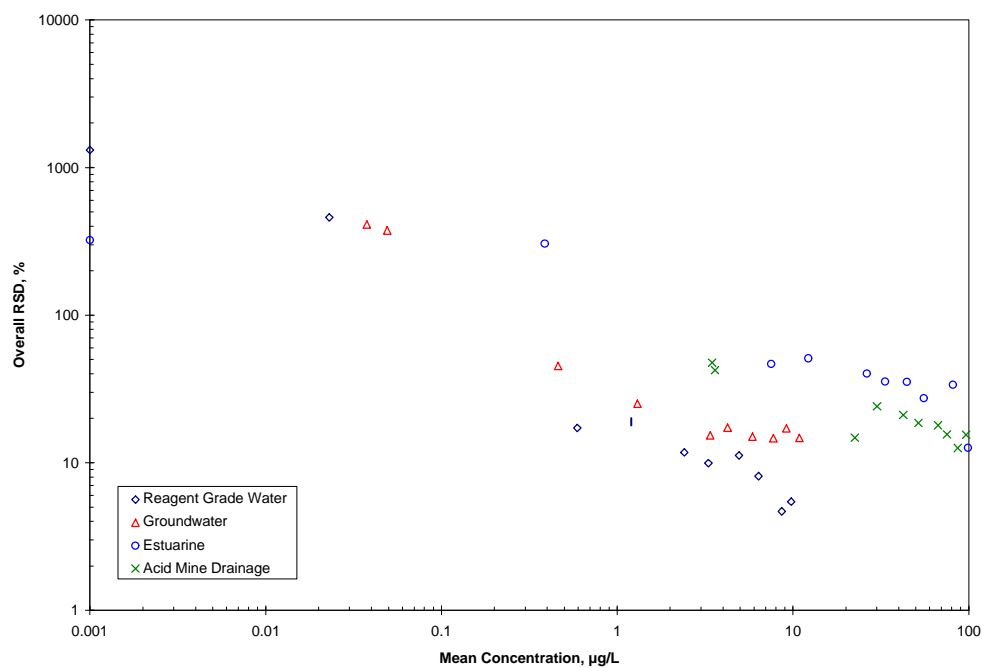


Figure 7-16 Plot of the overall relative standard deviation versus the mean concentration for cadmium by GFAAS

**Cadmium Recovery.** Figure 7-17 is the plot of the recovery (mean result versus true concentration) for cadmium in all matrices. Some recoveries for estuarine and acid mine drainage were beyond the 90 to 110% percent recovery range, but all recoveries were within 80 to 120%. Figures 7-18 through 7-21, recovery plots by matrix with the weighted linear regression shown, illustrate good linearity of the recovery data with the recoveries trending a bit high for reagent grade water, groundwater and acid mine drainage. The estuarine recoveries were fairly linear but trended low at the lower concentrations.

### 7.3.3 Chromium

**Chromium Standard Deviation.** Figure 7-22 shows the single operator standard deviation versus true concentration of chromium for all matrices. The single operator regression curves are similar for all matrices across the concentration ranges studied. Figure 7-23, the overall standard deviation plot, shows that the higher TDS matrices, estuarine and acid mine drainage, have higher absolute standard deviations than the lower TDS matrices, reagent grade water and groundwater. Absolute standard deviations were highest for acid mine drainage above approximately 50 µg/L.

Figures 7-24 and 7-25 plot the single operator and overall relative standard deviation versus mean concentration for all matrices using a log/log scale. A general trend of decreasing RSD with increasing concentration is observed, leveling off at less than about 10% for single operator RSDs and 20% for overall RSD.

**Chromium Recovery.** The recoveries (mean results versus true concentrations) for chromium in all matrices, plotted in Figure 7-26, were within  $\pm 10\%$ . The plots by individual matrix, Figures 7-27 through 7-30, illustrate the good recoveries for each matrix.

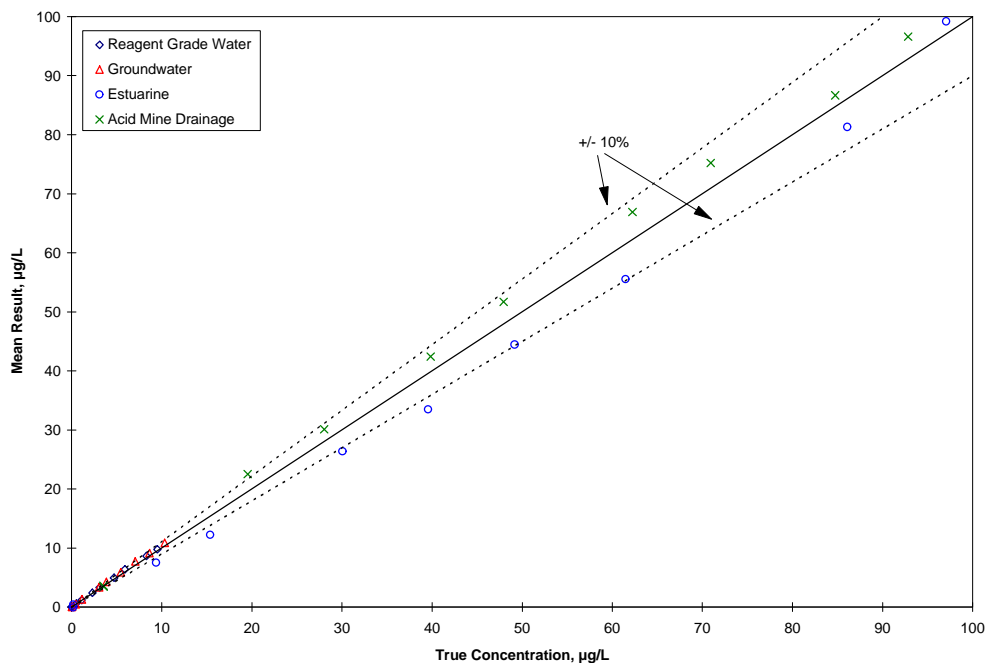


Figure 7-17 Plot of the mean result versus the true concentration for cadmium in all matrices by GFAAS

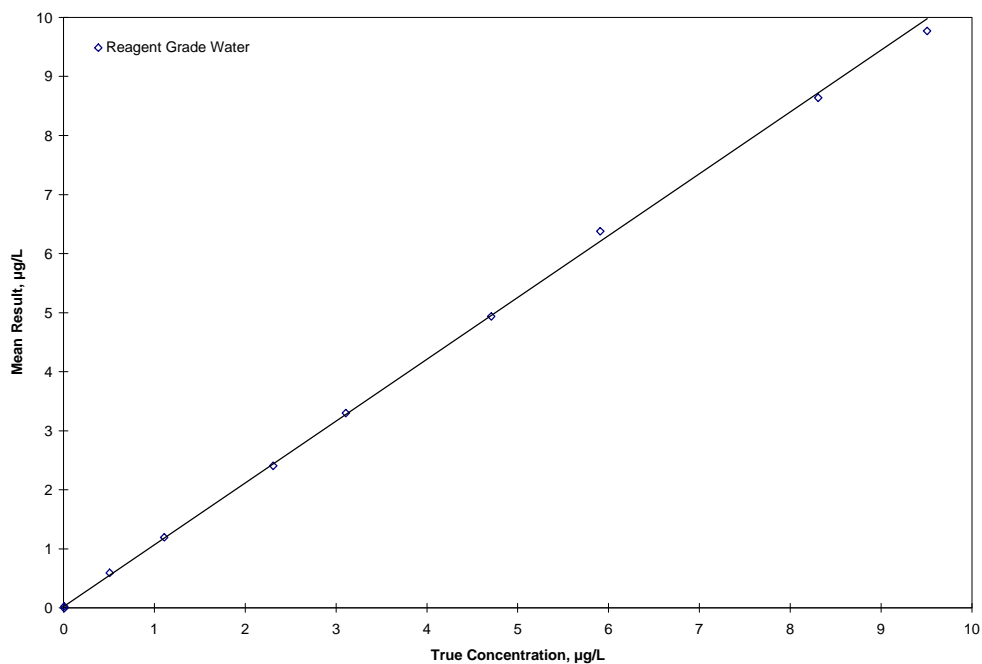


Figure 7-18 Plot of the mean result versus the true concentration for cadmium in reagent grade water by GFAAS

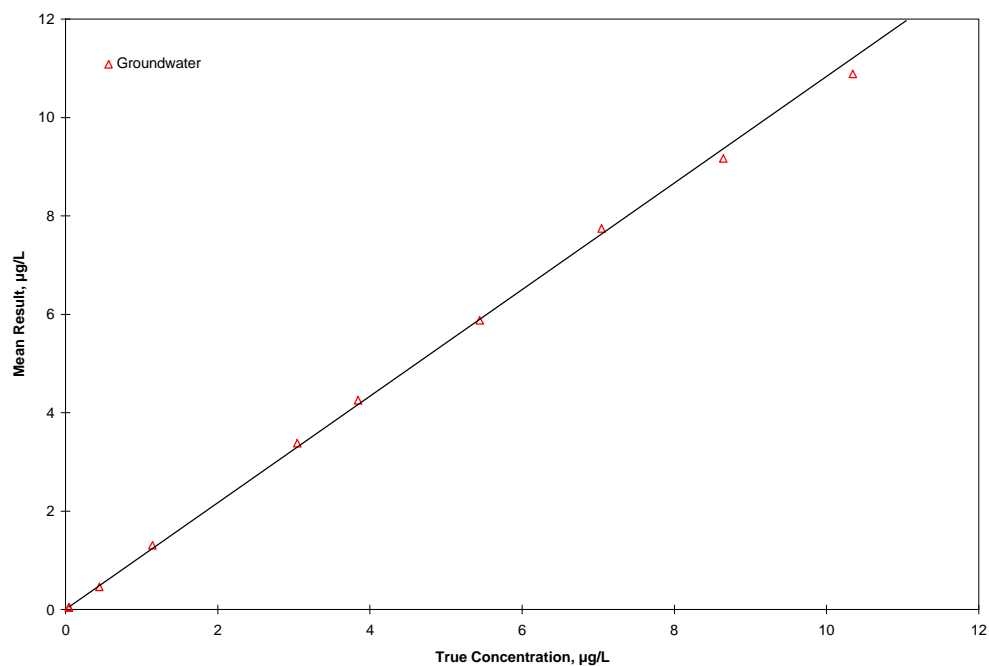


Figure 7-19 Plot of the mean result versus the true concentration for cadmium in groundwater by GFAAS

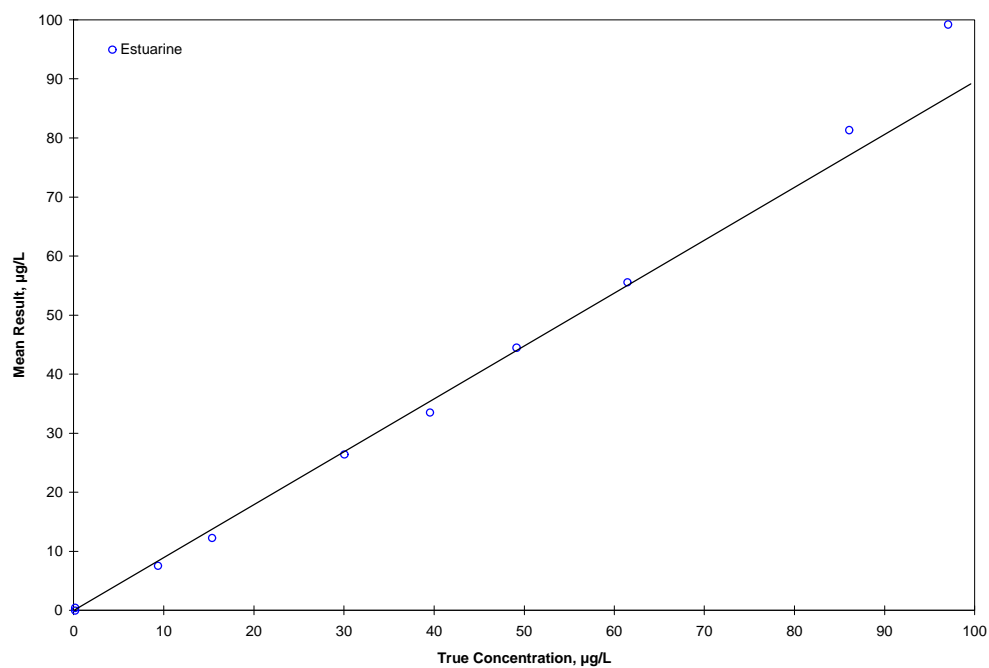


Figure 7-20 Plot of the mean result versus the true concentration for cadmium in estuarine water by GFAAS



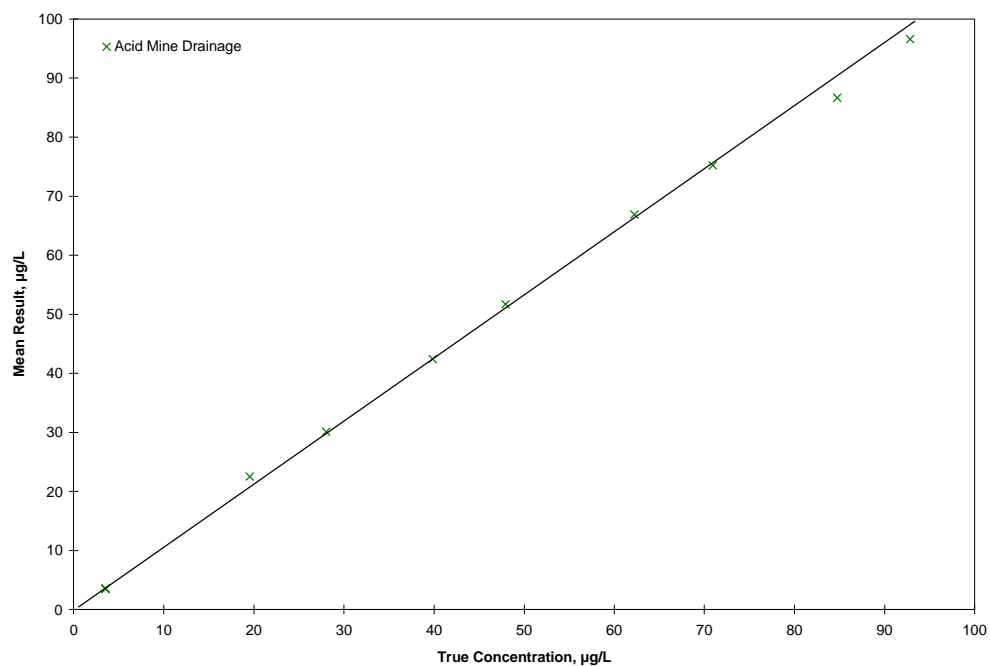


Figure 7-21 Plot of the mean result versus the true concentration for cadmium in acid mine drainage by GFAAS

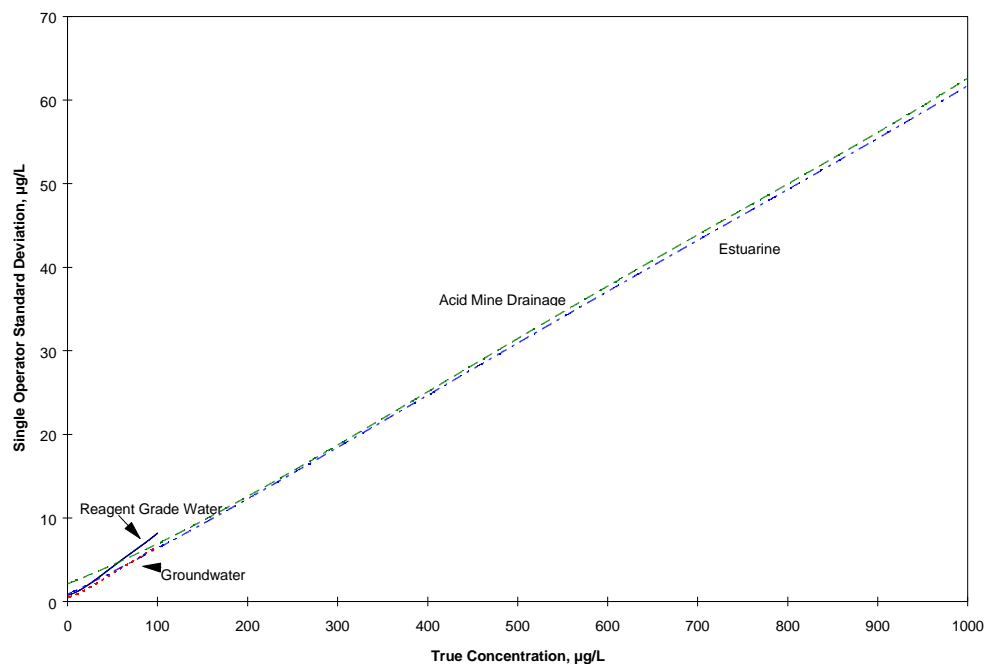


Figure 7-22 Plot of the single operator standard deviation versus the true concentration for chromium by GFAAS

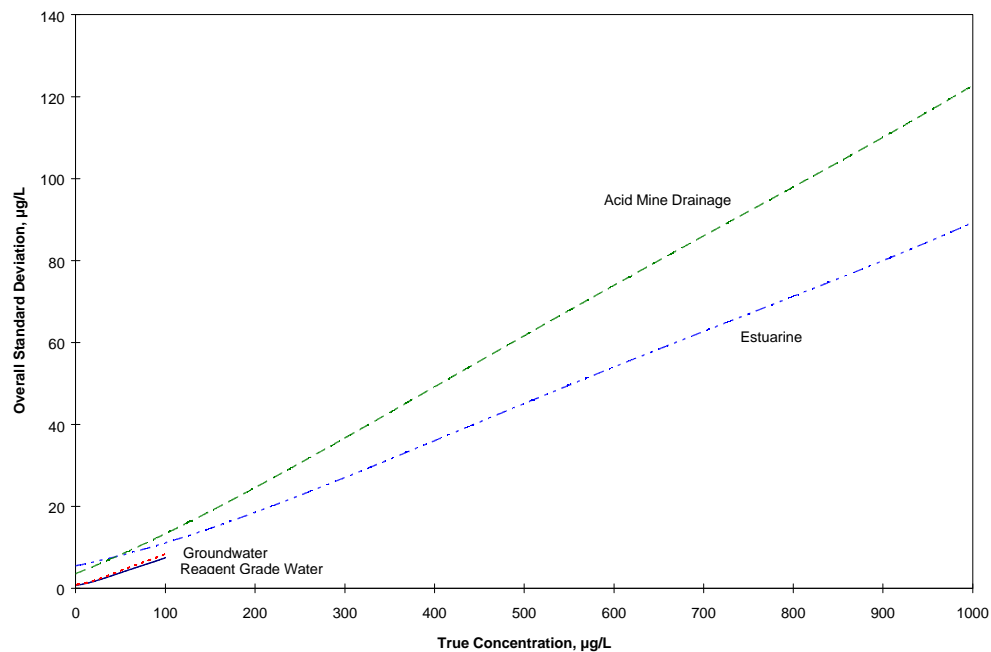


Figure 7-23 Plot of the overall standard deviation versus the true concentration for chromium by GFAAS

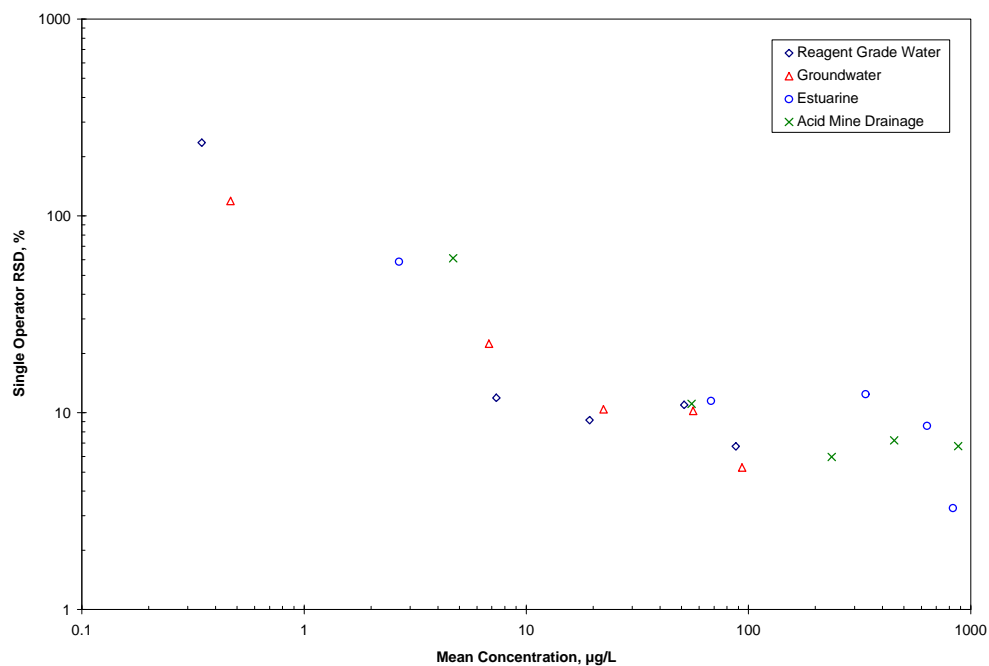


Figure 7-24 Plot of the single operator relative standard deviation versus the mean concentration for chromium by GFAAS

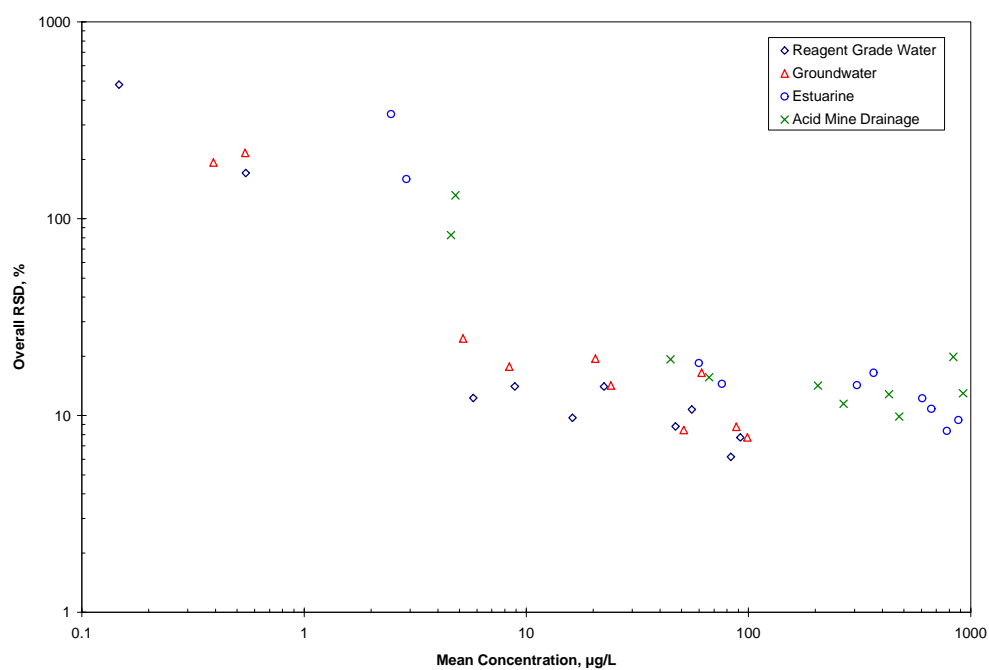


Figure 7-25 Plot of the overall relative standard deviation versus the mean concentration for chromium by GFAAS

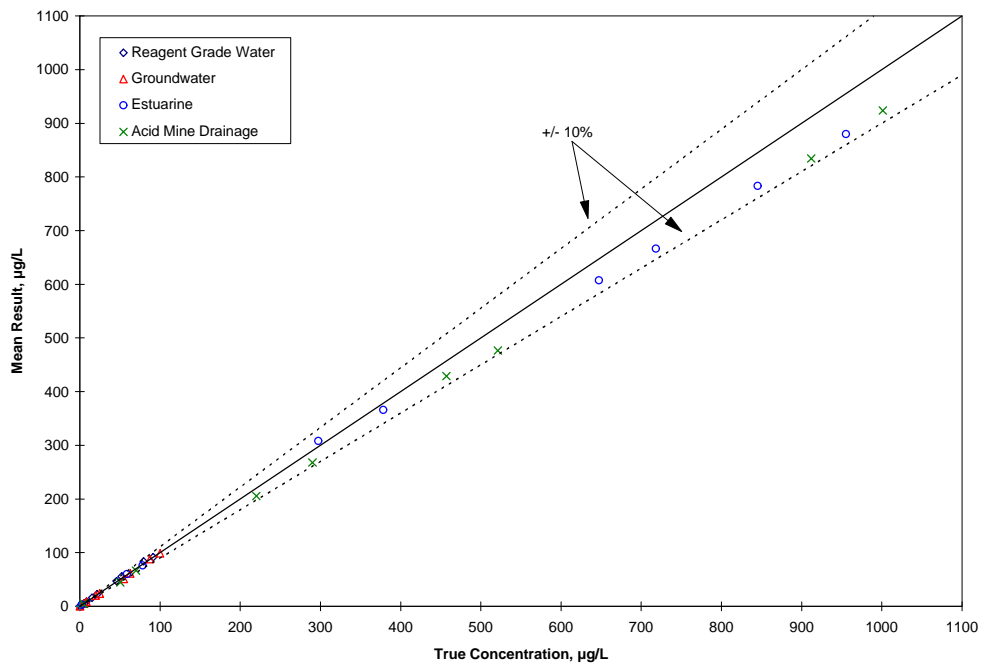


Figure 7-26 Plot of the mean result versus the true concentration for chromium in all matrices by GFAAS

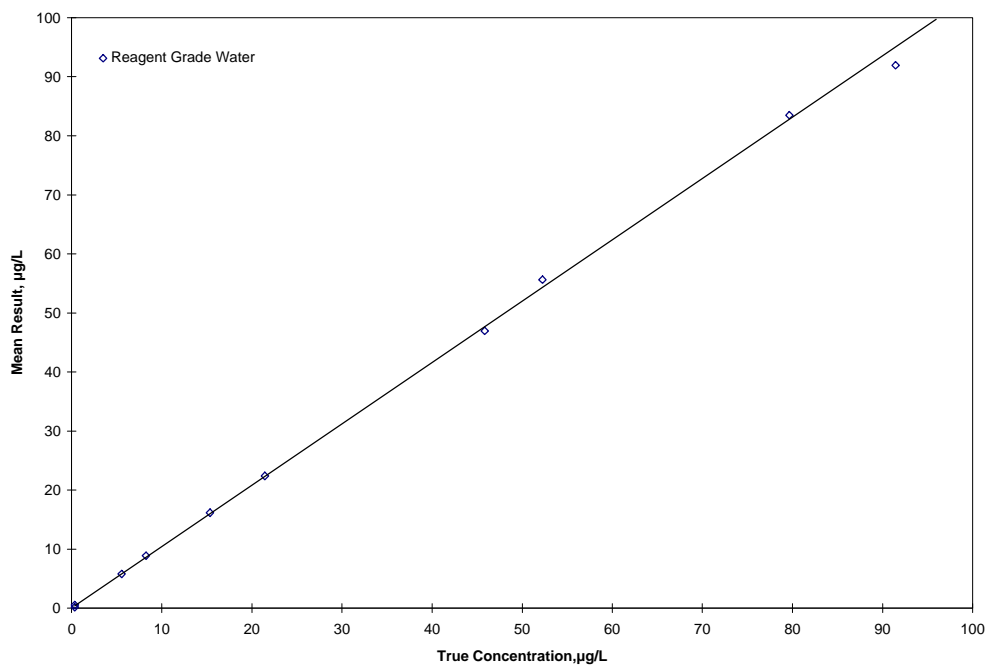


Figure 7-27 Plot of the mean result versus the true concentration for chromium in reagent grade water by GFAAS

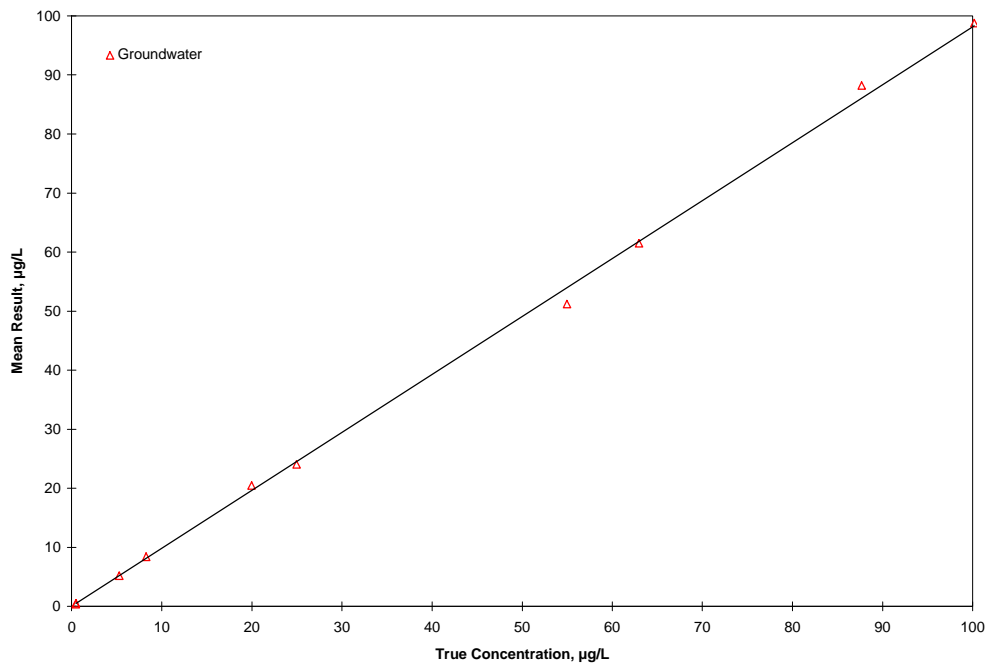


Figure 7-28 Plot of the mean result versus the true concentration for chromium in groundwater by GFAAS

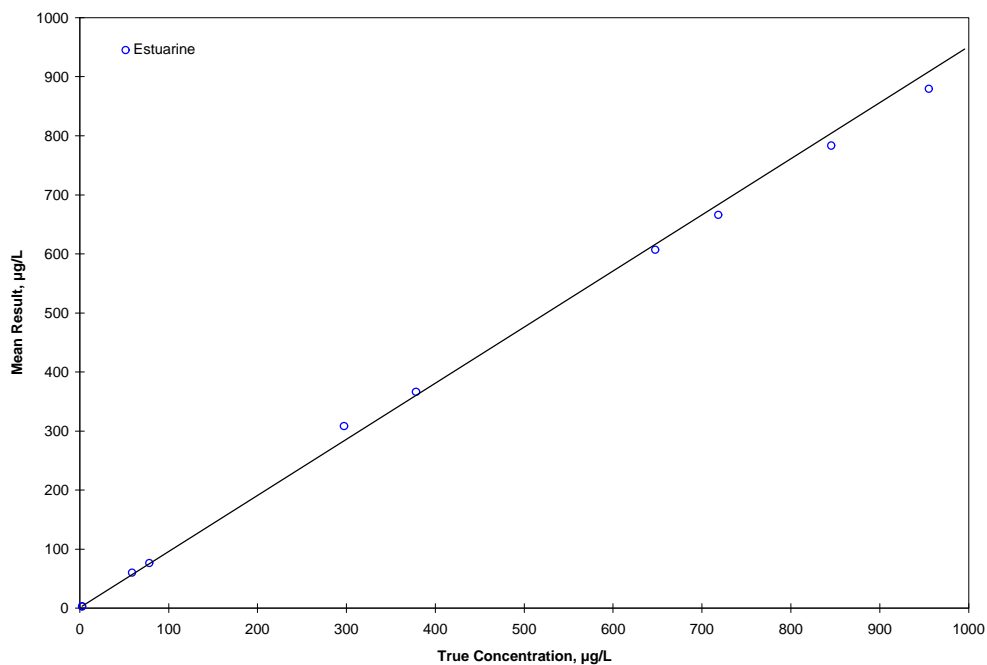


Figure 7-29 Plot of the mean result versus the true concentration for chromium in estuarine water by GFAAS

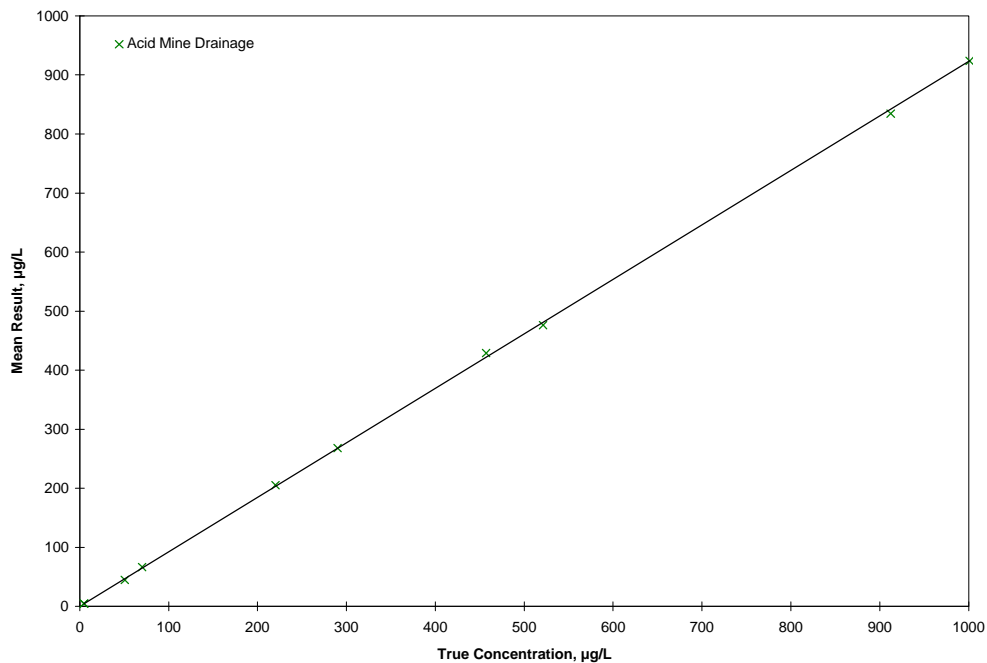


Figure 7-30 Plot of the mean result versus the true concentration for chromium in acid mine drainage

## 7.4 References

1. American Society for Testing and Materials, "Standard Practice for Determination of Precision and Bias of Applicable Methods of Committee D-19 on Water," D2777-96, *Annual Book of ASTM Standards*, 1997.

# 8

## ALTERNATIVE MINIMUM LEVEL

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In order to evaluate and negotiate permit levels, utilities require detection and quantification level definitions and values that specifically address compliance monitoring situations by incorporating the following:

- Interlaboratory standard deviation to account for the variability associated with the analysis of split samples by the utility and the regulator, and the use of different laboratories over the life of the permit
- Estimates of the standard deviation over a range of concentrations including zero, if possible, to account for changes in standard deviation with concentration
- Terms and definitions readily discernible by users as different from existing definitions based on single-operator or pooled single-operator standard deviation
- Statistical treatment of data appropriate for future monitoring decisions.

In the 1994 draft EPA guidance (1) for dealing with detection and quantification levels in the National Pollutant Discharge Elimination System (NPDES) for setting and determining compliance with water quality-based effluent limitations (WQBEL), when measured data are below the quantification level the USEPA proposed that:

- Zero would be used in place of all analytical results below the quantification level
- Quantification would be computed using the interim Minimum Level (ML).

Setting the quantification level at the interim ML, as the USEPA proposes to define it, is not justified for a number of technical reasons. This section will explain the technical and regulatory issues behind the selection of a quantification level and will provide the background for the approach recommended by EPRI to compute a quantification level that can be used in the compliance monitoring environment.

Section 8.1 describes the fundamentals of detection and quantification levels using terminology based on the commonly accepted convention by Currie (2, 3). In Section 8.2, we briefly summarize several of the key approaches suggested for defining detection and quantification levels that have been considered to date. Also in Section 8.2 the shortcomings with the USEPA 40 CFR Part 136 Method Detection Limit (MDL) and EPA's proposed interim Minimum Level (ML) definitions for detection and quantification, respectively, are documented. During 1995, EPRI participated in an industry coalition that developed a technical consensus on principles and properties associated with detection and quantification. As a result, a statistically defensible

estimate of a quantification level called the Alternative Minimum Level (AML) was developed. In Section 8.3 the problems and proposed solutions to modeling standard deviation data are illustrated using data developed from this EPRI project. Section 8.4 presents the Alternative Minimum Level (AML), and explains how the AML relates to the earlier Compliance Monitoring Detection Level (CMDL) and Compliance Monitoring Quantitation Level (CMQL) definitions published by EPRI. Section 8.4 also shows how the AML addresses the problems with the interim ML and presents the procedure for computing the AML using the interlaboratory data from this validation program. In Section 8.5 the reader is provided guidance on the use of the data in this report in the context of compliance monitoring permits. The ASTM Interlaboratory Detection Estimate (IDE) is introduced in Section 8.6.

## 8.1 Technical Approaches to Detection and Quantification Levels for Demonstrating Regulatory Compliance

There are a myriad of terms for levels of detection (e.g., Method Detection Limit (MDL), Detection Level (DL), Instrument Detection Level (IDL)), but their conceptual foundations are often quite diverse leading to inconsistency in practice. Although less intensively studied, the same problem exists for limits of quantification (4). Over the years chemists have used "2-sigma" and "3-sigma" detection levels without precise definition or meaning. The United States Environmental Protection Agency (USEPA) continued this practice when they published detection levels (DL) without definition in the Methods of Chemical Analysis of Water and Wastes (MCAW) (5). Unfortunately, these levels have been widely used in the regulatory environment, where they were neither intended nor appropriate, because levels specific to compliance monitoring had not been introduced (6,7). To provide a framework within which to compare and contrast these various methodologies, the pioneering work of Currie (2) is used.

### 8.1.1 The Detection Problem

With respect to analytical detection, Currie (2) defined two levels; the critical level ( $L_c$ ) and the detection level ( $L_d$ ). The  $L_c$  is the point at which "one may decide whether or not the result of an analysis indicates detection." The  $L_d$  is the point at which "a given analytical procedure may be relied upon to lead to a detection." There is an important distinction between these two levels. At the  $L_c$  we have confidence that a measurement is not a "false positive." We are minimizing the chance of erroneously reporting that something is present when it is not. However we must go up to the detection level before we can be confident that the analytical procedure is not "missing" a substance when it is actually present. At the  $L_d$  we are confident that a measurement is not a "false negative" or a "false positive."

Statistically, the  $L_c$  is the concentration above which the response signal is significantly different from zero (Figure 8-1). When a measurement exceeds  $L_c$ , we can make the



binary decision, "detected." A measured result at or above the critical level tells us the pollutant is present. But a measured result below the critical level does not tell us with confidence that the pollutant is absent. That is because replicate measurements of a sample with a true value equal to the critical level will fall both above and below the critical level at roughly the same frequency.

Those measured results falling below the critical level will be deemed non-detects. But those measured results really are false non-detects, given that the true value is equal to the critical level (and thus we know the pollutant is present). Note that when the "true" concentration is zero, the probability of the correct decision "not detected" is  $(1 - \alpha)$  where  $\alpha$  is the Type I error rate or false positive rate of the statistical test. The Currie  $L_c$  is equivalent in concept to the EPRI Compliance Monitoring Detection Level (CMDL) developed in an earlier effort (Z).

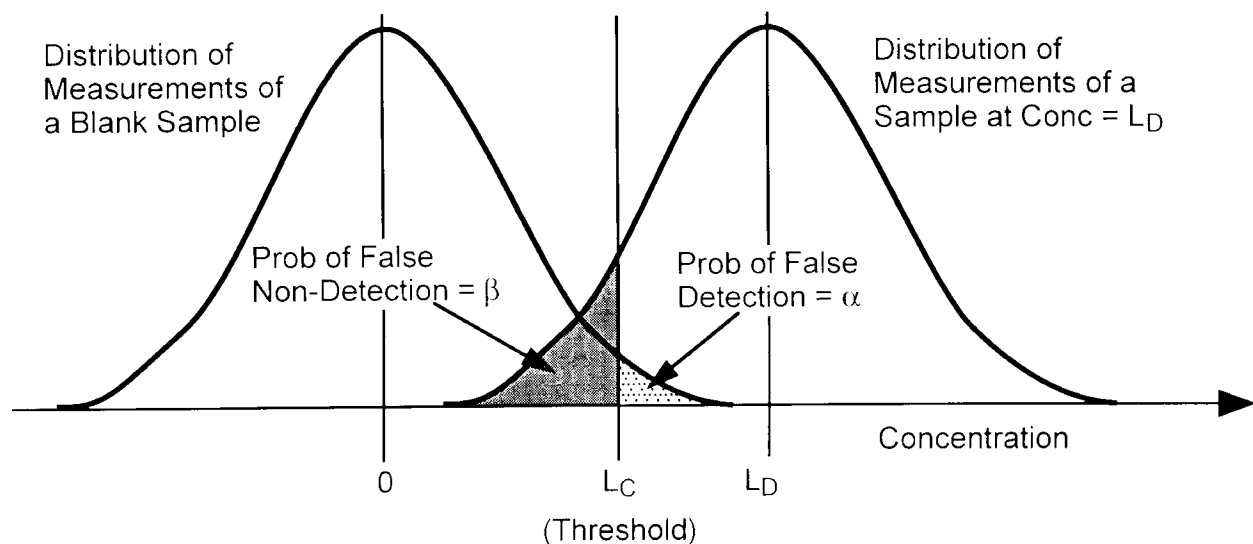


Figure 8-31 Relationship between Currie's  $L_c$  and  $L_d$ .

Assuming a symmetric distribution of measurement errors, when the "true" concentration is equal to  $L_c$  the probability of reporting it below  $L_c$  is 50%. This is termed the Type II error rate or false negative rate ( $\beta$ ).

To accommodate both Type I and II errors Currie developed the "detection level"  $L_d$ . At the detection level, the non-detect problem is controlled. While replicate measurements of a sample with a true value equal to the  $L_d$  will fall both above and below the  $L_d$ , the detection level has been developed to ensure that virtually all of the measurements falling below it will nonetheless fall above the  $L_c$ . Thus, for a true value equal to the  $L_d$ , virtually all of the measurements that fall below the  $L_d$  will be deemed detected. Only a very small set percentage (e.g., 1 %) of those measurements will fall below the critical level and be deemed erroneously non-detects.

When the true concentration is  $L_D$ , then the Type II error rate ( $\beta$ ) using  $L_C$  as the critical level is small. For example, assuming that  $\alpha = \beta = 0.01$ , then another way of stating this is that 99 % of the measured concentrations for samples not containing the analyte will be less than the  $L_C$  and 99% of the measured concentrations for samples with true concentration equal to  $L_D$  will be greater than  $L_C$ . That is, when the true concentration is equal to the  $L_D$ , the probability of a measurement below the  $L_C$  is 1% (2). Currie's  $L_D$  definition is conceptually equivalent to the EPRI Compliance Monitoring Quantitation Level (CMQL) developed in earlier efforts (7). It should be noted that Currie did not specify the source of data variability whether from within lab or between lab errors.

As can be seen from these definitions, the critical level and detection level are quite distinct. Above the critical level, we can have  $(1 - \alpha)$  100% confidence that the true concentration is greater than zero; whereas above the detection level we can have  $(1 - \beta)$  100% confidence that the true concentration is greater than  $L_C$ . Figure 8-1 illustrates the relationship between  $L_C$  and  $L_D$  and Table 8-1 summarizes the definition and implications of the Currie scheme for defining detection and quantification levels. A number of other authors have followed Currie's lead and proposed definitions for detection and quantification levels to include control of both false positive and false negative rates (8, 9, 10, 11, 12, 13).

### 8.1.2 The Quantification Problem

Currie (2) defined the determination level ( $L_Q$ ) as the concentration "at which a given procedure will be sufficiently precise to yield a satisfactory quantitative estimate." This definition is similar to that used by Adams, Passmore and Campbell (14) who defined a "minimum working concentration" as that for which the relative standard deviation (RSD) was 10%. The American Chemical Society (ACS) (11) chose to define quantification as the lowest concentration at which a  $\pm 10\%$  relative standard deviation (RSD) could be obtained. The determination level has since been described by several names, most notably "Practical Quantitation Level" PQL (15) and "Limit of Quantitation" (16). USEPA (16) defines the PQL as "the lowest level achievable by good laboratories within specified limits during routine laboratory operating conditions." The USEPA has also defined the quantification level over the years in at least two ways: (1) as 5 or 10 times the method detection limit (MDL), and (2) as the lowest true concentration at which 75 % of the laboratories in an interlaboratory study can measure within the "acceptance limits." The first definition is arbitrary, and depends completely on the validity of the corresponding method detection limit, about which serious questions have already been raised (17). The second definition is considerably better; however, the interlaboratory studies are often done in experienced government laboratories that "knew they were being tested with standard samples in distilled water without matrix interferences." The USEPA (15) also points out that, "Actual day-to-day operations in a wide variety of laboratories using real samples in natural water would be expected to produce poorer results, i.e., wider performance ranges especially at the lower concentration levels."

Table 8-1

## Summary of Currie's(2) Scheme for Detection and Quantification Levels

Level	Definition	Statistical Implications
Critical level, $L_c$	"The point at which one may decide whether or not the result of an analysis indicates detection."	False positive (Type I) error rate controlled; signal is statistically different from zero. Equivalent to the EPRI CMDL.
Detection level, $L_d$	"The point at which a given analytical procedure may be relied upon to lead to a detection."	False positive and false negative (Type II) error rate controlled; essentially the definition of the EPRI CMQL
Quantification level, $L_q$	"The concentration at which a given procedure will be sufficiently precise to yield a satisfactory quantitative estimate."	Lowest concentration at which an RSD of 10% obtained.

Kempic of the USEPA presented detailed procedures (18) using interlaboratory studies for calculating acceptance limits (ACL) and the practical quantitation level (PQL) which the USEPA (19) defined as the lowest true concentration for which greater than 75% of the laboratories can measure within  $\pm$  the ACL. The latter was based on the 95% confidence limit at the maximum contaminant level goal (MCLG) or, where the MCLG was zero, at a concentration five times the Method Detection Limit. Britton (20) of the USEPA proposed an alternative definition for LOQ - the lowest true concentration for which the probability of an analytical response below the detection level is small. This definition was similar to one proposed earlier by Currie (2). It is important to note that the ACS definition, the USEPA definition of PQL as a multiple of the MDL, as well as the above Britton alternative utilize only intralaboratory standard deviation for their derivation. (See Koorse (21) for a review of the legal implications of these definitions.)

### 8.1.3 Calibration Curve Methods for Computing Detection and Quantification Levels

In recent years, a great deal of interest has been shown in the use of "calibration curve" procedures to compute the two fundamental detection parameters defined by Currie: his critical level ( $L_c$ ) and his detection level ( $L_d$ ). Some prescribed procedure is followed using replicate samples at multiple levels of known concentration (but in almost all instances, the replicate samples are not externally prepared reference samples), to produce a set of points of measured (observed) concentration vs. actual (true) concentration. Some form of linear or other regression on this set of points is then performed to produce the curve of actual vs. measured concentration, known as the "Calibration Curve." An uncertainty interval around the curve is then calculated. All of the calibration curve methodologies follow the above basic procedure: it is in the details of the type of regression (ordinary least squares, weighted least squares, curvilinear, etc.) and the type of uncertainty interval (prediction or tolerance intervals) that the various methods differ. Once generated, this calibration graph or expression can be readily applied to determine the two fundamental detection parameters defined by Currie. Included in this class are methods by Hubaux and Vos (22), Clayton, et al. (23) USATHAMA (24), Gibbons, et al. (25), Coleman (26).

## 8.2 EPA Definitions of Detection and Quantification and Their Problems

The concept for the Method Detection Limit (MDL) was proposed in 1981 by Glaser et al. (12). The proposed approach computed a detection level based on the standard deviation of replicate measurements at a single concentration combined with a hypothesis test (at the 0.99 level) to determine a quantity similar to the critical level defined by Currie (2). The method (13) currently applied by EPA in 40 CFR Part 136 closely follows the method of Glaser (12). For a particular sample analyte,  $n$  replicate analyses (minimum of 7) are performed at a single spiking concentration. All  $n$  replications typically are performed at the same laboratory. Based on the standard deviation(s) of these  $n$  measurements, a Currie  $L_c$  type parameter (which EPA calls the "Method Detection Limit" (MDL)) is calculated as:

$$MDL = t_{(0.01, n-1)} \cdot s \quad (\text{eq. 102})$$

where  $t$  is the appropriate value from the  $t$ -distribution for  $n-1$ .

The EPA's current estimate of a limit resembling a quantification level is based loosely on the "Limit of Quantitation (LOQ)" defined by the American Chemical Society (9) as the lowest concentration with an RSD of 10% (i.e., the ratio of measurement standard deviation to measurement mean concentration = 0.1 or, the measurement mean is ten times the standard deviation). While the ACS and Currie have also expressed the

quantification level ( $L_Q$ ) as a “10 sigma” limit, their sigma actually refers to the standard deviation of a net signal or concentration and not the true population standard deviation. If one assumes the “sigma” to be constant versus concentration, the 10 sigma quantification level can be shown to give an RSD of 10% because:

$$RSD = \left( \frac{s}{L_Q} \right) \times 100\% \quad (\text{eq. 103})$$

$$RSD = \left( \frac{s}{10s} \right) \times 100\% \quad (\text{eq. 104})$$

$$RSD = (0.10) \times 100\% \quad (\text{eq. 105})$$

or

$$RSD = 10\% \quad (\text{eq. 106})$$

The EPA interim Minimum Level (ML), described on page 8-1, was derived from the “10 sigma” definition by assuming that the standard deviation at the MDL and the interim ML are the same hence:

$$MDL = 3.14s \quad (\text{eq. 107})$$

and

$$ML \cong 10s \quad (\text{eq. 108})$$

so

$$\frac{ML}{MDL} = \frac{10s}{3.14s} = 3.18 \quad (\text{eq. 109})$$

thus:

$$ML \cong 3.18 \times MDL \quad (\text{eq. 110})$$

In the compliance monitoring situation, there are a number of problems with EPA’s approach to computing an interim ML. The EPA draft guidance (1) directs that an

interim ML be developed by multiplying the published MDL by 3.18 and then rounding “to the nearest multiple of 1, 2, 5, 10, 20, 50 etc.” Yet by EPA’s definition, the interim ML is supposed to represent the lowest value that can be reliably quantified. If the calculated value for the interim ML is rounded down, the resulting value will fall below the level that EPA deems to be quantifiable.

The biggest problem with the interim ML is that it is nothing more than a multiple of the MDL, which itself is a flawed statistic for a number of reasons:

- MDLs are based on intralaboratory data - Compliance monitoring is an interlaboratory comparison between the permittee and the permitter, yet the MDL can be based on only one analyst in one lab performing the MDL analysis in reagent grade water. Table 8-2 developed from EPRI RP1851 and EPA Method Study data, shows that the ratio of interlaboratory ( $s_i$ ) to intralaboratory ( $s_o$ ) precision (pooled single operator) varies from 1.2 to 2.5.
- The MDL is not reproducible - The EPA specifically states in 40 CFR Part 136, Appendix B that MDLs “are not necessarily reproducible on a routine basis in a given laboratory, even when the same analytical procedures, instrumentation and sample matrix are used.” What this means in practice is that an MDL computed from day to day or analyst to analyst will vary. A statistic with this sort of problem is not a good way to assess the ability of a method to measure analytes at or below the water quality based effluent limits (WQBEL).
- MDLs assume constant variance - The implicit EPA model of the MDL assumes that the standard deviation at zero is the same as that at the MDL. However, since variance is not constant with concentration, the MDL will be highly dependent on the spiking concentration. The lower the spike concentration the lower the MDL will be. In effect the MDL is not anchored statistically. If the MDL is to be determined in reagent grade water, 40 CFR Part 136 recommends that the test concentration be within a factor of 1 to 5 times the estimated MDL in reagent grade water. For a sample, if the analyte concentration does not exceed 10 times the estimated MDL in reagent grade water, the sample may be used as is for the determination of the MDL. Since the spiking concentration can vary over a wide range, the computed MDL can vary over that range. Figure 8-2 illustrates the point. Using the data from previous RP1851 validation studies, an MDL was computed at various spike ratios that were in the prescribed range stated in 40 CFR Part 136, Appendix B. As Figure 8-2 shows, the MDL varies by over a factor of 2.5 in this example. There are other examples where the spike to MDL levels off below 5:1, so that essentially any estimate of the MDL over some minimum concentration range would be valid.
- MDLs are not statistical predictors of laboratory performance - MDLs are based on the t-statistic which establishes a distribution of parameter estimates. It is not meant to predict multiple future events. The Alternative Minimum Level (AML) uses the

tolerance statistic which predicts a percentage of multiple future measurements with a desired level of confidence in the computation of a quantification level.

- In the published 40 CFR Part 136 methods, some MDLs have been listed, but no supporting data have been published with the methods.

**Table 8-2**

**Summary of Representative Ratios of  
Interlaboratory to Intralaboratory Standard  
Deviation.**

<b>Method</b>	<b><math>s_i/s_o</math></b>
<b>Organic Pollutants</b>	
MS-24, Method 601	2.2
MS-14, Method 604	2.3
MS-18, Method 608	1.2
MS-20, Method 610	1.5
NCASI, Method 1653	2.1
<b>Metal Pollutants</b>	
MS-31, 200 Series GFAAS	1.5
AWWA, 200.9 STPGFAAS	1.6
EPRI, 200 Series GFAAS	2.5

$s_i$  - Interlaboratory standard deviation

$s_o$  - Intralaboratory (pooled single operator) standard deviation

For a more complete discussion of the issues and problems associated with the interim ML (and MDL), the reader is directed to Koorse (27).

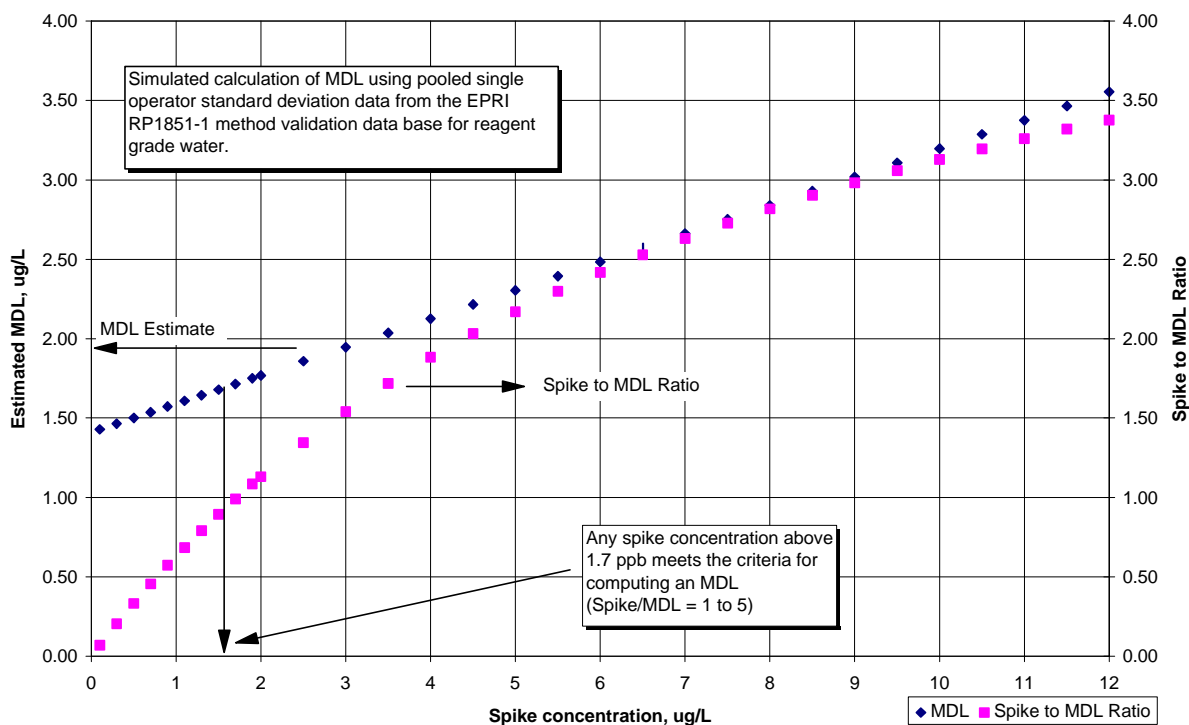


Figure 8-2. Effect of Changing the Spike Concentration on the Computation of the EPA MDL in Reagent Grade Water for Selenium by GFAAS

### 8.3 Modeling Standard Deviation Data

The original EPRI model for the behavior of standard deviation postulated that at or below the critical level the standard deviation would be nearly constant, primarily influenced by instrument noise. At some concentration the standard deviation would start to increase and eventually be proportional to the true concentration. Initially a linear equation was fitted to the standard deviation versus true data under the assumption that all the test concentrations were close to the detection limit. However, plots of the data and occasional negative intercepts indicated that our assumption was incorrect. To compensate for the curvature in the data sets, the data were fitted subsequently to an expression in the form:

$$s_t = a_0 a_1^T \quad (\text{eq. 111})$$

or

$$s_t = a_0 e^{a_1 T} \quad (\text{eq. 112})$$



where  $s_i$  is the interlaboratory standard deviation (as defined by ASTM D2777). Figure 8-3 shows the precision data from all of the EPRI GFAAS tests for the RGW, RW and APO matrices (note: the x-axis is logarithmic to accentuate the low concentrations). The exponential fit is reasonable and conceptually provides a relationship consistent with chemical laboratory observations.

Recently, Rocke and Lorenzato (28) suggested a model that appears to reflect the “hockey stick” form of the relationship between standard deviation and the true concentration. The Rocke-Lorenzato (R-L) equation can be simplified to the form:

$$s_i = (a_0 + a_1 T^2)^{1/2} \quad (\text{eq. 113})$$

This model is based on the assumption that the variance is composed principally of two error terms: 1) errors that are unrelated to analyte concentration (e.g. ambient contamination) and 2) errors that are proportional to analyte concentration (e.g. nebulizer flow variability).

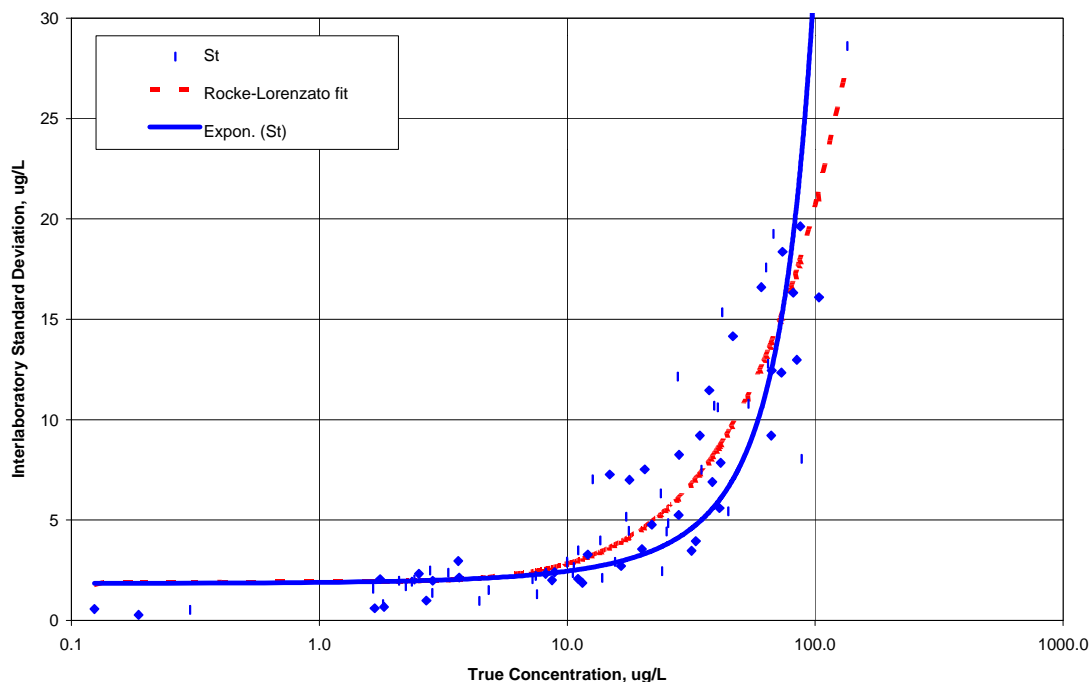


Figure 8-3. Curvilinear relationship of Interlaboratory Standard Deviation versus True Concentration; EPRI GFAAS Data for RGW, RW and APO.

Looking at Figure 8-3, both the exponential and the R-L models do a reasonable job at fitting the data to the lower concentrations, but the R-L model has a much better fit to the data above 10  $\mu\text{g/L}$  (this point is very apparent when the x-axis is a linear scale).

## 8.4 Alternative Minimum Level

During the summer of 1995, EPRI along with the Inter-Industry Analytical Group (IIAG), an industry coalition, conducted an extensive review of available detection and quantification level definitions (27). This evaluation produced two major outputs:

- A list of properties and performance standards to evaluate detection and quantification level definitions, and
- A consensus agreement on an Alternative Minimum Level (AML) to estimate a method's quantification level.

An evaluation of the original Compliance Monitoring Detection Level (CMDL) and Compliance Monitoring Quantitation Level (CMQL) definitions against the list of properties and performance standards for detection and quantification levels indicated that improvements were necessary to explicitly incorporate the dependence of quantification on relative standard deviation. Working within the industry coalition, EPRI developed a definition called the Alternative Minimum Level (AML) based on the CMDL and CMQL, but with additional statistical improvements to address relative standard deviation requirements. The following sections provide the background and computational approach to the AML.

### 8.4.1 Background and Overview

To address the problems identified with the MDL and the standard deviation data (single operator, single concentration) used to compute it, EPRI (7) originally developed the concept of the CMDL. The CMDL addressed the need for an interlaboratory based estimate of a detection level directed at the compliance monitoring case where the discharge permit was set at no permissible discharge (zero) of the regulated pollutant. In that situation the EPRI CMDL was equivalent to the concept behind Currie's (2) critical level ( $L_c$ ) (which is simply the lowest concentration that is distinct from zero to a specific level of confidence, thereby avoiding false positive errors). In EPRI's case, the CMDL was computed from the interlaboratory precision data from round robin validation studies with 20-30 laboratories and expressed as a curvilinear regression equation. A tolerance statistic was used to make the defined limit suitable for future measurements rather than the t-statistic used by the EPA, which is only meant to describe an existing population. This change in the computational process (7) addressed the problems described above with the MDL, but did not fully bring the CMDL to an estimate of a detection level under Currie's definition. The CMDL, however, may still be valuable possibly in cases where the regulatory limit is set at zero.

In this report  $L_{CI}$ , where the subscript “I” refers to interlaboratory to differentiate it from Currie’s  $L_{CI}$ , will be used in place of the CMDL to provide a direct link to Currie’s approach to detection. The  $L_{CI}$  is computed in the same fashion as the CMDL was, but the calculation of the degrees of freedom has changed from “n-2” to “n”. This change will cause a decrease in the k-factor used to compute the  $L_{CI}$  compared with the k factor used for the CMDL; therefore, the  $L_{CI}$  will be slightly lower than the CMDL.

Along with the CMDL, EPRI had developed a definition for the CMQL which, as we noted in Section 8.1.1, is conceptually equivalent to Currie’s  $L_D$  (detection limit). The CMQL provides both false positive (finding the substance present when it not) and false negative (not detecting it when it is present) protection. The CMQL, while not a true measure of the quantification level as defined by Currie, provides a useful measure for non-zero compliance levels that are at or below the CMDL. In those cases we will have at least 99% confidence that the true concentration is greater than the compliance limit if the measured concentration exceeds the CMQL. For the same reasons stated for the CMDL, the  $L_{DI}$  will be slightly lower than the CMQL due to the change in degrees of freedom. Thus both the CMDL ( $L_{CI}$ ) and the CMQL ( $L_{DI}$ ) may still have a role in compliance monitoring limits under specific conditions, perhaps as benchmarks to test compliance. To confidently know what the actual discharge value is, we must be at or above the quantification level. The AML was developed to provide an estimate of the true quantification level.

In its draft guidance (1) for dealing with detection and quantification levels in the National Pollutant Discharge Elimination System (NPDES), the USEPA proposed the interim ML as the method for calculating quantification levels. The interim ML, as we have shown above, is a “10 sigma” approach to computing a quantification level. The USEPA, however, has not developed a rigorous procedure for calculation, but instead has simply used a factor times the MDL. All the deficiencies associated with the MDL are thus carried over to the interim ML. Furthermore, because the MDL and ML are not based on a calibration design, which would allow estimation of the standard deviation at any concentration, the relative standard deviation at the ML is not known.

The AML is also a “10 sigma” estimate of the quantification level, but with significant computational improvements and statistical rigor to avoid the problems identified with the interim ML. The AML is defined as 10 times the interlaboratory standard deviation ( $s_{CI}$ ) at the lowest concentration that is differentiable from zero ( $L_{CI}$ ). The lowest concentration that is differentiable from zero can be statistically determined and, in the EPRI computational approach, it is anchorable, unlike the MDL which is used to compute the interim ML. Once the lowest concentration differentiable from zero is calculated, the standard deviation is computed at that concentration (using the regression expression for standard deviation versus true concentration that is developed from the interlaboratory data) and then multiplied by 10. The final steps in the computation process correct the raw “10s” value for errors in estimating the standard deviation and true concentration. The AML computational approach does not

guarantee a specific RSD, but since the standard deviation versus true concentration equation exists, the RSD at the AML can be computed and compared, for example, to a project's data quality objectives. The resulting approach has been presented to the USEPA at a recent public meeting on behalf of a coalition of interested industries (27).

Inherent in the computation of the AML is the use of the interlaboratory standard deviation and recovery data collected for at least five concentrations starting at zero and going to five times the hypothesized AML. The protocol also includes a mechanism to use intralaboratory data (developed within a single laboratory and matrix) to compute an AML where appropriate interlaboratory method validation data are not available.

The approach for calculating AMLs will depend on the availability of data. Ideally, the data used for calculating an AML should be derived from an interlaboratory data base that reflects the matrix (i.e., the chemical characteristics of the sample in which the pollutant of concern is being measured) for the effluent being analyzed. Such matrix-specific data bases already are available for certain industries. Where industry-specific interlaboratory data are not available, and time or other constraints do not allow for those data to be collected, data from an acceptable interlaboratory method study performed on reagent grade water will have to suffice. The USEPA has developed several interlaboratory data bases that could be applied to calculate AMLs.

For many pollutants, however, no acceptable interlaboratory data are available or a site may need to determine a matrix specific AML for their permit. Whether or not industry-specific interlaboratory or intralaboratory data are available, permittees should have the option of seeking a matrix-specific AML, if their particular matrix interferes with the ability of qualified laboratories to perform acceptably at a prior published AML concentration. In most of those cases, intralaboratory data are available or can be readily generated. While the standard deviation data needed to calculate AMLs cannot be obtained directly from intralaboratory data, such data together with adjustment factors to correct for the difference between interlaboratory and single operator pooled standard deviation can be used to estimate the standard deviation for calculating the AML (see Table 8-2 and section 8.4.2 for additional information).

#### **8.4.2 Computation of the AML from Interlaboratory Data**

Reference 29 describes in detail the development and computation of the AML and includes a diskette containing the AML program. An overview of the approach to compute the AML is given in Figure 8-4 in the form of a summary protocol. The following sections will provide the user with the necessary information to design an interlaboratory test program and compute an AML from the outlier free data set. Appendix B of Reference 29 provides the user with a protocol to compute an AML from intralaboratory replicate data when interlaboratory data are not available. It is expected

- A. The AML shall be calculated based on data from one of the following sources in order of priority:
1. If available, interlaboratory effluent matrix data shall be utilized for effluent-specific AML.
  2. If data in section A.1. are not available, interlaboratory data for laboratory reagent water may be utilized.
  3. If data in section A.1. or A.2. are not available, or are not appropriate, intralaboratory laboratory data for effluent matrix waters may be utilized with an appropriate correction factor to account for the ratio of interlaboratory/intralaboratory standard deviation.
  4. If data in section A.3. are not available, intralaboratory data for laboratory reagent water may be utilized with an appropriate correction factor to account for the ratio of interlaboratory/intralaboratory standard deviation.
- B. If interlaboratory data in A.1. and A.2. are utilized, the AML shall be derived as follows:
1. Derive recovery data collected for five or more concentrations starting at zero to 5 times the estimated AML from 6 or more laboratories in a blind study.
  2. Process the data using the outlier removal protocols from ASTM D2777 to produce an outlier free data set.
  3. Prepare an input file for the AML program using the outlier free data from step B.2.
  4. Under “Analysis” in the AML program select “Measured Concentration” and “Best Fit” and then select “Run.” Leave the “Screen Outliers” option off as the outliers have already been removed. The program will compute the AML and produce a chart with the  $L_{CI}$ ,  $L_{DI}$ , and the AML.
- C. If intralaboratory data in A.3. and A.4. are utilized, the AML shall be derived as follows (see (29) Appendix B for details):
1. Conduct a blind intralaboratory study. Prepare test samples at five (or more) concentrations (background plus four spikes) with a minimum of five blind replicates at each test concentration (i.e., one analyst prepares the samples and another analyzes the samples as part of their routine laboratory effort) for a total of 25 test samples.
  2. Determine background concentration using the AML program. Prepare an input file for the AML program using the data from step C.1. Under “Analysis” in the AML program select “Measured Concentration,” “Screen Outliers” and “Best Fit” and then select “Run.” The recovery equation from this first iteration of the raw data can be solved for the x-intercept, which is the background concentration in the matrix. Add the background concentration to all the raw data test concentrations.
  3. Submit the corrected data set to the AML program. Under “Analysis” in the AML program select “Measured Concentration,” “Screen Outliers” and “Best Fit” and then select “Run.” The program will compute the AML and produce a chart with the  $L_{CI}$ ,  $L_{DI}$ , and the AML.
  4. Correct the intralaboratory AML to an estimate of the interlaboratory AML by multiplying it by the appropriate interlaboratory/pooled single operator standard deviation correction factor from Table 8-2 or select a factor from the range of values given in Figure B-3 (29).

Figure 8-4 Summary of AML Test Protocol and Computation.

that the user will employ the AML program contained with the AML report (29) to compute the AML. The AML program is a Windows® based program (runs in Windows 3.1 or Win95®) developed by Gibbons (30) that will process outlier free data files or raw test data, compute the regression equation (exponential, R-L or best fit) for standard deviation and recovery and then compute the AML. The AML program will also output a worksheet containing the AML equations in order of solution with the user's data inserted and plots of the standard deviation and recovery data. Application of this program to computing AMLs will be discussed below and the user is directed to the AML User's Guide in Reference 29, Appendix C for details on installation and operation.

#### 8.4.2.1 Collection of the Interlaboratory Data

As we have described above, the AML is insensitive to the test concentrations used to compute the AML. However, the user should note that the range of spiking concentrations must be relevant for computing the AML. In general, the user should attempt to cover the range of concentrations from zero through five times the hypothesized AML. Note, however, that if blank samples are used (i.e., concentration equal to zero), approximately 50% of the measured concentrations should be negative. If the instrument censors these negative concentrations (i.e., sets them equal to zero), the estimated AML (or any other estimator including the MDL and interim ML) will be too low since only half of the true variability is observed. If this is the case, the user should configure the instrument to accept and report negative values. In the event that this is not possible, the operator can select the lowest test concentration at which the censoring of data by the instrument will not occur.

The number of laboratories and replicates depends on the source of data.

- For interlaboratory studies a minimum of 6 laboratories remaining after laboratory ranking and outlier testing are required for each level of each matrix/analyte combination. In practice this usually implies that 8-9 labs should participate in the test program to retain 6 labs. Each participant should be sent 5 Youden pair test concentrations (total of 10 samples) in the test matrix/analyte combination as blind samples. In an alternate test design, the central lab in charge of sample preparation can prepare replicate samples at each of the 5 test concentration (at least 3 replicates per test concentration for a total of at least 15 samples). A second alternative approach is to send sufficient volumes of the 5 test samples so that the laboratory can prepare its own replicates. In this latter case, different personnel should prepare and analyze the samples to maintain the blind nature of the test program.
- When only a single laboratory is performing an AML study, a minimum of 5 test concentrations with 5 blind replicates for each level in the test matrices should be run (a total of 25 samples). Additional test concentrations and replicates can be run if the user chooses. These samples must be prepared as blind samples by someone other than the analyst, randomized and spread over several days while labeled and

analyzed as routine samples. See Appendix B (29) for details on the test design and data analysis protocol for estimating the AML from intralaboratory data.

In both cases the samples should be placed in the laboratory as routine samples to accurately reflect the normal variability and bias in the laboratory.

#### **8.4.2.2 Testing for Outliers in the Data Sets**

All of the data in this report were first processed through EPRI's software program STATCALC (preliminary research grade) to remove laboratories with consistent bias (lab ranking) and individual outliers (described in Section 6). STATCALC is an implementation of ASTM D2777. Reference 31 describes in detail the D2777 lab ranking and outlier rejection protocol and the procedure was summarized in Section 6. The user can choose to implement the D2777 protocol manually or assisted by a spreadsheet program of their design. They may also request a copy of STATCALC from EPRI by contacting the EPRI Project Manager, Dr. Babu Nott.

For interlaboratory studies we recommend that the D2777 outlier rejection protocol be followed. The resulting outlier free data sets can then be formatted and loaded into the AML program, which uses a spreadsheet-like format for manual data loading or can accept formatted text files directly (see AML User's Guide (29) for further details). For intralaboratory studies, the raw data from the study can be loaded into the AML program and the outlier rejection option selected. The AML program will automatically perform an outlier test on the data and compute the AML. It is not recommended that the outlier test in the AML program be used to process data from interlaboratory studies, because it will not reject labs which consistently perform poorly on the test matrices.

#### **8.4.2.3 Computation of the AML**

The computation approach described in this section is specifically intended for use where the true concentration of all five sample levels is known. Figure 8-4 provides an overview of how to compute an estimate of the AML from intralaboratory data; part of which requires determining the concentration of the background. Appendix B of Reference 29 provides a detailed protocol for computing an AML using intralaboratory data including determining the background concentration. When interlaboratory data are used, the grand mean of the background concentration is taken as the true concentration and the remaining test concentrations are computed by adding the spike concentrations to the background concentration.

The computation approach described in this section can be implemented with the standard deviation versus true concentration data expressed in either the exponential or the R-L form (Section 8.3). The AML program is designed to test for the best fit between the exponential and R-L model for standard deviation versus true concentration. In

most cases the R-L model will provide the best fit; however, the user can visually verify the fit of either the exponential or the R-L model by selecting it from the menu. For this example, we will use the R-L equations to describe the AML computation process.

The outlier free data set is analyzed to produce expressions of the interlaboratory standard deviation versus true concentration and mean concentration versus true concentration. The interlaboratory standard deviation versus true concentration in the R-L format is:

$$s_t = (a_0 + a_1 T^2)^{1/2} \quad (\text{eq. 114})$$

where  $s_t$  is the interlaboratory standard deviation from the validation study and  $T$  is the true concentration of the test samples. The recovery equation is a linear regression equation in the form of:

$$X = b_0 + b_1 T \quad (\text{eq. 115})$$

where  $X$  is the measured concentration. Once the interlaboratory standard deviation data are expressed by equation 115 (or an exponential model), the calculation of the AML can proceed in the following manner:

1. The first step is to compute  $Y_{CI}$  which is defined as the upper 95% confidence 99% coverage tolerance limit for measured concentrations when the true concentration is zero:

$$Y_{CI} = k s_t + b_0 \quad (\text{eq. 116})$$

where  $k$  is the tolerance factor for 95% confidence, 99% coverage and the degrees of freedom,  $n$ , are equal to the number of data points at each concentration summed over all concentrations levels.

2. Substitute the interlaboratory regression equation for  $s_t$  and set  $T$  to  $Y_{CI}$  and solve for  $Y_{CI}$ :

$$Y_{CI} = k \left( a_0 + a_1 \left( (Y_{CI} - b_0) / b_1 \right)^2 \right)^{1/2} + b_0 \quad (\text{eq. 117})$$

which requires an iterative solution. The recovery equation (eq. 116) is used to convert all computation involving the standard deviation from a mean concentration estimate (standard deviation is based on the actual data collected) to a true value.



3. Since  $Y_{CI}$  is computed from the standard deviation (a measured value), it is a measured concentration.  $L_{CI}$  is the corresponding true concentration:

$$L_{CI} = (Y_{CI} - b_0) / b_1 \quad (\text{eq. 118})$$

4. Once the  $L_{CI}$  is found, compute  $s_{CI}$ , the interlaboratory standard deviation at the  $L_{CI}$ , using equation (14):

$$s_{CI} = \left( a_0 + a_1 (L_{CI})^2 \right)^{1/2} \quad (\text{eq. 119})$$

5. Compute the average instrument response (in measurement units) at 10 times the  $s_{CI}$  as:

$$Y_{QI} = 10s_{CI} + b_0 \quad (\text{eq. 120})$$

Note that  $b_0$  is added to  $10s_{CI}$  to convert  $Y_{QI}$  into a measured concentration instead of response variation.

6. Since  $Y_{QI}$  is derived from a factor times the standard deviation ( a measured value) at the  $L_{CI}$ , the recovery equation (15) is used to correct  $Y_{QI}$  to the corresponding true concentration:

$$T_{QI} = (Y_{QI} - b_0) / b_1 \quad (\text{eq. 121})$$

7. Finally, estimate the AML by approximating the upper 95% prediction limit for a single new measurement at  $T_{QI}$ :

$$AML \approx T_{QI} + (ts_{T_{QI}} / b_1) \quad (\text{eq. 122})$$

where  $t$  is the upper 95th percentile of Student's  $t$ -distribution  $n-2-p$  degrees of freedom (where  $n$  is the number of data points as defined in step 1),  $p$  is the number of unknown parameters in the standard deviation model and  $s_{T_{QI}}$  is the interlaboratory standard deviation at  $T_{QI}$  computed by:

$$s_{T_{QI}} = \left( a_0 + a_1 (T_{QI})^2 \right)^{1/2} \quad (\text{eq. 123})$$

Note equation (22) is a good approximation of the true prediction limit found in the AML program when  $n > 25$  which is the case for interlaboratory validation studies. Figure 8-4 summarizes the AML calculation protocol.

Using the interlaboratory precision data, the equivalent of the Currie detection level,  $L_{DI}$ , can be computed. The  $L_{DI}$  will control both Type I and II errors when the true concentration is equal to  $L_{DI}$ . Operationally, the  $L_{DI}$  is computed in the following steps:

$$Y_{DI} = Y_{CI} + ks_{L_{DI}} \quad (\text{eq. 124})$$

substituting the R-L regression equation for  $s_{L_{DI}}$  and using  $Y_{DI}$  to represent mean concentrations:

$$Y_{DI} = Y_{CI} + k \left( a_0 + a_1 \left( (Y_{DI} - b_0) / b_1 \right)^2 \right)^{1/2} \quad (\text{eq. 125})$$

$Y_{DI}$  is converted to a true concentration using the recovery equation (116):

$$L_{DI} = (Y_{DI} - b_0) / b_1 \quad (\text{eq. 126})$$

This definition is equivalent to the EPRI CMQL(Z) developed earlier.

## 8.5 Determining Regulatory Compliance

The AML, as an estimate of the quantification level,  $L_Q$ , can be applied to two general regulatory cases: (1) the compliance limit is at a quantifiable level (i.e., the standard is equal to or greater than  $L_Q$ ) and (2) the compliance limit is below the quantification level (e.g., some water quality-based effluent limitations).

### 8.5.1 Regulatory Compliance Limit Greater Than or Equal to the Quantification Level

If the permit regulatory compliance limit (RCL) is at a quantifiable level (i.e.,  $RCL \geq L_Q$ ), then any measurement that exceeds the RCL also exceeds  $L_Q$ . Therefore, the measurement is quantifiable and its concentration can be directly compared to the standard. A measurement above the standard indicates noncompliance.

### 8.5.2 Regulatory Compliance Limit Below the Quantification Level

In the draft guidance (1) for dealing with detection and quantification levels in the National Pollutant Discharge Elimination System (NPDES) for setting and determining compliance with water quality-based effluent limitations (WQBEL), the USEPA has proposed that when measured data are below the quantification level:

- Zero would be reported in place of all such data
- Quantification level would be computed using the interim Minimum Level (ML).

As it has been shown in the preceding sections, the ML has a number of serious deficiencies that the AML corrects. The AML is proposed as a direct replacement for the ML in permits requiring compliance with limits set below the quantification level.

## 8.6 ASTM Interlaboratory Detection Estimate (IDE)

EPRI has been directly involved in the development of consensus approaches to define detection and quantification in a manner that is relevant to industry's needs. As discussed in Section 8.4, EPRI played a key role with the IIAG in developing the Alternative Minimum Level which provides a scientifically based alternative to the EPA's proposed interim Minimum Level. In parallel with the AML development, EPRI participated in the American Society of Testing and Materials (ASTM) task group D19.02.04.07 and helped develop the Interlaboratory Detection Estimate (IDE) (32). The IDE addresses all of the problems with the MDL outlined in Section 8.2 and provides the utility industry with a true consensus standard for detection for use in their permits.

The IDE is defined as "the lowest concentration at which there is 90% confidence that a single measurement from a laboratory selected from the population of qualified laboratories represented in an interlaboratory study will have a true detection probability of a least 95% and a true non-detection probability of at least 99%" (32). It is an implementation of the basic principles for detection outlined by Currie (2) combined with the general approaches advocated by developers of calibration based detection levels. A measured critical level is computed from the standard deviation data and corrected to a true concentration using the recovery equation. A detection level is then computed. The key feature of the IDE is that it is based on interlaboratory standard deviation models and it uses tolerance limits to address the issue of estimating performance of multiple laboratories in the future. As an interlaboratory estimate of the detection level, the IDE can be used in compliance monitoring situations involving permit limitations expressed in terms such as "no detectable discharge". For a detailed presentation on the procedure by which to calculate the IDE, see reference 32: ASTM D6091 "Standard Practice for a 99%/95% Interlaboratory Detection Estimate (IDE) for Analytical Methods with Negligible Calibration Error."

The IDE and AML share a common heritage based on Currie, though they address two different issues: detection (IDE) and quantification (AML), respectively. Both use interlaboratory test data and similar models for characterizing standard deviation vs. concentration data. They both compute an  $L_c$  using a similar approach, though at slightly different tolerance limits. Together, they represent a serious effort by credible institutions to address the shortcomings in the EPA definitions for detection (MDL) and quantification (interim ML).

Building on the success of the IDE effort, ASTM is working on the development of an interlaboratory quantification estimate. EPRI will participate in that work. The AML may serve as a suitable approach for consideration by ASTM in the development of an interlaboratory quantification estimate.

## 8.7 Acknowledgments

Portions of this section were excerpted from Koorse (27), which was prepared collectively by Dr. Robert D. Gibbons, Professor of Biostatistics, University of Illinois; Dr. Raymond F. Maddalone, TRW; Mr. David E. Coleman, Alcoa; Dr. Babu Nott, Electric Power Research Institute; Mr. Larry LaFleur, National Council of the Paper Industry for Air and Stream Improvement, Inc.; and James K. Rice, P.E. Their work was sponsored by American Automobile Manufacturers Association, American Forest & Paper Association, Chemical Manufacturers Association, Electric Power Research Institute, National Association of Metal Finishers, American Electroplaters and Surface Finishers Society, Utility Water Act Group, and Alcoa.

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# 9

## SUMMARY OF AMLS COMPUTED FROM THE TEST DATA

In the preceding section, the approach to computing the  $L_{CI}$ ,  $L_{DI}$  and the Alternative Minimum Level (AML) was presented. Utilizing those procedures, the data from the AMQ-IV Round 2 test program were used to compute the  $L_{CI}$ ,  $L_{DI}$ , AML and the RSD at the AML. The results of that analysis are shown in Table 9-1. These data are compared with the EPA-quoted detection limit for each method and the freshwater Water Quality Criteria (WQC) (1) for each element. The following sections will discuss the findings for each element separately.

**Table 9-1**  
**Summary of Alternative Minimum Levels for Arsenic, Cadmium and Chromium by GFAAS for AMQ-IV Round 2**

Element	Matrix	Lower Test Conc (µg/L)	Upper Test Conc (µg/L)	$L_{CI}$ (µg/L)	$L_{DI}$ (µg/L)	Curve Fit RL	Exp	RSD <sup>1</sup> %	AML (µg/L)	EPA DL <sup>2</sup> (µg/L)	WQC <sup>3</sup> (µg/L)
As	RGW	4.4	98.6	2.9	5.9		X	9.3	13.7	1	190
As	GW	0.09	91.3	5.0	10.6	X		11.7	28.8	1	190
As	EST	5.4	859	18.2	39.2		X	13.4	92.9	1	190
As	AMD	8.3	942	41.6	88.9		X	13.1	213	1	190
Cd	RGW	0.01	9.5	0.25	0.51		X	9.4	1.2	0.1	1.0
Cd	GW	0.04	10.3	0.43	0.98		X	16.1	2.3	0.1	1.0
Cd	EST	0.17	97.1	2.79	7.1		X	19.8	15.8	0.1	1.0
Cd	AMD	3.5	92.8	4.1	9.2		X	15.8	21.7	0.1	1.0
Cr	RGW	0.35	91.4	2.1	4.3		X	10.5	10.4	1	10 (hex)

**Table 9-1**

**Summary of Alternative Minimum Levels for Arsenic, Cadmium and Chromium by GFAAS for AMQ-IV Round 2**

Element	Matrix	Lower Test Conc (µg/L)	Upper Test Conc (µg/L)	L <sub>CL</sub> (µg/L)	L <sub>DL</sub> (µg/L)	Curve Fit RL Exp	RSD <sup>1</sup> %	AML (µg/L)	EPA DL <sup>2</sup> (µg/L)	WQC <sup>3</sup> (µg/L)
Cr	GW	0.47	100	2.6	5.4	X	11.4	13.1	1	10 (hex)
Cr	EST	2.7	955	18.7	39.4	X	11.9	93.5	1	10 (hex)
Cr	AMD	4.7	1001	15.4	34.1	X	15.0	80.8	1	10 (hex)

<sup>1</sup> RSD = Relative Standard Deviation at the AML

<sup>2</sup> Detection Limit, Methods for Chemical Analysis of Water and Wastes (EPA 600/4-79-020, Revised March 1983)

<sup>3</sup> Water Quality Criteria, Freshwater Criteria Continuous Concentration expressed as dissolved (60FR22236, May 4, 1995), 100 mg/L hardness where applicable

RGW = Reagent Grade Water, GW = Groundwater, EST = Estuarine, AMD = Acid Mine Drainage

## 9.1 Arsenic

The freshwater Criteria Continuous Concentration (CCC) water quality criteria for arsenic is 190 µg/L. The L<sub>DL</sub>s (Figure 9-1) and AMLs (Figure 9-2) for arsenic were lower than the water quality criteria for all of the study matrices except the AML for acid mine drainage, which was 213 µg/L.

The L<sub>DL</sub> for arsenic in reagent grade water was 5.9 µg/L compared to the EPA-quoted detection limit for the method of 1 µg/L. The L<sub>DL</sub>s and AMLs were lowest for reagent grade water, followed by groundwater, estuarine and acid mine drainage, in that order.

The Relative Standard Deviations (RSDs) at the AML for arsenic were very good, ranging from 9.3 to 13.4%. As a general rule, something that is considered quantified exhibits an RSD of 10 to 20% at these concentrations.



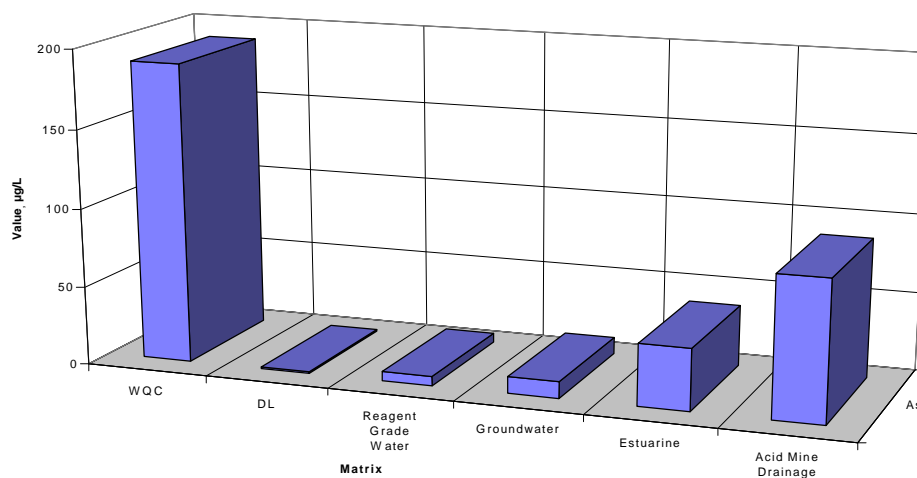


Figure 9-1 Comparison of Arsenic  $L_{DI}$ s by Matrix to WQC and DL

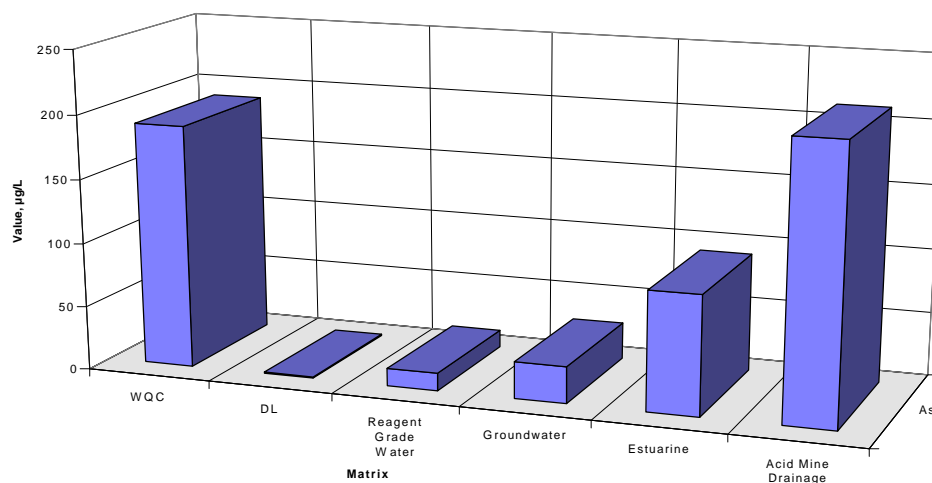


Figure 9-2 Comparison of Arsenic AMLs by Matrix to WQC and DL

## 9.2 Cadmium

A comparison of the cadmium  $L_{DI}$ s to the freshwater CCC water quality criteria and the detection limit quoted in the method is shown in Figure 9-3. The  $L_{DI}$ s for reagent grade water and groundwater were lower than the water quality criteria. The  $L_{DI}$ s for the more complex matrices, estuarine and acid mine drainage, were a factor of approximately 7 and 9 times higher than the water quality criteria. The  $L_{DI}$  for reagent grade water, 0.51  $\mu\text{g/L}$ , was 5 times higher than the detection limit of 0.1  $\mu\text{g/L}$  quoted in the EPA method.

The AMLs obtained for the cadmium data are illustrated in Figure 9-4. The cadmium AMLs ranged from 1.2  $\mu\text{g/L}$  for reagent grade water to 21.7  $\mu\text{g/L}$  for acid mine drainage. The AMLs obtained for all four matrices were higher than the water quality criteria of 1.0  $\mu\text{g/L}$ , however the AML for reagent grade water, 1.2  $\mu\text{g/L}$  was only slightly higher. The RSDs at the AML were in the 10 to 20% range.

### 9.3 Chromium

The  $L_{DI}$ s for chromium in reagent grade water and groundwater were lower than the water quality criteria of 10  $\mu\text{g/L}$  for hexavalent chromium (Figure 9-3). The  $L_{DI}$ s for estuarine and acid mine drainage were approximately 3 times higher than the water quality criteria. The  $L_{DI}$  for reagent grade water, 4.3  $\mu\text{g/L}$ , was approximately 4 times higher than the detection limit of 1  $\mu\text{g/L}$  quoted in the EPA method.

The AMLs for chromium in reagent grade water and groundwater were slightly higher than the water quality criteria. The AMLs for estuarine and acid mine drainage were considerably higher. The RSDs at the AML were in the 10 to 15% range.

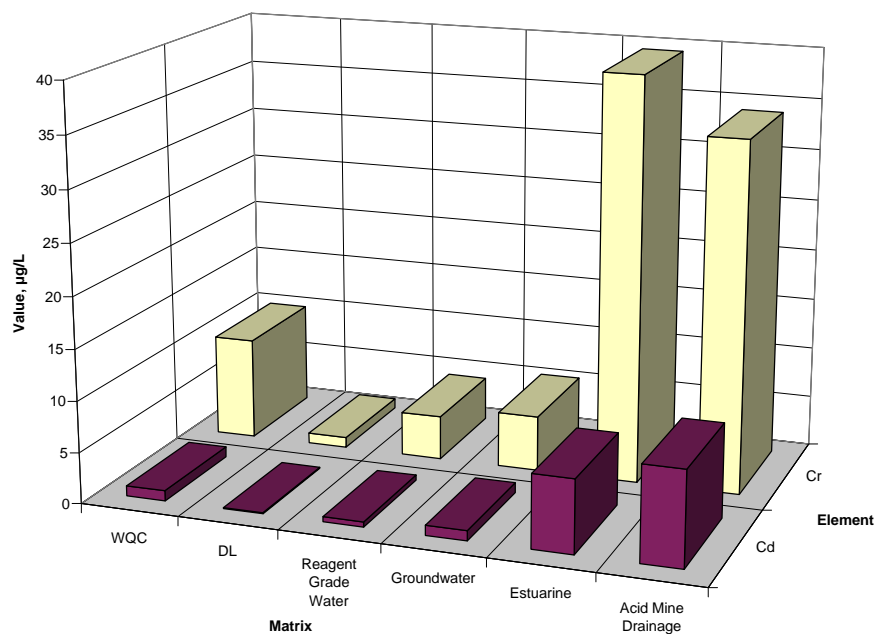


Figure 9-3 Comparison of Cadmium and Chromium  $L_{DI}$ s by Matrix to WQC and DL

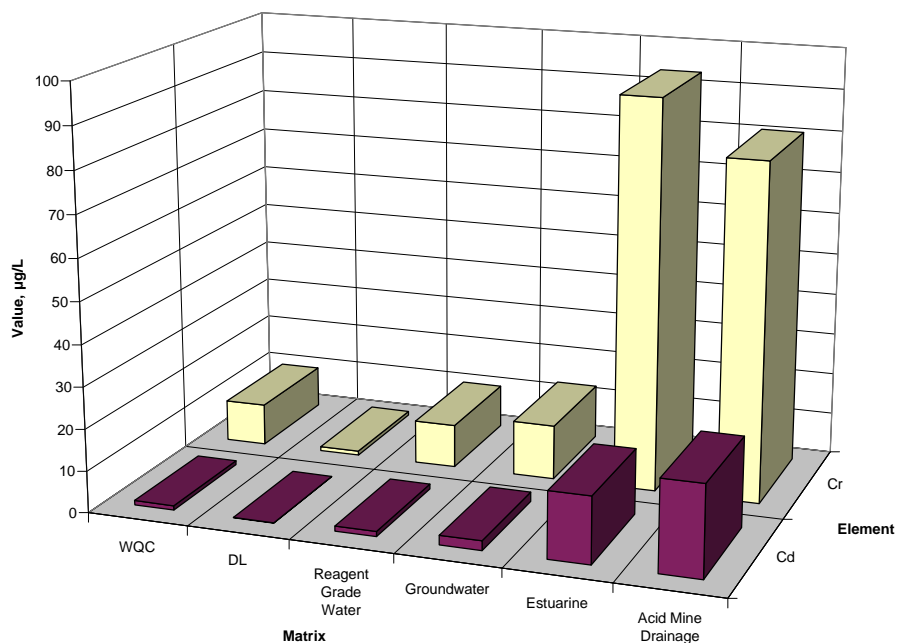


Figure 9-4 Comparison of Cadmium and Chromium AMLs by Matrix to WQC and DL

#### 9.4 References

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# 10

## CONCLUSIONS

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Based on the results of the AMQ-IV validation effort, the following conclusions can be made:

- For all elements, the samples prepared by the spike and split approach taken in this project were stable over the period of time (three months) required to complete the validation effort.
- Participants were qualified to perform the analyses:
  - Over half of the GFAAS analysts had five or more years' experience, with nearly half of these having in excess of ten years' experience.
  - Seventy-two percent of the supervisors had BA/BS degrees and seventy-seven percent had more than ten years of experience.
  - Seventy-eight percent of the analysts had at least a Bachelor's degree in chemistry, biology or a related field of study.
- Ninety percent of the participants used autosamplers for sample introduction.
- Seventy-two percent of the laboratories used platform furnace instruments for all analytes, eleven percent used tube graphite furnace for all analytes, and seventeen percent used platform graphite furnace for some analytes and tube graphite furnace for others.
- All of the participants used commercially prepared standard reference materials for instrument calibration.
- Eighty percent of the data sets tested normal by the Shapiro/Wilk normality test. A normal data distribution is important since it is the basic assumption in the type of statistics that are used to reduce the data.
- Most of the data points removed were lost in the laboratory ranking step. Overall, the average outlier removal rate by laboratory ranking was 14.9%. An additional average of 2.6% of the data was removed by the individual outlier removal process.
- Recoveries of arsenic and chromium in all matrices were within  $\pm 10\%$  for all matrices. Cadmium recoveries were within  $\pm 20\%$  for all matrices.
- RSDs at the AML were in the 10 to 15% range for arsenic and chromium and in the 10 to 20% range for cadmium.
- Table 10-1 summarizes the performance of the methods against the detection limit quoted in the EPA method (DL) and the EPA freshwater water quality criteria

## Conclusions

(WQC). All of the calculated  $L_{DL}$ s were higher than the corresponding detection limit published in the method. Three of the arsenic were lower than the corresponding water quality criteria.

**Table 10-1**  
**Summary of As, Cd and Cr  $L_{DL}$ s and AMLs**  
**Compared to EPA Criteria**

Element	Matrix	DL <sup>1</sup>	WQC <sup>2</sup>
Arsenic	Reagent Grade Water	H	L
Arsenic	Groundwater	H	L
Arsenic	Estuarine	H	L
Arsenic	Acid Mine Drainage	H	H
Cadmium	Reagent Grade Water	H	H
Cadmium	Groundwater	H	H
Cadmium	Estuarine	H	H
Cadmium	Acid Mine Drainage	H	H
Chromium	Reagent Grade Water	H	H
Chromium	Groundwater	H	H
Chromium	Estuarine	H	H
Chromium	Acid Mine Drainage	H	H

L = lower than criteria, H = higher than criteria

<sup>1</sup>  $L_{DL}$  compared to DL

<sup>2</sup> AML compared to WQC

# A

## NOMENCLATURE

---

Table A-1  
Nomenclature Used in This Report

Abbreviation	Description
AAS	Atomic Absorption Spectroscopy
ACL	Acceptance Limits
ACS	American Chemical Society
Ag	Silver
AMQ	Analytical Methods Qualification
AML	Alternative Minimum Level
APO	Ash Pond Overflow
Al	Aluminum
As	Arsenic
ASTM	American Society for Testing and Materials
B	Boron
Ba	Barium
Be	Beryllium
Ca	Calcium
Cd	Cadmium
CFR	Code of Federal Regulations
CMDL	Compliance Monitoring Detection Level
CMQL	Compliance Monitoring Quantitation Level
Co	Cobalt
Cr	Chromium

## Nomenclature

Table A-1  
Nomenclature Used in This Report

Abbreviation	Description
Cu	Copper
CVAAS	Cold Vapor AAS
DL	Detection Limit
DMR/QA	Discharge Monitoring Report/Quality Assurance
EMSL	Environmental Monitoring and Support Laboratory
EPA	Environmental Protection Agency
Fe	Iron
FLAAS	Flame AAS
FR	Federal Register
FW	Freshwater
GFAAS	Graphite Furnace AAS
GHAAS	Gaseous Hydride AAS
HCl	Hydrochloric Acid
Hg	Mercury
HNO <sub>3</sub>	Nitric Acid
ICP-AES	Inductively Coupled Plasma - Atomic Emission Spectroscopy
ICP-MS	Inductively Coupled Plasma - Mass Spectrometry
IDL	Instrument Detection Limit
K	Potassium
L <sub>c</sub>	Critical Level (Currie)
L <sub>cl</sub>	Interlaboratory Critical Level
L <sub>d</sub>	Detection Level (Currie)
L <sub>dl</sub>	Interlaboratory Detection Level
L <sub>q</sub>	Determination Level (Currie)
LDRF	Laboratory Data Reporting Form
Li	Lithium



Table A-1  
Nomenclature Used in This Report

Abbreviation	Description
LOD	Limit of Detection
LOQ	Limit of Quantitation
MCAW	<i>Methods for Chemical Analysis of Water and Wastes</i> , EPA 600/4-79-020 (Revised March 1983)
MCLG	Maximum Contaminant Level Goal
MDL	Method Detection Limit
Mg	Magnesium
ML	Minimum Level
Mn	Manganese
Mo	Molybdenum
MPRF	Method Parameters Reporting Form
NCWD	Non-Cooling Water Discharge
Na	Sodium
Ni	Nickel
NPDES	National Pollution Discharge Elimination System
Pb	Lead
PQL	Practical Quantitation Level
RCL	Regulatory Compliance Limit
R-L	Rocke-Lorenzato
RGW	Reagent Grade Water
RSD	Relative Standard Deviation
RW	River Water
SAUP	Sampling and Analysis of Utility Pollutants
Se	Selenium
Sn	Tin
Sr	Strontium

---

*Nomenclature*

Table A-1  
Nomenclature Used in This Report

<b>Abbreviation</b>	<b>Description</b>
SWD	Seawater Discharge
SWI	Seawater Intake
TCMCW	Treated Chemical Metal Cleaning Waste
TDS	Total Dissolved Solids
Ti	Titanium
Tl	Thallium
UWAG	Utility Water Act Group
V	Vanadium
WQBEL	Water Quality-Based Effluent Limitation
WQC	Water Quality Criteria
Zn	Zinc

# ***B***

## **LABORATORY CONTACT WORKSHEET**

---

AMQ-TC

LABORATORY CONTACT WORKSHEET

1. Utility: \_\_\_\_\_

2. Business Address \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

3. Shipping Address \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

4. Key Contact/Title: \_\_\_\_\_

5. Telephone: \_\_\_\_\_

6. Alternate Contacts:

Name	Phone Number
_____	_____
_____	_____

7. EPRI Member? Yes \_\_\_\_\_ No \_\_\_\_\_

8. Can you participate in the program? Yes \_\_\_\_ No \_\_\_\_

Comments: \_\_\_\_\_

9. Overload time of year? \_\_\_\_\_

10. Turnaround time? \_\_\_\_\_

11. GFAAS

<u>Metal</u>	<u>Monitor?</u>	<u>Routine?</u>	<u>Monitor for Permit?</u>	<u>Det Lim</u>
As	_____	_____	_____	_____
Cd	_____	_____	_____	_____
Cr	_____	_____	_____	_____

12. GHAAS

As \_\_\_\_\_

13. Background Correction: \_\_\_\_\_

14. Matrices:

"Clean" Groundwater	_____
Acid Mine Drainage	_____
Estuarine Groundwater	_____
Reagent Grade Water	_____

15. Source of procedures currently used:

MCAW \_\_\_\_\_ Standard Methods \_\_\_\_\_  
 MDMES\* \_\_\_\_\_ Other \_\_\_\_\_

\* Methods for the Determination of Metals in Environmental Samples June 1991

16. Problems with / Modifications to Method \_\_\_\_\_  
 \_\_\_\_\_

17. Other utilities that might want to participate?

<u>Name</u>	<u>Contact</u>
_____	_____
_____	_____
_____	_____

# C

## **INSTRUCTIONS TO PARTICIPANTS**

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*Instructions to Participants*

TO: AMQ-TC - PARTICIPANTS

FROM: N. T. Whiddon / J. W. Scott

SUBJECT: Instructions for AMQ-TC Test Program

With this memo we are sending you the samples to be analyzed in the Analytical Methods Qualification - Tailored Collaboration(AMQ-TC) project. Both my staff and Babu Nott, the EPRI Project Manager, greatly appreciate the cooperation you have shown in committing to complete these analyses.

PLEASE READ THE COMPLETE INSTRUCTION PACKET BEFORE BEGINNING THE ANALYSES. It is important that all participating laboratories have the same information in order for the results to be valid.

If you have any questions, don't hesitate to contact Nina Whiddon (310-813-9351) or Judy Scott (310-813-9321).

We would like all results returned by November 18, 1994 to:

Nina Whiddon  
TRW  
One Space Park, 01/2070  
Redondo Beach, CA 90278

These results should include:

- 1) The completed Laboratory Data Reporting Forms for each sample. Make a copy for your records.
- 2) The completed Method Parameters Reporting Form.
- 3) The completed Laboratory Equipment and Practices Form.

We look forward to receiving your results.



TO: EPRI Analytical Method Qualification (AMQ) Participants

SUBJECT: Instructions for Determination of AMQ-TC Elements

Thank you for volunteering to participate in the AMQ-TC project.

PLEASE READ THESE INSTRUCTIONS BEFORE REMOVING SAMPLE BOTTLES  
FROM THE SHIPPING CARTON.

### Project Goals

The goal of this project is to collect "real world" precision and bias data on analytical methods used by the utilities for utility matrices. To meet this objective, the analyses you perform for this project should be as representative of your routine analyses as possible. This means that there is no need to run practice determinations and all data should be regarded as valid. The intent is not to test your laboratory, but to develop a data base on the capabilities of the methods available for utility use.

All data will be coded for reporting purposes.

This instruction packet is organized into 5 parts as follows:

- Part 1. Overview of Elements and Matrices
- Part 2. Sample Preparation and Analytical Procedures
- Part 3. QA/QC Requirements
- Part 4. Explanation of Reporting Requirements
- Part 5. Explanation of Bottle Coding

### Part 1. Overview of Elements and Matrices

In this round of the EPRI AMQ project you have been sent the following sets of test matrices:

- Reagent Grade Water
- Freshwater
- Estuarine Water
- Acid Mine Drainage

For each matrix, there are ten sample bottles.

A separate Laboratory Data Reporting Form is included for each sample. Please ensure that the samples you receive match those on the Reporting Forms. It is important that you note on the form the condition of each sample upon arrival. In the event that any precipitate has formed in the samples or if there is evidence of leakage, please contact TRW for discussion of whether a replacement sample is needed.

## Part 2. Sample Preparation and Analytical Procedures

The procedures provided are from the EPA Methods for Chemical Analysis of Water and Wastes, (EPA-600/4-79-020, revised March 1983).

"Metals - Atomic Absorption Methods" - general description from Methods for Chemical Analysis of Water and Wastes (MCAW)

Arsenic- MCAW Method 206.2, Atomic Absorption, Furnace Technique

Cadmium - MCAW Method 213.2, Atomic Absorption, Furnace Technique

Chromium - MCAW Method 218.2, Atomic Absorption, Furnace Technique

For the purposes of interpretation of the round-robin test data, it is important that all procedures be followed exactly.

**NOTE: CALL TRW BEFORE USING PROCEDURES OR METHODS DIFFERENT FROM THOSE SPECIFIED!**

Digestion. The EPA method for arsenic includes a hydrogen peroxide digestion. TRW conducted a research study to determine if the peroxide digestion would be necessary for this study since a separate digestion for arsenic would significantly impact the workload of our volunteer laboratories. The study determined that the peroxide digestion is not necessary for the determination of arsenic in the AMQ-TC matrices. A single nitric acid digestion is sufficient for all three test elements.

The digestion procedure which will be used in this study is that designated for "total recoverable metals" in Section 4.1.4 of the MCAW general "Metals" write-up. Although this procedure calls for the addition of 5 mL/L HNO<sub>3</sub> at the time of sample collection/preparation, shipping restrictions made this impractical. Instead each sample was preserved by adding nitric acid to give a pH of 2 or

less (maximum  $\text{HNO}_3$  concentration approximately 0.15% by volume). Therefore, 0.5 mL of concentrated redistilled  $\text{HNO}_3$  should be added to each 100 mL digest aliquot before heating.

**NOTE: HYDROCHLORIC ACID WILL NOT BE ADDED TO DIGEST ALIQUOTS BECAUSE OF ITS INTERFERENCE WITH FURNACE ANALYSIS.**

Each element being analyzed in this study requires different matrix modifiers. Please use the accompanying "Recommended AMQ-TC Sample Aliquots" flowchart as a guide in preparing your samples for analysis.

Each sample will be analyzed once beginning with the digestion step. A laboratory reagent blank should be digested and analyzed with each lot of samples prepared for analysis.

In some previous cases, a light precipitate has been reported either on arrival or after digestion. Agitate the sample bottle before taking a sample to ensure a well mixed and representative aliquot. If the amount of precipitate seems excessive, call TRW for advice. **DO NOT FILTER THE SAMPLE BEFORE DIGESTION.** The EPA procedure for "total recoverable metals" permits filtration of the sample after digestion to remove precipitates.

A precipitate may form during the digestion step, particularly for the high dissolved solids samples (Estuarine Water and Acid Mine Drainage). **DO NOT FILTER THE DIGESTED SAMPLE BEFORE IT HAS BEEN DILUTED TO FINAL VOLUME.** After the sample has been diluted to 100 mL, you may filter the sample if necessary.

Test Concentrations. For the two simplest matrices, Freshwater and Reagent Grade Water, test concentrations were selected to remain between the natural background level and the upper end of the optimum concentration range stated in the method if background concentrations permitted. Depending on the background concentrations of the elements of interest, it may be necessary to dilute some of these samples in order to remain within the linear range of the calibration curve.

The more complex matrices, Estuarine Water and Acid Mine Drainage have high total dissolved solids values which require that they be diluted for GFAAS analysis. Accordingly, these matrices

have been spiked to allow a 1:10 dilution. All sample sets include at least one unspiked background sample that may have very low concentrations of the analytes of interest.

### Part 3. QA/QC Instructions

Following are the QA/QC instructions for the AMQ-TC study. If your laboratory has a QA/QC program in place for GFAAS that provides equivalent quality assurance and quality control, you may use your normal procedures.

#### 3.1 Labware

For trace elemental analysis, it is very important that all labware that comes in contact with the samples and standards be thoroughly cleaned. This includes sample containers, volumetric flasks, etc. The choice of cleaning methods is left up to the analyst as long as it can be demonstrated that the procedure does not cause any interference with the analyses.

#### 3.2 Reagents

Acid - Due to the high sensitivity of GFAAS, only highest purity nitric acid should be used to acidify the samples and standards. Ultrex Ultrapure Reagent nitric acid has been found to be suitable.

Water - ASTM Type I water (ASTM D1193) or equivalent is required for analysis.

Standard Stock Solutions - Standard stock solutions may be prepared according to the enclosed EPA Metals Methods or purchased from a reputable commercial supplier.

#### 3.3 Standardization

The initial standardization should consist of a solvent blank (reagent water with 0.5% redistilled nitric acid) and a minimum of three standards. The standardization should be verified by analyzing an independent quality control sample. Recovery should be +/- 10 percent of the certified value.

### 3.4 Standardization Checks

A standardization blank and standardization independent quality control sample should be analyzed every 10 samples. If the measured concentration exceeds  $\pm 10$  percent of the true concentration, the analysis should be stopped and the source of error identified. All analyses since the last valid standardization check should be repeated. If the sample matrix is causing the drift, it may be necessary to perform standard additions to analyze the samples. See Section 8.5 of the EPA Metals Method (Metals for Chemical Analysis of Water and Wastes).

### 3.5 Spike Recovery

At least one spiked sample should be analyzed with each set of samples. Spike recovery should be within  $\pm 10$  percent.

### 3.6 Calculations

Be sure to include all dilution factors in your calculations!

## Part 4. Explanation of Reporting Requirements

Before analyses are begun, it is important to examine the "Laboratory Data Reporting Form," "Method Parameters Reporting Form," and "Laboratory Equipment and Practices Survey," so that all information requested can be provided.

The digestion step will be performed on all test matrices, including the reagent grade water set. All samples will be analyzed only once each. This approach is required to assess the accuracy and precision of all phases of the procedure. If multiple injections or standard additions are used for a particular sample, report only a single average value for each concentration. Report both values for the matrix background sample. Where possible, please report at least three significant figures for each analytical result.

REPORT THE ACTUAL VALUE CALCULATED FOR THE SAMPLE CONCENTRATION, EVEN IF IT IS BELOW THE DETECTION LIMIT. THIS INCLUDES ZERO AND NEGATIVE VALUES.

At the conclusion of the testing, you will have an opportunity to compare your results with the averaged results of all the participating laboratories. Please retain all original data, including multiple injection or standard addition values, to facilitate follow-up review.

#### Part 5. Explanation of Bottle Coding

The bottle codes are designed for simple identification of sample matrix and test concentration level and to facilitate computer manipulation of test results. The several parts of the code are described in Figure 1. The first three digits comprise a code unique to your laboratory and should appear on each sample you receive. Each laboratory will be identified only by its code in the final summary of results. The two-digit Matrix Code is to facilitate your sorting of samples; matrix types and code numbers are listed on the Test Label. As a further aid to sorting the samples, the Test Labels have been color coded. All samples from a particular matrix have the same color label. The letter code is a randomly assigned code for concentration level. Youden pair studies do not permit the analyst to know the relative concentration of the test samples, so this code has meaning only for TRW. Do not try to "sort" the concentration levels alphabetically. The final two digits are for traceability of the bottle fill order.

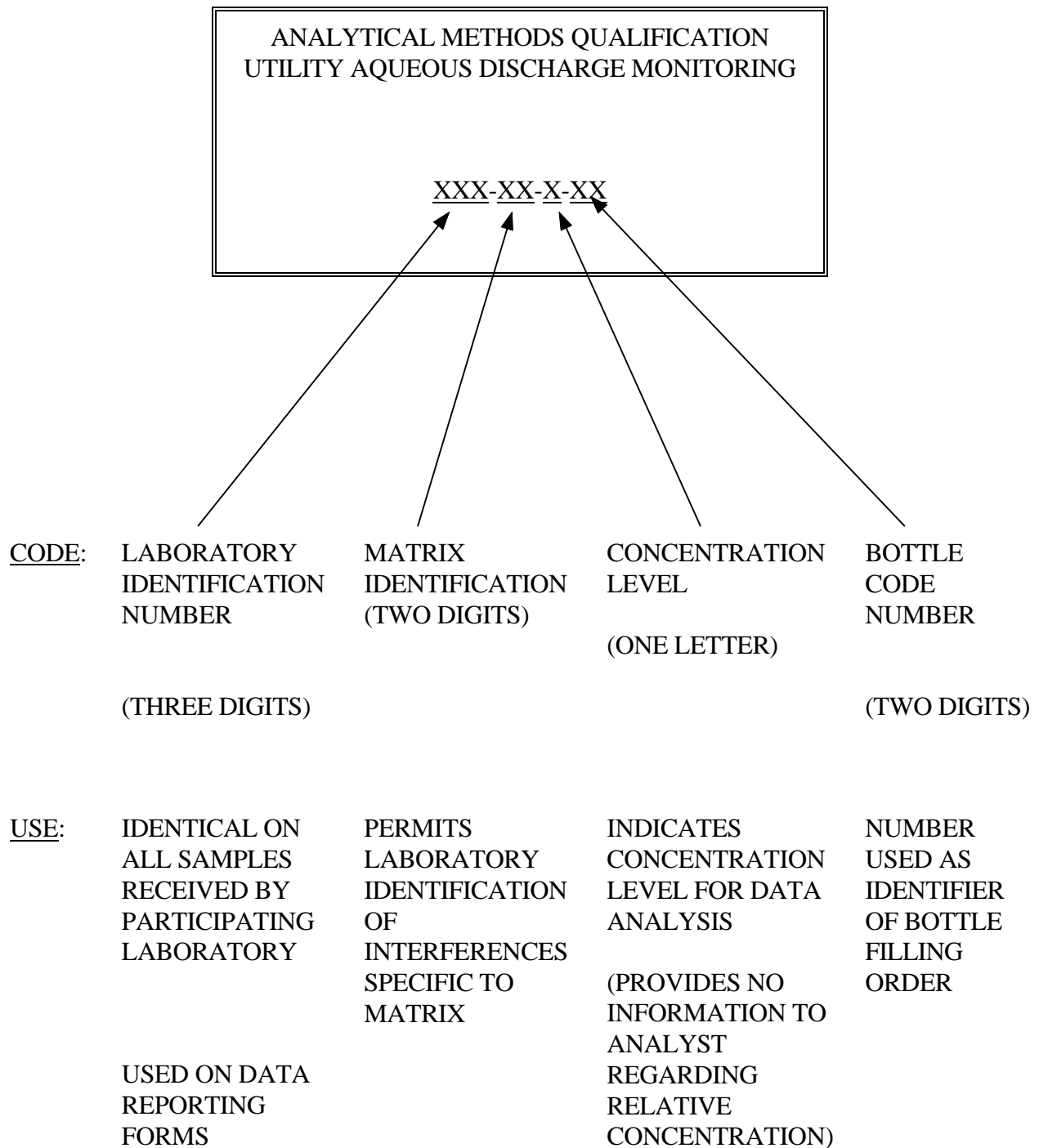


Figure 1. Sample Code System.





# *D*

## **METHOD PARAMETERS REPORTING FORM**

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EPRI AMQ-TC  
METHOD PARAMETERS REPORTING FORM

Laboratory No. \_\_\_\_\_ Laboratory Name \_\_\_\_\_  
Date \_\_\_\_\_ Analyst(s) \_\_\_\_\_

**ARSENIC**

Wavelength \_\_\_\_\_ nm

Calibration Range \_\_\_\_\_ to \_\_\_\_\_ µg/L

Injection Volume \_\_\_\_\_ µL

Purge Gas \_\_\_\_\_

Purge Gas Mode: Constant Flow \_\_\_\_ Stop Flow \_\_\_\_ Pressurized \_\_\_\_

Type of Background Correction: Deuterium Arc \_\_\_\_ Smith-Hieftje \_\_\_\_ Secondary Line \_\_\_\_

Zeeman \_\_\_\_ None \_\_\_\_ Other \_\_\_\_\_

		Furnace Conditions, °C, Sec							
		Drying		Ash		Atomization			
Matrix	Std Addn ?	Temp	Time	Temp	Time	Temp	Time	Pyrolytic or Non-Pyrolytic?	Tube or Platform?
RGW (05)									
FW (08)									
EST (09)									
AMD (10)									

Were other elements determined using this same furnace tube/platform?

Yes \_\_\_\_; List elements: \_\_\_\_\_

No \_\_\_\_

Operator experience analyzing arsenic by GFAAS:

Routine \_\_\_\_ Frequency \_\_\_\_\_ Conc. levels \_\_\_\_\_ Matrices \_\_\_\_\_

Occasional \_\_\_\_ Frequency \_\_\_\_\_ Conc. levels \_\_\_\_\_ Matrices \_\_\_\_\_

None \_\_\_\_

How do you normally analyze arsenic? GFAAS \_\_\_\_ FLAAS \_\_\_\_ ICP-AES \_\_\_\_ Other \_\_\_\_

What is your usual digestion method for arsenic? \_\_\_\_\_

Comments

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EPRI AMQ-TC  
METHOD PARAMETERS REPORTING FORM (Cont'd)

Laboratory No. \_\_\_\_\_ Laboratory Name \_\_\_\_\_  
Date \_\_\_\_\_ Analyst(s) \_\_\_\_\_

**CADMIUM**

Wavelength \_\_\_\_\_ nm

Calibration Range \_\_\_\_\_ to \_\_\_\_\_ µg/L

Injection Volume \_\_\_\_\_ µL

Purge Gas \_\_\_\_\_

Purge Gas Mode: Constant Flow \_\_\_\_ Stop Flow \_\_\_\_ Pressurized \_\_\_\_

Type of Background Correction: Deuterium Arc \_\_\_\_ Smith-Hieftje \_\_\_\_ Secondary Line \_\_\_\_

Zeeman \_\_\_\_ None \_\_\_\_ Other \_\_\_\_\_

		Furnace Conditions, °C, Sec							
		Drying		Ash		Atomization			
Matrix	Std Addn ?	Temp	Time	Temp	Time	Temp	Time	Pyrolytic or Non-Pyrolytic?	Tube or Platform?
RGW (05)									
FW (08)									
EST (09)									
AMD (10)									

Were other elements determined using this same furnace tube/platform?

Yes \_\_\_\_; List elements: \_\_\_\_\_

No \_\_\_\_

Operator experience analyzing cadmium by GFAAS:

Routine \_\_\_\_ Frequency \_\_\_\_\_ Conc. levels \_\_\_\_\_ Matrices \_\_\_\_\_

Occasional \_\_\_\_ Frequency \_\_\_\_\_ Conc. levels \_\_\_\_\_ Matrices \_\_\_\_\_

None \_\_\_\_

How do you normally analyze cadmium? GFAAS \_\_\_\_ FLAAS \_\_\_\_ ICP-AES \_\_\_\_ Other \_\_\_\_

What is your usual digestion method for cadmium? \_\_\_\_\_

Comments

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## METHOD PARAMETERS REPORTING FORM (Cont'd)

Laboratory No. \_\_\_\_\_ Laboratory Name \_\_\_\_\_  
 Date \_\_\_\_\_ Analyst(s) \_\_\_\_\_

**CHROMIUM**

Wavelength \_\_\_\_\_ nm

Calibration Range \_\_\_\_\_ to \_\_\_\_\_ µg/L

Injection Volume \_\_\_\_\_ µL

Purge Gas \_\_\_\_\_

Purge Gas Mode: Constant Flow \_\_\_\_ Stop Flow \_\_\_\_ Pressurized \_\_\_\_

Type of Background Correction: Deuterium Arc \_\_\_\_ Smith-Hieftje \_\_\_\_ Secondary Line \_\_\_\_

Zeeman \_\_\_\_ None \_\_\_\_ Other \_\_\_\_\_

		Furnace Conditions, °C, Sec							
		Drying		Ash		Atomization			
Matrix	Std Addn ?	Temp	Time	Temp	Time	Temp	Time	Pyrolytic or Non-Pyrolytic?	Tube or Platform?
RGW (05)									
FW (08)									
EST (09)									
AMD (10)									

Were other elements determined using this same furnace tube/platform?

Yes \_\_\_\_; List elements: \_\_\_\_\_

No \_\_\_\_

Operator experience analyzing chromium by GFAAS:

Routine \_\_\_\_ Frequency \_\_\_\_\_ Conc. levels \_\_\_\_\_ Matrices \_\_\_\_\_

Occasional \_\_\_\_ Frequency \_\_\_\_\_ Conc. levels \_\_\_\_\_ Matrices \_\_\_\_\_

None \_\_\_\_

How do you normally analyze chromium? GFAAS \_\_\_\_ FLAAS \_\_\_\_ ICP-AES \_\_\_\_ Other \_\_\_\_

What is your usual digestion method for chromium? \_\_\_\_\_

Comments

\_\_\_\_\_  
 \_\_\_\_\_

## METHOD PARAMETERS REPORTING FORM (Cont'd)

Laboratory No. \_\_\_\_\_ Laboratory Name \_\_\_\_\_  
Date \_\_\_\_\_ Analyst(s) \_\_\_\_\_

Miscellaneous Questions

1. Aliquot introduced to furnace by:  
Glass pipet \_\_\_\_  
Plastic micropipet \_\_\_\_  
Autosampler \_\_\_\_  
Micro-boat \_\_\_\_  
Other \_\_\_\_\_
2. If plastic micropipet tips were used for introduction of aliquot, were they acid cleaned prior to use?  
Yes \_\_\_\_ Acid \_\_\_\_\_  
No \_\_\_\_
3. Please identify the color and state manufacturer of the plastic micropipet tips:  
Yellow \_\_\_\_  
Blue \_\_\_\_  
Clear \_\_\_\_  
Manufacturer \_\_\_\_\_

## Comments

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***E***

## **HIGHLIGHTS OF LAB OPERATING DATA SURVEY**

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EPRI AMQ-TC  
LABORATORY EQUIPMENT AND PRACTICES SURVEY

LABORATORY Summary of responses for AMQ-IV Round 2 laboratories

KEY CONTACT/PHONE \_\_\_\_\_

( ) # of laboratories responding. Total of 18 laboratories participated.

MATRICES ANALYZED (Please Circle)

- (05) Reagent Grade Water
- (08) Freshwater
- (09) Estuarine
- (10) Acid Mine Drainage

Apparatus

1. Atomic Absorption Spectrometer (AAS): (22 instruments)

Manufacturer

Model

Instrumentation Laboratory \_\_\_\_\_

Perkin-Elmer 73% 1100(1); 2100(2); 3030(1); 3100(1); 5000(4); 5100(7)

Varian 18% 400Z(2); SpectrAA40(1); SpectrAA600Z(1)

Jarrell-Ash 9% SH-12(1); SH-4000(1)

Other \_\_\_\_\_

2. Graphite Furnace manufactured by: (22 instruments)

Manufacturer

Model

Instrumentation Laboratory \_\_\_\_\_

Perkin-Elmer 73% HGA400(2); HGA500(3); HGA600(2); HGA700(1); 4100(2) 5100(5)

Varian 18% 400Z(2); GTA100(1); SpectrAA40(1)

Jarrell-Ash 9% 188(1); SH-4000(1)

Other \_\_\_\_\_

3. Type of Graphite Furnace (17 - varied by element)

Tube 41%

Platform 82%

Other \_\_\_\_\_

4. Type of AAS: (16)

Single Beam 31%

Double Beam 69%



5. AAS instrument control: (17 - multiple responses)

Manual\_\_\_\_\_

Microprocessor 47%

Outside computer 59%

Other\_\_\_\_\_

6. Was an autosampler used for these analyses?

Yes 89%

No 11%

7. If data reduction is performed by microprocessor or computer, describe program mode:

Comparison to calibration curve? (linear 52% non-linear 24%)

Least squares program 6%

Other Quadratic (12%); Best-fit (6%)

8. Type of spectral emission source: (18 - varied by element)

Hollow cathode 94%

Electrodeless discharge 67%

Hollow cathode w/ changeable cathode\_\_\_\_\_

Other\_\_\_\_\_

9. Date of last major repair:\_\_\_\_\_

10. Date of last vendor calibration:\_\_\_\_\_

#### Laboratory Standards and Sample Handling

1. Type of volumetric laboratory equipment used: (18)  
(check all that apply)

Plastic micropipets, single volume 56%

Plastic micropipets, variable volume 56%

Glass class A pipets 67%

Plastic volumetric flasks 11%

Glass volumetric flasks 100%

Autodilutor 11%

Other; specify\_\_\_\_\_

## Highlights of Lab Operating Data Survey

2. What was the source of standard reference materials used for instrument calibration and/or method of standard addition? (18)

Commercial 100%

Self-prepared 6% (in addition to commercial)

3. In what type of container were standards stored? (18 labs, multiple responses)

Glass 22%

Polypropylene 28%

Polyethylene 61%

Teflon         

Other   

4. What was the date of receipt or preparation of standard solutions?

Element	Date of receipt/prep	Date(s) of use
<u>        </u>	<u>                                </u>	<u>                                </u>
<u>        </u>	<u>                                </u>	<u>                                </u>
<u>        </u>	<u>                                </u>	<u>                                </u>

5. Which of the following were used for precleaning glassware and sample and standards storage bottles? (18 labs - some varied cleaning for glassware, sample or standard storage)

HCl only 11%

HNO<sub>3</sub> only 39%

Detergent only (brand) 11%

Detergent (brand)                         , HCl and HNO<sub>3</sub> 11%

Detergent (brand)                          and HNO<sub>3</sub> 33%

Other sample bottles purchased precleaned - 5%

no cleaning of sample bottles - 5%

Detergents
Alconox 2
Dawn 1
Ivory 1
Liquinox 1
Micro Clean 2
Sparkleen 1
Unspecified

6. How were test samples stored? (18)

Refrigerated 6%

Room temperature 94%





Operator Experience

1. Have operators attended GFAAS training classes for the specific instrument employed? (18)

Yes 61%

No 39%

2. What are the number of years experience with GFAAS for the primary operator(s)?

First Operator (18)

0 to 0.5 6%

0.5 to 1 6%

1 to 5 38%

5 to 10 28%

>10 22%

Second Operator (9)

0 to 0.5         

0.5 to 1 11%

1 to 5 56%

5 to 10 22%

>10 11%

3. What is the degree level and major field of study of the primary operator(s)?

First Operator (18)

Degree

No degree 11%

A.A. 11%

B.A. or B.S. 72%

M.A. or M.S.         

Ph.D. 6%

Major

Chem Eng (1); Chem Tech (1)

Bio (3); Chem (6); Chem/Bio (1) Micro (1)

Bio (1)

Second Operator (9)

Degree

No degree 22%

A.A. 11%

B.A. or B.S. 56%

M.A. or M.S. 11%

Ph.D.         

Major

Unspecified (1)

Bio (1); Chem (1); Geo (1); Enviro (1);

Unspecified (1)

Organic Synth (1)

4. What is the degree level and major field of study of the laboratory supervisor responsible for AAS analysis? (18)

Degree	Major
No degree_____	_____
A.A. _____	_____
B.A. or B.S. <u>89%</u>	<u>Bio (1); Chem (10); Chem/Bio (1)</u>
	<u>Biochem (1); Micro (1); Enviro (1)</u>
	<u>Unspecified (1)</u>
M.A. or M.S. <u>11%</u>	<u>Organic Synth (1); Chem (1)</u>
Ph.D. _____	_____

5. How many years of experience (beyond B.S.) does the above supervisor have?

0-1 6%  
 1-5 11%  
 5-10 6%  
 >10 77%

***F***

## **LABORATORY DATA REPORTING FORM**

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## Laboratory Data Reporting Form

**EPRI AMQ-TC – Round 1****AMQTC****Round 1****Sample ID:** \_\_\_\_\_ - \_\_\_\_\_ - \_\_\_\_\_ - \_\_\_\_\_**Matrix Type:** Reagent Grade Water (05)  
Freshwater (08)  
Estuarine (09)  
Acid Mine Drainage (10)**IMPORTANT NOTICE**

Report the actual value calculated for the sample concentration, even if it is below your detection limit. Indicate your detection limit in the space provided.

**PLEASE REPORT ALL RESULTS TO 0.1 ug/L.**

ELEMENT	MEASURED ALIQUOT CONC (ug/L)	DILUTION FACTOR	CALCULATED CONCENTRATION OF ORIGINAL SAMPLE (ug/L)	DETECTION LIMIT * (ug/L)	ANALYST *	TESTING DATES *	
						STARTED	COMPLETED
As	_____	_____	_____	_____	_____	_____	_____
Cd	_____	_____	_____	_____	_____	_____	_____
Cr	_____	_____	_____	_____	_____	_____	_____

Sample condition on Arrival: \_\_\_\_\_

Comments / Problems: \_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\* If same for all samples in a matrix set, it is necessary to fill in only on first page of matrix set.

**Please retain all data and lab records in order to answer any questions that may arise.****Make a copy of this completed form to keep with your records.**



G

## RAW DATA

Table G-1  
Arsenic Raw Data

Lab	Matrix	As Bkg1	As Bkg2	As-1	As-2	As-3	As-4	As-5	As-6	As-7	As-8
1	5	-0.3400	0.2200	4.9400	6.8400	22.6000	31.4000	53.8000	57.2000	83.0000	84.5000
1	8	0.9700	0.9800	5.4200	8.9000	17.3000	23.0000	39.8000	49.8000	81.0000	83.0000
1	10	3.9000	5.7000	65.7000	98.2000	316.0000	387.0000	660.0000	684.0000	510.0000	670.0000
2	5	-1.5000	-2.3000	4.1000	5.4000	22.4000	28.9000	58.6000	65.4000	106.3000	124.5000
2	8	-1.2000	-0.6000	3.3000	6.2000	14.7000	18.9000	34.5000	42.2000	96.8000	109.9000
2	10	-0.5000	-1.1000	58.0000	66.0000	300.0000	37.7000	712.0000	816.0000	993.0000	1089.0000
5	5	-0.1000	-0.7000	4.3000	6.5000	20.1000	26.9000	49.3000	55.6000	89.6000	107.4000
5	8	1.0000	1.1000	5.3000	9.3000	18.9000	24.2000	41.7000	51.0000	90.9000	98.7000
5	9	14.0000	13.0000	58.0000	70.0000	254.0000	313.0000	614.0000	677.0000	907.0000	974.0000
5	10	12.0000	19.0000	82.0000	108.0000	341.0000	424.0000	731.0000	802.0000	917.0000	984.0000
6	5	-0.3000	-0.5000	3.8000	5.4000	20.6000	28.3000	56.7000	55.5000	86.4000	96.8000
6	8	-0.6000	0.2000	4.3000	9.1000	18.0000	23.5000	40.5000	49.7000	91.8000	98.2000
6	9	-4.0000	-3.0000	48.0000	48.0000	219.0000	255.0000	561.0000	611.0000	799.0000	929.0000
6	10	5.0000	5.0000	81.0000	119.0000	367.0000	481.0000	811.0000	879.0000	965.0000	1026.0000
7	5	-2.4200	-1.7200	3.1800	4.7200	23.1000	30.9000	53.8000	63.1000	90.6000	96.6000
7	8	-5.4900	-4.9500	-2.5500	3.3200	10.6000	17.8000	31.7000	39.2000	69.4000	79.0000
7	9	-2.1500	2.2600	22.2000	23.3000	163.0000	172.0000	437.0000	470.0000	641.0000	618.0000

## Raw Data

Table G-1  
Arsenic Raw Data

Lab	Matrix	As Bkg1	As Bkg2	As-1	As-2	As-3	As-4	As-5	As-6	As-7	As-8
7	10	-4.4200	5.4800	57.0000	83.0000	321.0000	403.0000	697.0000	772.0000	841.0000	938.0000
8	5	1.2000	0.6000	4.2000	6.7000	17.8000	25.8000	10.8000	47.8000	89.4000	89.4000
8	8	2.4000	0.0000	5.2000	9.2000	15.9000	21.7000	33.7000	38.5000	75.3000	67.5000
8	9	3.0000	0.2000	48.4000	65.7000	238.0000	318.0000	422.0000	384.0000	864.0000	760.0000
8	10	0.0000	0.0000	18.3000	20.7000	45.4000	40.8000	836.0000	944.0000	928.0000	992.0000
10	5	-0.8000	1.3000	1.8000	7.3000	22.5000	29.4000	57.5000	66.0000	93.8000	89.9000
10	8	-1.7000	-2.3000	-1.3000	-1.4000	25.5000	26.2000	51.3000	58.1000	68.9000	90.2000
10	9	5.7000	19.5000	36.0000	1.0000	228.0000	213.0000	487.0000	727.0000	727.0000	1040.0000
10	10	36.0000	6.0000	45.0000	58.0000	217.0000	474.0000	739.0000	668.0000	790.0000	917.0000
11	5	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
11	8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
11	10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
15	5	1.1000	0.4000	5.4000	7.0000	19.0000	25.6000	46.0000	53.1000	93.6000	99.3000
15	8	0.0000	0.6000	4.6000	8.5000	16.7000	22.1000	41.1000	51.5000	92.6000	7.9000
15	9	4.2000	2.7000	32.0000	42.0000	185.0000	242.0000	494.0000	568.0000	749.0000	820.0000
15	10	4.7000	3.0000	62.0000	81.0000	288.0000	348.0000	736.0000	595.0000	775.0000	931.0000
16	5	9.4000	5.5000	8.3000	10.0000	31.1000	36.1000	62.2000	73.3000	90.0000	107.0000
16	8	12.2000	7.2000	13.3000	18.3000	28.9000	42.8000	59.4000	64.4000	95.6000	101.0000
16	9	60.0000	60.0000	167.0000	66.0000	367.0000	254.0000	722.0000	833.0000	723.0000	888.0000
16	10	52.2000	9.0000	175.0000	122.0000	422.0000	589.0000	800.0000	770.0000	988.0000	112.0000
17	5	0.0000	0.0000	6.0000	8.0000	24.0000	32.0000	62.0000	68.0000	127.2000	129.0000
17	8	1.0000	2.0000	6.0000	10.0000	27.0000	27.0000	48.0000	56.0000	116.0000	120.0000

Table G-1  
Arsenic Raw Data

Lab	Matrix	As Bkg1	As Bkg2	As-1	As-2	As-3	As-4	As-5	As-6	As-7	As-8
17	9	3.0000	3.0000	48.0000	58.0000	261.0000	280.0000	560.0000	620.0000	840.0000	880.0000
17	10	6.0000	57.0000	100.0000	140.0000	400.0000	490.0000	220.0000	930.0000	1080.0000	770.0000
20	5	0.5000	2.4000	6.1000	7.5000	24.2000	29.8000	52.9000	58.4000	87.5000	103.1000
20	8	0.6000	1.5000	5.7000	11.0000	21.0000	26.3000	44.1000	95.5000	94.0000	101.5000
20	9	26.0000	20.0000	67.0000	67.0000	275.0000	320.0000	664.0000	657.0000	896.0000	969.0000
20	10	13.0000	18.0000	94.0000	118.0000	364.0000	448.0000	779.0000	855.0000	952.0000	1062.0000
21	5	-1.0000	-1.0000	4.4000	6.4000	22.2000	28.3000	50.0000	57.0000	87.4000	99.6000
21	8	0.8000	0.6000	5.0000	8.4000	17.3000	22.5000	37.8000	44.5000	79.3000	79.6000
21	9	3.0000	2.7000	44.5000	55.0000	220.0000	269.0000	532.0000	578.0000	791.0000	835.0000
21	10	37.0000	37.9000	59.0000	87.0000	310.0000	389.0000	633.0000	675.0000	765.0000	819.0000
22	5	11.0000	10.5600	11.3000	11.6000	27.1000	34.1000	55.5000	64.6000	96.2000	120.8000
22	8	12.7000	12.7000	13.0000	14.4000	20.1000	24.6000	35.9000	42.2000	66.7000	71.6000
22	9	14.0000	16.5000	51.9000	66.2000	269.0000	311.0000	491.0000	562.0000	848.0000	793.0000
24	5	0.0000	1.0800	3.8100	7.4200	22.0000	29.4000	56.2000	67.9000	87.0000	126.0000
24	8	1.4900	0.0000	7.2200	8.3200	18.6000	18.5000	42.0000	40.1000	90.5000	96.9000
24	9	6.0000	6.2000	47.1000	55.0000	152.0000	168.0000	318.0000	718.0000	919.0000	1167.0000
24	10	21.4000	21.5000	96.6000	158.0000	375.0000	680.0000	779.0000	950.0000	1090.0000	1156.0000
25	5	0.0000	0.0000	5.7000	6.9000	22.6000	27.6000	43.2000	58.4000	89.2000	107.0000
25	8	0.0000	0.0000	6.2000	9.3000	13.7000	22.6000	45.1000	44.8000	80.0000	85.6000
25	9	3.2000	3.2000	42.9000	56.1000	240.0000	267.0000	594.0000	535.0000	861.0000	939.0000
25	10	0.0000	0.0000	52.8000	294.0000	380.0000	384.0000	648.0000	713.0000	818.0000	889.0000
26	5	-0.5000	-0.8000	5.2000	6.7000	22.0000	28.5000	50.8000	59.3000	88.7000	99.5000

*Raw Data*Table G-1  
Arsenic Raw Data

Lab	Matrix	As Bkg1	As Bkg2	As-1	As-2	As-3	As-4	As-5	As-6	As-7	As-8
26	8	0.2000	0.3000	4.5000	10.0000	19.2000	24.6000	40.6000	51.7000	90.3000	94.9000
26	9	-6.0000	10.0000	54.0000	55.0000	251.0000	313.0000	603.0000	677.0000	831.0000	924.0000
26	10	-1.0000	0.0000	64.0000	84.0000	323.0000	394.0000	725.0000	737.0000	904.0000	973.0000
27	5	-1.0000	0.0000	4.0000	7.0000	19.0000	25.0000	47.0000	54.0000	88.0000	88.0000
27	8	-2.0000	-2.0000	2.0000	6.0000	14.0000	20.0000	36.0000	45.0000	81.0000	97.0000
27	9	-20.0000	-30.0000	20.0000	30.0000	190.0000	240.0000	530.0000	530.0000	770.0000	770.0000
27	10	-20.0000	-10.0000	60.0000	90.0000	350.0000	430.0000	670.0000	810.0000	840.0000	960.0000

Table G-2  
Cadmium Raw Data

Lab	Matrix	Cd Bkg1	Cd Bkg2	Cd-1	Cd-2	Cd-3	Cd-4	Cd-5	Cd-6	Cd-7	Cd-8
1	5	0.0000	-0.0200	6.1100	8.5100	15.3000	21.1000	49.9000	56.9000	84.8000	101.8000
1	8	0.0900	0.1300	8.4800	6.0500	14.8000	21.6000	42.5000	45.9000	83.5000	92.2000
1	10	12.4000	11.4000	40.5000	58.1000	165.1000	214.7000	399.0000	440.0000	1123.0000	1022.0000
2	5	-0.2000	-0.3000	5.1000	8.4000	15.4000	21.3000	38.3000	42.4000	65.6000	80.6000
2	8	-0.1000	-0.5000	4.4000	7.5000	17.6000	21.5000	45.1000	48.0000	97.0000	106.0000
2	10	2.0000	3.0000	47.0000	66.0000	210.0000	279.0000	430.0000	410.0000	744.0000	732.0000
5	5	0.5000	0.2000	5.3000	8.7000	15.2000	21.5000	47.1000	55.2000	85.3000	101.3000
5	8	0.6000	0.5000	4.7000	7.4000	19.5000	22.7000	50.3000	58.9000	80.9000	93.3000
5	9	2.0000	0.0000	55.0000	74.0000	283.0000	372.0000	618.0000	697.0000	820.0000	932.0000
5	10	3.0000	3.0000	41.0000	59.0000	180.0000	247.0000	378.0000	436.0000	752.0000	817.0000
6	5	-0.7000	-0.9000	4.3000	7.6000	15.4000	22.0000	49.2000	55.0000	85.9000	96.3000
6	8	-0.1000	1.6000	3.3000	6.4000	15.4000	19.1000	44.3000	49.6000	75.9000	90.7000
6	9	-7.0000	-10.0000	48.0000	70.0000	282.0000	337.0000	648.0000	732.0000	816.0000	944.0000
6	10	0.0000	-7.0000	39.0000	54.0000	206.0000	290.0000	446.0000	505.0000	863.0000	951.0000
7	5	-0.4930	-0.6500	6.0800	8.1400	16.1000	23.2000	49.8000	56.1000	81.9000	92.6000
7	8	0.1410	-0.4470	4.4700	8.7400	20.4000	26.8000	55.4000	64.8000	86.2000	110.0000
7	9	1.5500	1.7300	45.5000	60.0000	323.0000	407.0000	645.0000	720.0000	797.0000	895.0000
7	10	5.1200	4.8200	43.4000	62.0000	206.0000	275.0000	418.0000	468.0000	796.0000	822.0000
8	5	2.5000	-1.2000	5.0000	10.1000	13.3000	22.0000	50.2000	46.1000	84.1000	89.9000
8	8	0.0000	1.4000	5.4000	9.4000	23.4000	23.1000	57.6000	56.9000	103.0000	109.0000
8	9	2.8000	0.9000	55.3000	75.5000	269.0000	286.0000	534.0000	601.0000	726.0000	818.0000

## Raw Data

Table G-2  
Cadmium Raw Data

Lab	Matrix	Cd Bkg1	Cd Bkg2	Cd-1	Cd-2	Cd-3	Cd-4	Cd-5	Cd-6	Cd-7	Cd-8
8	10	0.9000	0.4000	30.3000	52.2000	172.0000	257.0000	394.0000	479.0000	794.0000	930.0000
10	5	0.7000	0.8000	6.1000	7.5000	15.7000	22.3000	45.1000	57.1000	82.7000	87.0000
10	8	0.8000	1.0000	3.9000	6.1000	15.9000	21.3000	53.1000	59.1000	78.5000	84.9000
10	9	29.5000	4.0000	58.5000	90.5000	372.5000	430.5000	729.5000	764.5000	980.0000	1050.0000
10	10	42.5000	100.0000	100.5000	73.5000	308.0000	343.0000	463.0000	466.0000	971.0000	1072.5000
11	5	-0.1000	-0.1000	5.6000	8.1000	15.8000	21.9000	47.2000	53.7000	84.7000	88.2000
11	8	0.2000	-0.1000	4.9000	8.3000	20.0000	25.1000	54.7000	64.3000	86.1000	104.0000
11	10	7.1000	8.2000	51.7000	69.8000	215.0000	276.0000	451.0000	505.0000	902.0000	990.0000
15	5	0.6000	1.1000	5.9000	8.5000	16.2000	22.0000	49.9000	51.6000	82.7000	80.6000
15	8	1.1000	0.9000	4.4000	7.5000	18.1000	23.3000	48.2000	54.1000	92.3000	98.9000
15	9	1.1000	1.0000	47.0000	67.0000	261.0000	333.0000	532.0000	642.0000	728.0000	878.0000
15	10	3.9000	4.1000	40.0000	59.0000	192.0000	247.0000	396.0000	413.0000	718.0000	855.0000
16	5	2.2000	7.8000	10.6000	11.1000	22.8000	28.3000	36.7000	67.8000	67.8000	88.3000
16	8	7.2000	6.1000	11.1000	16.7000	32.8000	38.9000	75.6000	90.0000	125.6000	143.9000
16	9	8.0000	84.0000	60.0000	100.0000	378.0000	269.0000	471.0000	582.0000	644.0000	700.0000
16	10	22.2000	8.9000	54.4000	111.0000	233.0000	322.0000	478.0000	460.0000	830.0000	910.0000
17	5	1.0000	0.0000	6.0000	9.0000	16.0000	23.0000	52.0000	59.0000	89.0000	119.7000
17	8	6.0000	5.0000	5.0000	9.0000	28.0000	28.0000	75.0000	70.0000	100.0000	30.0000
17	9	6.0000	3.0000	66.0000	94.0000	376.0000	420.0000	690.0000	780.0000	910.0000	1249.0000
17	10	6.0000	4.0000	53.0000	69.0000	223.0000	303.0000	512.0000	580.0000	1020.0000	1211.0000
20	5	1.5000	0.7000	5.1000	7.2000	16.8000	22.7000	45.0000	52.6000	81.2000	90.4000
20	8	1.0000	0.6000	266.0000	10.1000	20.5000	25.7000	54.1000	67.6000	90.7000	96.4000

Table G-2  
Cadmium Raw Data

Lab	Matrix	Cd Bkg1	Cd Bkg2	Cd-1	Cd-2	Cd-3	Cd-4	Cd-5	Cd-6	Cd-7	Cd-8
20	9	27.0000	23.0000	80.0000	90.0000	329.0000	390.0000	682.0000	735.0000	873.0000	972.0000
20	10	24.0000	18.0000	87.0000	96.0000	266.0000	343.0000	507.0000	563.0000	937.0000	1052.0000
21	5	4.8000	0.1000	6.8000	10.0000	17.4000	22.9000	48.7000	54.1000	80.0000	95.7000
21	8	4.1000	2.1000	7.1000	8.6000	18.7000	25.6000	50.6000	59.7000	82.2000	97.4000
21	9	1.0000	0.5000	61.0000	76.0000	293.0000	378.0000	596.0000	698.0000	823.0000	905.0000
21	10	2.9000	2.0000	36.0000	53.0000	171.0000	244.0000	376.0000	439.0000	765.0000	869.0000
22	5	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
22	8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
22	9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
24	5	0.0000	0.9800	5.5000	11.1000	19.8000	29.2000	70.5000	66.3000	62.8000	97.6000
24	8	0.2700	0.0000	4.0100	11.7000	29.1000	31.3000	54.5000	83.8000	87.2000	87.6000
24	9	7.0000	0.0000	74.2000	67.1000	397.0000	487.0000	717.0000	548.0000	734.0000	801.0000
24	10	5.2000	0.0000	32.9000	73.4000	230.0000	258.0000	487.0000	496.0000	450.0000	106.0000
25	5	0.3000	0.0000	7.1000	8.4000	18.6000	18.4000	41.6000	57.6000	88.0000	92.4000
25	8	0.4000	0.0000	5.0000	8.9000	21.8000	16.8000	49.6000	51.7000	77.7000	101.2000
25	9	2.4000	0.0000	62.7000	81.4000	321.0000	409.0000	667.0000	768.0000	848.0000	949.0000
25	10	0.0000	2.4000	58.3000	81.4000	269.0000	295.0000	459.0000	529.0000	1020.0000	949.0000
26	5	0.2000	0.2000	5.8000	8.1000	15.8000	21.8000	49.2000	56.0000	86.0000	99.0000
26	8	0.0000	-0.1000	5.0000	7.7000	19.3000	23.8000	53.0000	73.5000	92.0000	103.0000
26	9	3.0000	0.0000	60.0000	73.0000	284.0000	335.0000	625.0000	670.0000	800.0000	950.0000
26	10	4.0000	4.0000	53.0000	81.0000	206.0000	268.0000	460.0000	490.0000	890.0000	950.0000
27	5	0.0000	1.0000	6.0000	10.0000	15.0000	16.0000	43.0000	45.0000	88.0000	78.0000

*Raw Data*Table G-2  
Cadmium Raw Data

Lab	Matrix	Cd Bkg1	Cd Bkg2	Cd-1	Cd-2	Cd-3	Cd-4	Cd-5	Cd-6	Cd-7	Cd-8
27	8	-1.0000	0.0000	6.0000	9.0000	20.0000	24.0000	48.0000	64.0000	86.0000	99.0000
27	9	10.0000	10.0000	70.0000	80.0000	280.0000	390.0000	550.0000	600.0000	790.0000	810.0000
27	10	10.0000	20.0000	40.0000	80.0000	170.0000	220.0000	300.0000	460.0000	780.0000	870.0000



Table G-3  
Chromium Raw Data

Lab	Matrix	Cr Bkg1	Cr Bkg2	Cr-1	Cr-2	Cr-3	Cr-4	Cr-5	Cr-6	Cr-7	Cr-8
1	5	0.0000	-0.0200	6.1100	8.5100	15.3000	21.1000	49.9000	56.9000	84.8000	101.8000
1	8	0.0900	0.1300	8.4800	6.0500	14.8000	21.6000	42.5000	45.9000	83.5000	92.2000
1	10	12.4000	11.4000	40.5000	58.1000	165.1000	214.7000	399.0000	440.0000	1123.0000	1022.0000
2	5	-0.2000	-0.3000	5.1000	8.4000	15.4000	21.3000	38.3000	42.4000	65.6000	80.6000
2	8	-0.1000	-0.5000	4.4000	7.5000	17.6000	21.5000	45.1000	48.0000	97.0000	106.0000
2	10	2.0000	3.0000	47.0000	66.0000	210.0000	279.0000	430.0000	410.0000	744.0000	732.0000
5	5	0.5000	0.2000	5.3000	8.7000	15.2000	21.5000	47.1000	55.2000	85.3000	101.3000
5	8	0.6000	0.5000	4.7000	7.4000	19.5000	22.7000	50.3000	58.9000	80.9000	93.3000
5	9	2.0000	0.0000	55.0000	74.0000	283.0000	372.0000	618.0000	697.0000	820.0000	932.0000
5	10	3.0000	3.0000	41.0000	59.0000	180.0000	247.0000	378.0000	436.0000	752.0000	817.0000
6	5	-0.7000	-0.9000	4.3000	7.6000	15.4000	22.0000	49.2000	55.0000	85.9000	96.3000
6	8	-0.1000	1.6000	3.3000	6.4000	15.4000	19.1000	44.3000	49.6000	75.9000	90.7000
6	9	-7.0000	-10.0000	48.0000	70.0000	282.0000	337.0000	648.0000	732.0000	816.0000	944.0000
6	10	0.0000	-7.0000	39.0000	54.0000	206.0000	290.0000	446.0000	505.0000	863.0000	951.0000
7	5	-0.4930	-0.6500	6.0800	8.1400	16.1000	23.2000	49.8000	56.1000	81.9000	92.6000
7	8	0.1410	-0.4470	4.4700	8.7400	20.4000	26.8000	55.4000	64.8000	86.2000	110.0000
7	9	1.5500	1.7300	45.5000	60.0000	323.0000	407.0000	645.0000	720.0000	797.0000	895.0000
7	10	5.1200	4.8200	43.4000	62.0000	206.0000	275.0000	418.0000	468.0000	796.0000	822.0000
8	5	2.5000	-1.2000	5.0000	10.1000	13.3000	22.0000	50.2000	46.1000	84.1000	89.9000
8	8	0.0000	1.4000	5.4000	9.4000	23.4000	23.1000	57.6000	56.9000	103.0000	109.0000
8	9	2.8000	0.9000	55.3000	75.5000	269.0000	286.0000	534.0000	601.0000	726.0000	818.0000

Raw Data

Table G-3  
Chromium Raw Data

Lab	Matrix	Cr Bkg1	Cr Bkg2	Cr-1	Cr-2	Cr-3	Cr-4	Cr-5	Cr-6	Cr-7	Cr-8
8	10	0.9000	0.4000	30.3000	52.2000	172.0000	257.0000	394.0000	479.0000	794.0000	930.0000
10	5	0.7000	0.8000	6.1000	7.5000	15.7000	22.3000	45.1000	57.1000	82.7000	87.0000
10	8	0.8000	1.0000	3.9000	6.1000	15.9000	21.3000	53.1000	59.1000	78.5000	84.9000
10	9	29.5000	4.0000	58.5000	90.5000	372.5000	430.5000	729.5000	764.5000	980.0000	1050.0000
10	10	42.5000	100.0000	100.5000	73.5000	308.0000	343.0000	463.0000	466.0000	971.0000	1072.5000
11	5	-0.1000	-0.1000	5.6000	8.1000	15.8000	21.9000	47.2000	53.7000	84.7000	88.2000
11	8	0.2000	-0.1000	4.9000	8.3000	20.0000	25.1000	54.7000	64.3000	86.1000	104.0000
11	10	7.1000	8.2000	51.7000	69.8000	215.0000	276.0000	451.0000	505.0000	902.0000	990.0000
15	5	0.6000	1.1000	5.9000	8.5000	16.2000	22.0000	49.9000	51.6000	82.7000	80.6000
15	8	1.1000	0.9000	4.4000	7.5000	18.1000	23.3000	48.2000	54.1000	92.3000	98.9000
15	9	1.1000	1.0000	47.0000	67.0000	261.0000	333.0000	532.0000	642.0000	728.0000	878.0000
15	10	3.9000	4.1000	40.0000	59.0000	192.0000	247.0000	396.0000	413.0000	718.0000	855.0000
16	5	2.2000	7.8000	10.6000	11.1000	22.8000	28.3000	36.7000	67.8000	67.8000	88.3000
16	8	7.2000	6.1000	11.1000	16.7000	32.8000	38.9000	75.6000	90.0000	125.6000	143.9000
16	9	8.0000	84.0000	60.0000	100.0000	378.0000	269.0000	471.0000	582.0000	644.0000	700.0000
16	10	22.2000	8.9000	54.4000	111.0000	233.0000	322.0000	478.0000	460.0000	830.0000	910.0000
17	5	1.0000	0.0000	6.0000	9.0000	16.0000	23.0000	52.0000	59.0000	89.0000	119.7000
17	8	6.0000	5.0000	5.0000	9.0000	28.0000	28.0000	75.0000	70.0000	100.0000	30.0000
17	9	6.0000	3.0000	66.0000	94.0000	376.0000	420.0000	690.0000	780.0000	910.0000	1249.0000
17	10	6.0000	4.0000	53.0000	69.0000	223.0000	303.0000	512.0000	580.0000	1020.0000	1211.0000
20	5	1.5000	0.7000	5.1000	7.2000	16.8000	22.7000	45.0000	52.6000	81.2000	90.4000
20	8	1.0000	0.6000	266.0000	10.1000	20.5000	25.7000	54.1000	67.6000	90.7000	96.4000

Table G-3  
Chromium Raw Data

Lab	Matrix	Cr Bkg1	Cr Bkg2	Cr-1	Cr-2	Cr-3	Cr-4	Cr-5	Cr-6	Cr-7	Cr-8
20	9	27.0000	23.0000	80.0000	90.0000	329.0000	390.0000	682.0000	735.0000	873.0000	972.0000
20	10	24.0000	18.0000	87.0000	96.0000	266.0000	343.0000	507.0000	563.0000	937.0000	1052.0000
21	5	4.8000	0.1000	6.8000	10.0000	17.4000	22.9000	48.7000	54.1000	80.0000	95.7000
21	8	4.1000	2.1000	7.1000	8.6000	18.7000	25.6000	50.6000	59.7000	82.2000	97.4000
21	9	1.0000	0.5000	61.0000	76.0000	293.0000	378.0000	596.0000	698.0000	823.0000	905.0000
21	10	2.9000	2.0000	36.0000	53.0000	171.0000	244.0000	376.0000	439.0000	765.0000	869.0000
22	5	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
22	8	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
22	9	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
24	5	0.0000	0.9800	5.5000	11.1000	19.8000	29.2000	70.5000	66.3000	62.8000	97.6000
24	8	0.2700	0.0000	4.0100	11.7000	29.1000	31.3000	54.5000	83.8000	87.2000	87.6000
24	9	7.0000	0.0000	74.2000	67.1000	397.0000	487.0000	717.0000	548.0000	734.0000	801.0000
24	10	5.2000	0.0000	32.9000	73.4000	230.0000	258.0000	487.0000	496.0000	450.0000	106.0000
25	5	0.3000	0.0000	7.1000	8.4000	18.6000	18.4000	41.6000	57.6000	88.0000	92.4000
25	8	0.4000	0.0000	5.0000	8.9000	21.8000	16.8000	49.6000	51.7000	77.7000	101.2000
25	9	2.4000	0.0000	62.7000	81.4000	321.0000	409.0000	667.0000	768.0000	848.0000	949.0000
25	10	0.0000	2.4000	58.3000	81.4000	269.0000	295.0000	459.0000	529.0000	1020.0000	949.0000
26	5	0.2000	0.2000	5.8000	8.1000	15.8000	21.8000	49.2000	56.0000	86.0000	99.0000
26	8	0.0000	-0.1000	5.0000	7.7000	19.3000	23.8000	53.0000	73.5000	92.0000	103.0000
26	9	3.0000	0.0000	60.0000	73.0000	284.0000	335.0000	625.0000	670.0000	800.0000	950.0000
26	10	4.0000	4.0000	53.0000	81.0000	206.0000	268.0000	460.0000	490.0000	890.0000	950.0000
27	5	0.0000	1.0000	6.0000	10.0000	15.0000	16.0000	43.0000	45.0000	88.0000	78.0000

*Raw Data*

Table G-3  
Chromium Raw Data

Lab	Matrix	Cr Bkg1	Cr Bkg2	Cr-1	Cr-2	Cr-3	Cr-4	Cr-5	Cr-6	Cr-7	Cr-8
27	8	-1.0000	0.0000	6.0000	9.0000	20.0000	24.0000	48.0000	64.0000	86.0000	99.0000
27	9	10.0000	10.0000	70.0000	80.0000	280.0000	390.0000	550.0000	600.0000	790.0000	810.0000
27	10	10.0000	20.0000	40.0000	80.0000	170.0000	220.0000	300.0000	460.0000	780.0000	870.0000

# H

## STATCALC INPUT/OUTPUT

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For each element, sorted by matrix, the following tables are presented:

- Data File (.DAT) - Displays original raw data submitted by each laboratory.
- Data Validation File (.DA~) - Audit record documenting the fate of each original data point. Includes information on values removed by lab ranking and outlier testing.
- Final Data File (.DAF) - Final data set submitted for statistical processing after removal of outliers.
- Data Preparation File (.PRP) - Displays the results of the factor of 5 screening, laboratory ranking, individual outlier removal, and normality testing.
- Summary Statistics (.STT) - Contains recovery, single operator standard deviation, and overall standard deviation results at each concentration; results of bias testing; linear and curvilinear equations for single operator and overall standard deviation; linear regression equations for recovery; and linear regression equations for both single operator and overall standard deviation versus recovery (obtained by substitution).

The Data Validation and Final Data files have a flag field to the left of each value which is used to provide information about the value. The following table lists the flags and their meanings.

Flag	Description	File
r	Value removed by lab ranking test	.DA~, .DAF
o	Value removed by individual outlier removal test	.DA~, .DAF
!	Value flagged for removal by lab ranking test but retained. Removal would have exceeded 20% cap on data removal by lab ranking.	.DA~
?	Value flagged for removal by individual outlier test but retained. Removal would have exceeded 10% cap on data removed by outlier testing.	.DA~
e	Temporary fill value for missing value. Calculated by linear regression through remaining data submitted by laboratory. Used for lab ranking test and then deleted.	.DA~
*	No value submitted	.DAF

as-5.dat

As	5	1	4.9400	6.8400	22.6000	31.4000	53.8000	57.2000	83.0000	84.5000
As	5	2	4.1000	5.4000	22.4000	28.9000	58.6000	65.4000	106.3000	124.5000
As	5	5	4.3000	6.5000	20.1000	26.9000	49.3000	55.6000	89.6000	107.4000
As	5	6	3.8000	5.4000	20.6000	28.3000	56.7000	55.5000	86.4000	96.8000
As	5	7	3.1800	4.7200	23.1000	30.9000	53.8000	63.1000	90.6000	96.6000
As	5	8	4.2000	6.7000	17.8000	25.8000	10.8000	47.8000	89.4000	89.4000
As	5	10	1.8000	7.3000	22.5000	29.4000	57.5000	66.0000	93.8000	89.9000
As	5	15	5.4000	7.0000	19.0000	25.6000	46.0000	53.1000	93.6000	99.3000
As	5	16	8.3000	10.0000	31.1000	36.1000	62.2000	73.3000	90.0000	107.0000
As	5	17	6.0000	8.0000	24.0000	32.0000	62.0000	68.0000	127.2000	129.0000
As	5	20	6.1000	7.5000	24.2000	29.8000	52.9000	58.4000	87.5000	103.1000
As	5	21	4.4000	6.4000	22.2000	28.3000	50.0000	57.0000	87.4000	99.6000
As	5	22	11.3000	11.6000	27.1000	34.1000	55.5000	64.6000	96.2000	120.8000
As	5	24	3.8100	7.4200	22.0000	29.4000	56.2000	67.9000	87.0000	126.0000
As	5	25	5.7000	6.9000	22.6000	27.6000	43.2000	58.4000	89.2000	107.0000
As	5	26	5.2000	6.7000	22.0000	28.5000	50.8000	59.3000	88.7000	99.5000
As	5	27	4.0000	7.0000	19.0000	25.0000	47.0000	54.0000	88.0000	88.0000

File Name: as-5  
Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte:  As      Matrix:  Reagent Grade Water
Project:  AMQ-TC   Matrix ID: 5
Date:    12/13/1995 Method:  GFAAS
Pairs:   4
Units:  ug/L
    
```

Level	1	2	3	4	5	6	7	8
Spike	4.3521	2.0000	14.8000	6.4000	21.7000	8.1000	30.0000	11.3000
Spike Increment	.0000	2.0000	16.8000	23.2000	44.9000	53.0000	83.0000	94.3000

Final Concentration		1	2	3	4	5	6	7	8
Lab ID		4.3521	6.3521	21.1521	27.5521	49.2521	57.3521	87.3521	98.6521
1		4.9400	6.8400	22.6000	31.4000	53.8000	57.2000	83.0000	84.5000
2		4.1000	5.4000	22.4000	28.9000	58.6000	65.4000	106.3000	124.5000
5		4.3000	6.5000	20.1000	26.9000	49.3000	55.6000	89.6000	107.4000
6		3.8000	5.4000	20.6000	28.3000	56.7000	55.5000	86.4000	96.8000
7		3.1800	4.7200	23.1000	30.9000	53.8000	63.1000	90.6000	96.6000
8	!	4.2000!	6.7000 !	17.8000!	25.8000 o	10.8000!	47.8000 !	89.4000!	89.4000
10		1.8000	7.3000	22.5000	29.4000	57.5000	66.0000	93.8000	89.9000
15		5.4000	7.0000	19.0000	25.6000	46.0000	53.1000	93.6000	99.3000
16	r	8.3000r	10.0000 r	31.1000r	36.1000 r	62.2000r	73.3000 r	90.0000r	107.0000
17	r	6.0000r	8.0000 r	24.0000r	32.0000 r	62.0000r	68.0000 r	127.2000r	129.0000
20		6.1000	7.5000	24.2000	29.8000	52.9000	58.4000	87.5000	103.1000
21		4.4000	6.4000	22.2000	28.3000	50.0000	57.0000	87.4000	99.6000
22	r	11.3000r	11.6000 r	27.1000r	34.1000 r	55.5000r	64.6000 r	96.2000r	120.8000
24		3.8100	7.4200	22.0000	29.4000	56.2000	67.9000	87.0000	126.0000
25		5.7000	6.9000	22.6000	27.6000	43.2000	58.4000	89.2000	107.0000
26		5.2000	6.7000	22.0000	28.5000	50.8000	59.3000	88.7000	99.5000
27		4.0000	7.0000	19.0000	25.0000	47.0000	54.0000	88.0000	88.0000

as-5.daf

As	5	1	4.9400	6.8400	22.6000	31.4000	53.8000	57.2000	83.0000	84.5000
As	5	2	4.1000	5.4000	22.4000	28.9000	58.6000	65.4000o		124.5000
As	5	5	4.3000	6.5000	20.1000	26.9000	49.3000	55.6000	89.6000	107.4000
As	5	6	3.8000	5.4000	20.6000	28.3000	56.7000	55.5000	86.4000	96.8000
As	5	7	3.1800	4.7200	23.1000	30.9000	53.8000	63.1000	90.6000	96.6000
As	5	8	4.2000	6.7000	17.8000	25.8000o		47.8000	89.4000	89.4000
As	5	10	1.8000	7.3000	22.5000	29.4000	57.5000	66.0000	93.8000	89.9000
As	5	15	5.4000	7.0000	19.0000	25.6000	46.0000	53.1000	93.6000	99.3000
As	5	20	6.1000	7.5000	24.2000	29.8000	52.9000	58.4000	87.5000	103.1000
As	5	21	4.4000	6.4000	22.2000	28.3000	50.0000	57.0000	87.4000	99.6000
As	5	24	3.8100	7.4200	22.0000	29.4000	56.2000	67.9000	87.0000	126.0000
As	5	25	5.7000	6.9000	22.6000	27.6000	43.2000	58.4000	89.2000	107.0000
As	5	26	5.2000	6.7000	22.0000	28.5000	50.8000	59.3000	88.7000	99.5000
As	5	27	4.0000	7.0000	19.0000	25.0000	47.0000	54.0000	88.0000	88.0000

## STATCALC Input/Output

File Name: as-5  
Data Preparation File (.PRP)

Analyte: As Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

```

***      Results of 5x - 1/5x Mean Error Check      ***
***      Questionable Data (Positive Values)        ***
-----
Total Number of Questionable Observations:      0

```

```

***      Results of Factor of 5 Error Check          ***
***      Questionable Data (All Values)             ***
-----
Conc  Lab  Rep      Mean      Mean      Obs      Ratio
Lev   No   No   Result      Result      Dev      Dev
-----
5     8    1    50.9588    10.8000    7.013    40.159    5.73
7     17   1    92.5823    127.2000   6.375    34.618    5.43
-----
Total Number of Questionable Observations:      2

```

File Name: as-5  
Data Preparation File (.PRP)

Analyte: As Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

```

***      Laboratory Ranking Results                ***
***      Two-Tailed 5% Significance Level          ***
-----
***      Upper Critical Value:    112.0            ***
***      Lower Critical Value:    32.0             ***
-----

```

```

Ranks
-----
Lab  Rank  Level  Level  Level  Level  Level  Level  Level  Level
     Sums   1     2     3     4     5     6     7     8
-----
1    62.0  10.00  8.00   11.50  14.00  9.50   7.00   1.00   1.00
2    85.5  6.00   2.50   9.00   9.00   15.00  13.00  16.00  15.00
5    54.0  8.00   5.00   4.00   4.00   5.00   5.00  10.00  13.00
6    42.0  3.00   2.50   5.00   6.50  13.00   4.00   2.00   6.00
7    66.5  2.00   1.00  13.00  13.00   9.50  11.00  12.00   5.00
8    31.5  7.00   6.50   1.00   3.00   1.00   1.00   9.00   3.00
10   79.5  1.00  12.00  10.00  10.50  14.00  14.00  14.00   4.00
15   52.0  12.00  10.50   2.50   2.00   3.00   2.00  13.00   7.00
16  122.5  16.00  16.00  17.00  17.00  17.00  17.00  11.00  11.50
17  124.0  14.00  15.00  14.00  15.00  16.00  16.00  17.00  17.00
20   87.5  15.00  14.00  15.00  12.00   8.00   8.50   5.00  10.00
21   52.5   9.00   4.00   8.00   6.50   6.00   6.00   4.00   9.00
22  118.0  17.00  17.00  16.00  16.00  11.00  12.00  15.00  14.00
24   80.0   4.00  13.00   6.50  10.50  12.00  15.00   3.00  16.00
25   68.5  13.00   9.00  11.50   5.00   2.00   8.50   8.00  11.50
26   64.0  11.00   6.50   6.50   8.00   7.00  10.00   7.00   8.00
27   34.0   5.00  10.50   2.50   1.00   4.00   3.00   6.00   2.00
-----
*** Laboratory 22 Rejected; Rank Sum 118.0 ***
*** Laboratory 16 Rejected; Rank Sum 122.5 ***
*** Laboratory 17 Rejected; Rank Sum 124.0 ***
-----

```

File Name: as-5  
Data Preparation File (.PRP)

Analyte: As Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

```

***      Outlier Testing Results                    ***
***      Two-Sided 5% Significance Level            ***
-----

```

```

-----
- Outlier(s) -
-----
Lev  Iter  Lab  Rep      Result      Mean      Std Dev      t      Crit t      n
-----
5     1     8    1    10.8000    49.0429    11.9197    3.208    2.507    14
7     1     2    1   106.3000    90.0357     5.4368    2.991    2.507    14
-----

```



File Name: as-5  
Data Preparation File (.PRP)

Analyte: As Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

-----						
- Normality Tests -						
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)	
1	14	W	A	.9561	.874	---
2	14	W	R	.8721	.874	---
3	14	W	A	.9103	.874	---
4	14	W	A	.9643	.874	---
5	13	W	A	.9617	.866	---
6	14	W	A	.9619	.874	---
7	13	W	A	.9466	.866	---
8	14	W	A	.8994	.874	---
-----						
- 1 Normality Rejection(s) -						
-----						

File Name: as-5  
Data Preparation File (.PRP)

Analyte: As Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

		Points As Received	After Lab Ranking		After Outlier Testing	
Lev	Mtrx		Points	%	Points	%
1	5	17	14	82.4	14	82.4
2	5	17	14	82.4	14	82.4
3	5	17	14	82.4	14	82.4
4	5	17	14	82.4	14	82.4
5	5	17	14	82.4	13	76.5
6	5	17	14	82.4	14	82.4
7	5	17	14	82.4	13	76.5
8	5	17	14	82.4	14	82.4
Totals:		136	112	82.4	110	80.9

## STATCALC Input/Output

File Name: as-5  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: As Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)
CONCENTRATION:	4.3521	6.3521	21.1521	27.5521	49.2521	57.3521	87.3521	98.6521
RECOVERY:								
Observations	14	14	14	14	13	14	13	14
Mean Result	4.3521	6.5557	21.4357	28.2714	51.9846	58.4786	88.7846	100.8286
Bias	.0000	.2036	.2836	.7193	2.7325	1.1264	1.4325	2.1764
Relative Bias %	.0000	3.2048	1.3406	2.6106	5.5479	1.9641	1.6399	2.2062
Maximum Result	6.1000	7.5000	24.2000	31.4000	58.6000	67.9000	93.8000	126.0000
Minimum Result	1.8000	4.7200	17.8000	25.0000	43.2000	47.8000	83.0000	84.5000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4	
Observations	14		14		13		13	
Standard Deviation	.8282		.7241		2.7448		7.9030	
Correction Factor	1.0194		1.0194		1.0210		1.0210	
Corrected Std Dev	.8443		.7381		2.8025		8.0692	
Relative Std Dev (%)	15.4798		2.9699		5.0631		8.4912	
OVERALL PRECISION:								
Observations	14	14	14	14	13	14	13	14
Standard Deviation	1.1002	.8273	1.8392	1.9277	4.7609	5.5420	2.8778	12.4076
Correction Factor	1.0194	1.0194	1.0194	1.0194	1.0210	1.0194	1.0210	1.0194
Corrected Std Dev	1.1216	.8433	1.8748	1.9651	4.8610	5.6495	2.9384	12.6483
Relative Std Dev %	25.7701	12.8639	8.7464	6.9508	9.3509	9.6607	3.3095	12.5443

File Name: as-5  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: As Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	4.3521	4.3521	.0000	.00	.000	3.012	NO
2	6.3521	6.5557	.2036	3.20	.553	3.012	NO
3	21.1521	21.4357	.2836	1.34	.495	3.012	NO
4	27.5521	28.2714	.7193	2.61	1.213	3.012	NO
5	49.2521	51.9846	2.7325	5.55	2.020	3.055	NO
6	57.3521	58.4786	1.1264	1.96	.746	3.012	NO
7	87.3521	88.7846	1.4325	1.64	1.684	3.055	NO
8	98.6521	100.8286	2.1764	2.21	.654	3.012	NO

File Name: as-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: As Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	14	71.12	5.3521	.8443	.6984
2	14	24.14	24.3521	.7381	1.3375
3	13	4.29	53.3021	2.8025	2.3112
4	13	.45	93.0021	8.0692	3.6466

- Curvilinear Model -  $s = a \cdot (b \cdot T)$  (  $\ln s = b' \cdot T + a'$  )  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	14	26.02	4.3521	.8443	.6438
2	14	26.02	6.3521	.7381	1.1050
3	13	23.98	21.1521	2.8025	2.5170
4	13	23.98	27.5521	8.0692	7.7831

File Name: as-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: As Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	14	59.11	4.3521	1.1216	.9556
2	14	32.82	6.3521	.8433	1.0976
3	14	3.94	21.1521	1.8748	2.1488
4	14	2.39	27.5521	1.9651	2.6034
5	13	.72	49.2521	4.8610	4.1446
6	14	.58	57.3521	5.6495	4.7199
7	13	.24	87.3521	2.9384	6.8507
8	14	.20	98.6521	12.6483	7.6533

- Curvilinear Model -  $s = a \cdot (b \cdot T)$  (  $\ln s = b' \cdot T + a'$  )  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	14	12.75	4.3521	1.1216	1.1600
2	14	12.75	6.3521	.8433	1.2126
3	14	12.75	21.1521	1.8748	1.6830
4	14	12.75	27.5521	1.9651	1.9393
5	13	11.75	49.2521	4.8610	3.1360
6	14	12.75	57.3521	5.6495	3.7523
7	13	11.75	87.3521	2.9384	7.2927
8	14	12.75	98.6521	12.6483	9.3667

## STATCALC Input/Output

File Name: as-5  
Statistical Analysis File (.STT)

-----  
\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*  
-----

Analyte: As                      Matrix: Reagent Grade Water  
Project: AMQ-TC                Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

=====

Intercept (a): -.0562

Slope (b): 1.0269

=====

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	14	45.16	4.3521	4.3521	4.4132
2	14	34.23	6.3521	6.5557	6.4671
3	14	8.93	21.1521	21.4357	21.6659
4	14	6.08	27.5521	28.2714	28.2384
5	13	2.23	49.2521	51.9846	50.5232
6	14	1.85	57.3521	58.4786	58.8414
7	13	.82	87.3521	88.7846	89.6499
8	14	.70	98.6521	100.8286	101.2544

-----

File Name: as-5  
Statistical Analysis File (.STT)

-----  
\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*  
-----

Analyte: As                      Matrix: Reagent Grade Water  
Project: AMQ-TC                Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

=====

Intercept (e): .5731

Slope (f): .0328

=====

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

=====

Intercept (e): .5537

(f): 1.0281

=====

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

=====

Intercept (e): .7012

Slope (f): .0692

=====

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

=====

Intercept (e): 1.0547

(f): 1.0218

=====

as-8.dat

As	8	1	0.9700	0.9800	5.4200	8.9000	17.3000	23.0000	39.8000	49.8000	81.0000	83.0000
As	8	2	-1.2000	-0.6000	3.3000	6.2000	14.7000	18.9000	34.5000	42.2000	96.8000	109.9000
As	8	5	1.0000	1.1000	5.3000	9.3000	18.9000	24.2000	41.7000	51.0000	90.9000	98.7000
As	8	6	-0.6000	0.2000	4.3000	9.1000	18.0000	23.5000	40.5000	49.7000	91.8000	98.2000
As	8	7	-5.4900	-4.9500	-2.5500	3.3200	10.6000	17.8000	31.7000	39.2000	69.4000	79.0000
As	8	8	2.4000	0.0000	5.2000	9.2000	15.9000	21.7000	33.7000	38.5000	75.3000	67.5000
As	8	10	-1.7000	-2.3000	-1.3000	-1.4000	25.5000	26.2000	51.3000	58.1000	68.9000	90.2000
As	8	15	0.0000	0.6000	4.6000	8.5000	16.7000	22.1000	41.1000	51.5000	92.6000	7.9000
As	8	16	12.2000	7.2000	13.3000	18.3000	28.9000	42.8000	59.4000	64.4000	95.6000	101.0000
As	8	17	1.0000	2.0000	6.0000	10.0000	27.0000	27.0000	48.0000	56.0000	116.0000	120.0000
As	8	20	0.6000	1.5000	5.7000	11.0000	21.0000	26.3000	44.1000	95.5000	94.0000	101.5000
As	8	21	0.8000	0.6000	5.0000	8.4000	17.3000	22.5000	37.8000	44.5000	79.3000	79.6000
As	8	22	12.7000	12.7000	13.0000	14.4000	20.1000	24.6000	35.9000	42.2000	66.7000	71.6000
As	8	24	1.4900	0.0000	7.2200	8.3200	18.6000	18.5000	42.0000	40.1000	90.5000	96.9000
As	8	25	0.0000	0.0000	6.2000	9.3000	13.7000	22.6000	45.1000	44.8000	80.0000	85.6000
As	8	26	0.2000	0.3000	4.5000	10.0000	19.2000	24.6000	40.6000	51.7000	90.3000	94.9000
As	8	27	-2.0000	-2.0000	2.0000	6.0000	14.0000	20.0000	36.0000	45.0000	81.0000	97.0000

File Name: as-5

Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte:  As      Matrix:  Reagent Grade Water
Project:  AMQ-TC   Matrix ID: 5
Date:    12/13/1995 Method:  GFAAS
Pairs:   4
Units:   ug/L

```

Level	1	2	3	4	5	6	7	8
Spike	4.3521	2.0000	14.8000	6.4000	21.7000	8.1000	30.0000	11.3000
Increment	.0000	2.0000	16.8000	23.2000	44.9000	53.0000	83.0000	94.3000

Final Concentration								
Lab ID	4.3521	6.3521	21.1521	27.5521	49.2521	57.3521	87.3521	98.6521
1	4.9400	6.8400	22.6000	31.4000	53.8000	57.2000	83.0000	84.5000
2	4.1000	5.4000	22.4000	28.9000	58.6000	65.4000	106.3000	124.5000
5	4.3000	6.5000	20.1000	26.9000	49.3000	55.6000	89.6000	107.4000
6	3.8000	5.4000	20.6000	28.3000	56.7000	55.5000	86.4000	96.8000
7	3.1800	4.7200	23.1000	30.9000	53.8000	63.1000	90.6000	96.6000
8	4.2000!	6.7000	17.8000!	25.8000	10.8000!	47.8000	89.4000!	89.4000
10	1.8000	7.3000	22.5000	29.4000	57.5000	66.0000	93.8000	89.9000
15	5.4000	7.0000	19.0000	25.6000	46.0000	53.1000	93.6000	99.3000
16	8.3000r	10.0000	31.1000r	36.1000	62.2000r	73.3000	90.0000r	107.0000
17	6.0000r	8.0000	24.0000r	32.0000	62.0000r	68.0000	127.2000r	129.0000
20	6.1000	7.5000	24.2000	29.8000	52.9000	58.4000	87.5000	103.1000
21	4.4000	6.4000	22.2000	28.3000	50.0000	57.0000	87.4000	99.6000
22	11.3000r	11.6000	27.1000r	34.1000	55.5000r	64.6000	96.2000r	120.8000
24	3.8100	7.4200	22.0000	29.4000	56.2000	67.9000	87.0000	126.0000
25	5.7000	6.9000	22.6000	27.6000	43.2000	58.4000	89.2000	107.0000
26	5.2000	6.7000	22.0000	28.5000	50.8000	59.3000	88.7000	99.5000
27	4.0000	7.0000	19.0000	25.0000	47.0000	54.0000	88.0000	88.0000

as-8.daf

As	8	1	.9700	.9800	5.4200	8.9000	17.3000	23.0000	39.8000	49.8000	81.0000	83.0000
As	8	2	-1.2000	-.6000	3.3000	6.2000	14.7000	18.9000	34.5000	42.2000	96.8000	109.9000
As	8	5	1.0000	1.1000	5.3000	9.3000	18.9000	24.2000	41.7000	51.0000	90.9000	98.7000
As	8	6	-.6000	.2000	4.3000	9.1000	18.0000	23.5000	40.5000	49.7000	91.8000	98.2000
As	8	8	2.4000	.0000	5.2000	9.2000	15.9000	21.7000	33.7000	38.5000	75.3000	67.5000
As	8	10	-1.7000	-2.3000	-1.3000o		25.5000	26.2000	51.3000	58.1000	68.9000	90.2000
As	8	15	.0000	.6000	4.6000	8.5000	16.7000	22.1000	41.1000	51.5000	92.6000o	
As	8	20	.6000	1.5000	5.7000	11.0000	21.0000	26.3000	44.1000o		94.0000	101.5000
As	8	21	.8000	.6000	5.0000	8.4000	17.3000	22.5000	37.8000	44.5000	79.3000	79.6000
As	8	22	o	o	o	14.4000	20.1000	24.6000	35.9000	42.2000	66.7000	71.6000
As	8	24	1.4900	.0000	7.2200	8.3200	18.6000	18.5000	42.0000	40.1000	90.5000	96.9000
As	8	25	.0000	.0000	6.2000	9.3000	13.7000	22.6000	45.1000	44.8000	80.0000	85.6000
As	8	26	.2000	.3000	4.5000	10.0000	19.2000	24.6000	40.6000	51.7000	90.3000	94.9000
As	8	27	-2.0000	-2.0000	2.0000	6.0000	14.0000	20.0000	36.0000	45.0000	81.0000	97.0000

## STATCALC Input/Output

File Name: as-8  
Data Preparation File (.PRP)

Analyte: As Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc	Lab	Rep	Mean	Result		Ratio
Lev	No	No	Result			
1	16	1	1.9624	12.2000		6.22
1	22	1	1.9624	12.7000		6.47
1	26	1	1.9624	.2000		.10
2	6	1	1.5988	.2000		.13
2	22	1	1.5988	12.7000		7.94
2	26	1	1.5988	.3000		.19
10	15	1	87.2059	7.9000		.09

Total Number of Questionable Observations: 7

*** Results of Factor of 5 Error Check ***							
*** Questionable Data (All Values) ***							
Conc	Lab	Rep	Mean	Result	Mean	Obs	Ratio
Lev	No	No	Result		Dev	Dev	
2	22	1	1.0194	12.7000	2.283	11.681	5.12
6	16	1	23.9000	42.8000	3.341	18.900	5.66
8	20	1	50.8353	95.5000	8.512	44.665	5.25

Total Number of Questionable Observations: 3

File Name: as-8  
Data Preparation File (.PRP)

Analyte: As Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***			
*** Two-Tailed 5% Significance Level ***			
***			
***	Upper Critical Value:	135.0	***
***	Lower Critical Value:	45.0	***

Ranks											
Lab	Rank	Level	Level	Level	Level	Level	Level	Level	Level	Level	Level
	Sums	1	2	3	4	5	6	7	8	9	10
1	89.0	11.00	12.00	11.00	8.00	7.50	9.00	7.00	10.00	7.50	6.00
2	62.5	4.00	4.00	4.00	4.00	4.00	3.00	3.00	4.50	16.00	16.00
5	115.0	12.50	13.00	10.00	11.50	11.00	11.00	11.00	11.00	11.00	13.00
6	87.0	5.00	8.00	5.00	9.00	9.00	10.00	8.00	9.00	12.00	12.00
7	17.0	1.00	1.00	1.00	2.00	1.00	1.00	1.00	2.00	3.00	4.00
8	59.0	15.00	6.00	9.00	10.00	5.00	5.00	2.00	1.00	4.00	2.00
10	78.0	3.00	2.00	2.00	1.00	15.00	14.00	16.00	15.00	2.00	8.00
15	79.0	6.50	10.50	7.00	7.00	6.00	6.00	10.00	12.00	13.00	1.00
16	162.0	16.00	16.00	17.00	17.00	17.00	17.00	17.00	16.00	15.00	14.00
17	149.0	12.50	15.00	13.00	13.50	16.00	16.00	15.00	14.00	17.00	17.00
20	138.0	9.00	14.00	12.00	15.00	14.00	15.00	13.00	17.00	14.00	15.00
21	71.0	10.00	10.50	8.00	6.00	7.50	7.00	6.00	6.00	5.00	5.00
22	104.0	17.00	17.00	16.00	16.00	13.00	12.50	4.00	4.50	1.00	3.00
24	87.0	14.00	6.00	15.00	5.00	10.00	2.00	12.00	3.00	10.00	10.00
25	82.0	6.50	6.00	14.00	11.50	2.00	8.00	14.00	7.00	6.00	7.00
26	101.0	8.00	9.00	6.00	13.50	12.00	12.50	9.00	13.00	9.00	9.00
27	49.5	2.00	3.00	3.00	3.00	3.00	4.00	5.00	8.00	7.50	11.00

\*\*\* Laboratory 17 Rejected; Rank Sum 149.0 \*\*\*  
\*\*\* Laboratory 16 Rejected; Rank Sum 162.0 \*\*\*  
\*\*\* Laboratory 7 Rejected; Rank Sum 17.0 \*\*\*

File Name: as-8  
Data Preparation File (.PRP)

Analyte: As Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Outlier Testing Results \*\*\*  
\*\*\* Two-Sided 5% Significance Level \*\*\*

-----  
- Outlier(s) -  
-----

Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n
1	1	22	1	12.7000	1.0471	3.5690	3.265	2.507	14
2	1	22	1	12.7000	.9343	3.5517	3.313	2.507	14
3	1	22	1	13.0000	5.0314	3.0838	2.584	2.507	14
4	1	10	1	-1.4000	8.3729	3.4526	2.831	2.507	14
8	1	20	1	95.5000	50.3286	14.0736	3.210	2.507	14
*	1	15	1	7.9000	84.4643	24.9993	3.063	2.507	14

-----

File Name: as-8  
Data Preparation File (.PRP)

Analyte: As Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

-----  
- Normality Tests -  
-----

Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)
1	13	W	A	.9720	.866 ---
2	13	W	A	.8852	.866 ---
3	13	W	R	.8500	.866 ---
4	13	W	A	.8771	.866 ---
5	14	W	A	.9403	.874 ---
6	14	W	A	.9523	.874 ---
7	14	W	A	.9459	.874 ---
8	13	W	A	.9517	.866 ---
9	14	W	A	.9126	.874 ---
10	13	W	A	.9498	.866 ---

-----  
- 1 Normality Rejection(s) -  
-----

File Name: as-8  
Data Preparation File (.PRP)

Analyte: As Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

-----

Lev	Mtrx	Points As Received	After Lab Ranking Points	%	After Outlier Testing Points	%
1	8	17	14	82.4	13	76.5
2	8	17	14	82.4	13	76.5
3	8	17	14	82.4	13	76.5
4	8	17	14	82.4	13	76.5
5	8	17	14	82.4	14	82.4
6	8	17	14	82.4	14	82.4
7	8	17	14	82.4	14	82.4
8	8	17	14	82.4	13	76.5
9	8	17	14	82.4	14	82.4
10	8	17	14	82.4	13	76.5
Totals:		170	140	82.4	134	78.8

-----

## STATCALC Input/Output

File Name: as-8  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: As Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	.0900	.0900	4.2900	8.1900	17.2900	22.2900	38.9900	47.4900	85.1900	91.2900
RECOVERY:										
Observations	13	13	13	13	14	14	14	13	14	13
Mean Result	.1508	.0292	4.4185	9.1246	17.9214	22.7643	40.2929	46.8538	84.2214	90.3538
Bias	.0608	-.0608	.1285	.9346	.6314	.4743	1.3029	-.6362	-.9686	-.9362
Relative Bias %	67.5214	-67.5214	2.9944	11.4117	3.6520	2.1278	3.3415	-1.3396	-1.1370	-1.0255
Maximum Result	2.4000	1.5000	7.2200	14.4000	25.5000	26.3000	51.3000	58.1000	96.8000	109.9000
Minimum Result	-2.0000	-2.3000	-1.3000	6.0000	13.7000	18.5000	33.7000	38.5000	66.7000	67.5000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4		Pair 5	
Observations	13		12		14		13		13	
Standard Deviation	.6576		.8291		1.5588		2.8112		5.1020	
Correction Factor	1.0210		1.0230		1.0194		1.0210		1.0210	
Corrected Std Dev	.6714		.8481		1.5890		2.8703		5.2093	
Relative Std Dev (%)	746.0185		12.5242		7.8112		6.6058		5.9757	
OVERALL PRECISION:										
Observations	13	13	13	13	14	14	14	13	14	13
Standard Deviation	1.2700	1.1146	2.1457	2.0839	3.0964	2.4200	4.6876	5.6082	9.5539	12.2867
Correction Factor	1.0210	1.0210	1.0210	1.0210	1.0194	1.0194	1.0194	1.0210	1.0194	1.0210
Corrected Std Dev	1.2967	1.1381	2.1908	2.1277	3.1565	2.4669	4.7785	5.7262	9.7392	12.5450
Relative Std Dev %	860.0747	3893.4530	49.5833	23.3182	17.6130	10.8368	11.8594	12.2213	11.5638	13.8843

File Name: as-8  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: As Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	.0900	.1508	.0608	67.52	.172	3.055	NO
2	.0900	.0292	-.0608	-67.52	.197	3.055	NO
3	4.2900	4.4185	.1285	2.99	.216	3.055	NO
4	8.1900	9.1246	.9346	11.41	1.617	3.055	NO
5	17.2900	17.9214	.6314	3.65	.763	3.012	NO
6	22.2900	22.7643	.4743	2.13	.733	3.012	NO
7	38.9900	40.2929	1.3029	3.34	1.040	3.012	NO
8	47.4900	46.8538	-.6362	-1.34	.409	3.055	NO
9	85.1900	84.2214	-.9686	-1.14	.379	3.012	NO
10	91.2900	90.3538	-.9362	-1.03	.275	3.055	NO



File Name: as-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: As Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .6307  
Slope (b): .0501  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	63.04	.0900	.6714	.6352
2	12	24.27	6.2400	.8481	.9433
3	14	9.14	19.7900	1.5890	1.6220
4	13	2.73	43.2400	2.8703	2.7967
5	13	.82	88.2400	5.2093	5.0508

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a: .8248 Intercept (a'): -.1927  
b: 1.0231 Slope (b'): .0228  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	20.00	.0900	.6714	.8265
2	12	18.30	.0900	.8481	.9509
3	14	21.70	4.2900	1.5890	1.2954
4	13	20.00	8.1900	2.8703	2.2116
5	13	20.00	17.2900	5.2093	6.1736

File Name: as-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: As Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): 1.2859  
Slope (b): .0992  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	13	32.68	.0900	1.2967	1.2948
2	13	32.68	.0900	1.1381	1.2948
3	13	15.37	4.2900	2.1908	1.7116
4	13	9.21	8.1900	2.1277	2.0986
5	14	4.28	17.2900	3.1565	3.0016
6	14	3.03	22.2900	2.4669	3.4977
7	14	1.29	38.9900	4.7785	5.1549
8	13	.86	47.4900	5.7262	5.9983
9	14	.34	85.1900	9.7392	9.7393
10	13	.27	91.2900	12.5450	10.3446

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a: 1.6314 Intercept (a'): .4895  
b: 1.0232 Slope (b'): .0229  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	13	9.67	.0900	1.2967	1.6348
2	13	9.67	.0900	1.1381	1.6348
3	13	9.67	4.2900	2.1908	1.7998
4	13	9.67	8.1900	2.1277	1.9679
5	14	10.49	17.2900	3.1565	2.4238
6	14	10.49	22.2900	2.4669	2.7178
7	14	10.49	38.9900	4.7785	3.9835
8	13	9.67	47.4900	5.7262	4.8394
9	14	10.49	85.1900	9.7392	11.4725
10	13	9.67	91.2900	12.5450	13.1921

## STATCALC Input/Output

File Name: as-8  
Statistical Analysis File (.STT)

-----  
\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*  
-----

Analyte: As                      Matrix: Freshwater  
Project: AMQ-TC                Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

=====

Intercept (a):	.1635
Slope (b):	1.0043

=====

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	13	28.98	.0900	.1508	.2539
2	13	28.98	.0900	.0292	.2539
3	13	16.59	4.2900	4.4185	4.4719
4	13	11.03	8.1900	9.1246	8.3886
5	14	5.81	17.2900	17.9214	17.5277
6	14	4.28	22.2900	22.7643	22.5491
7	14	1.97	38.9900	40.2929	39.3208
8	13	1.35	47.4900	46.8538	47.8572
9	14	.55	85.1900	84.2214	85.7190
10	13	.45	91.2900	90.3538	91.8452

-----

File Name: as-8  
Statistical Analysis File (.STT)

-----  
\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*  
-----

Analyte: As                      Matrix: Freshwater  
Project: AMQ-TC                Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

=====

Intercept (e):	.4680
Slope (f):	.0499

=====

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

=====

Intercept (e):	.8217
(f):	1.0230

=====

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

=====

Intercept (e):	1.1231
Slope (f):	.0988

=====

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

=====

Intercept (e):	1.6254
(f):	1.0231

=====

as-9.dat

```

As 9 5 14.0000 13.0000 58.0000 70.0000 254.0000 313.0000 614.0000 677.0000 907.0000 974.0000
As 9 6 -4.0000 -3.0000 48.0000 48.0000 219.0000 255.0000 561.0000 611.0000 799.0000 929.0000
As 9 7 -2.1500 2.2600 22.2000 23.3000 163.0000 172.0000 437.0000 470.0000 641.0000 618.0000
As 9 8 3.0000 0.2000 48.4000 65.7000 238.0000 318.0000 422.0000 384.0000 864.0000 760.0000
As 9 10 5.7000 19.5000 36.0000 1.0000 228.0000 213.0000 487.0000 727.0000 727.0000 1040.0000
As 9 15 4.2000 2.7000 32.0000 42.0000 185.0000 242.0000 494.0000 568.0000 749.0000 820.0000
As 9 16 60.0000 60.0000 167.0000 66.0000 367.0000 254.0000 722.0000 833.0000 723.0000 888.0000
As 9 17 3.0000 3.0000 48.0000 58.0000 261.0000 280.0000 560.0000 620.0000 840.0000 880.0000
As 9 20 26.0000 20.0000 67.0000 67.0000 275.0000 320.0000 664.0000 657.0000 896.0000 969.0000
As 9 21 3.0000 2.7000 44.5000 55.0000 220.0000 269.0000 532.0000 578.0000 791.0000 835.0000
As 9 22 14.0000 16.5000 51.9000 66.2000 269.0000 311.0000 491.0000 562.0000 848.0000 793.0000
As 9 24 6.0000 6.2000 47.1000 55.0000 152.0000 168.0000 318.0000 718.0000 919.0000 1167.0000
As 9 25 3.2000 3.2000 42.9000 56.1000 240.0000 267.0000 594.0000 535.0000 861.0000 939.0000
As 9 26 -6.0000 10.0000 54.0000 55.0000 251.0000 313.0000 603.0000 677.0000 831.0000 924.0000
As 9 27 -20.0000 -30.0000 20.0000 30.0000 190.0000 240.0000 530.0000 530.0000 770.0000 770.0000

```

File Name: as-9

Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte: As      Matrix: Estuarine
Project: AMQ-TC   Matrix ID: 9
Date: 12/13/1995 Method: GFAAS
Pairs: 5
Units: ug/L

```

Level	1	2	3	4	5	6	7	8	9	10
Spike	5.4590	.0000	44.9000	11.4000	167.0000	53.0000	270.0000	49.0000	199.0000	59.0000
Increment	.0000	.0000	44.9000	56.3000	223.3000	276.3000	546.3000	595.3000	794.3000	853.3000

Final Concentration															
Lab ID	5.4590	5.4590	50.3590	61.7590	228.7590	281.7590	551.7590	600.7590	799.7590	858.7590					
5	!	14.0000!	13.0000	!	58.0000!	70.0000	!	254.0000!	313.0000	!	614.0000!	677.0000	!	907.0000!	974.0000
6		-4.0000	-3.0000		48.0000	48.0000		219.0000	255.0000		561.0000	611.0000		799.0000	929.0000
7	r	-2.1500r	2.2600	r	22.2000r	23.3000	r	163.0000r	172.0000	r	437.0000r	470.0000	r	641.0000r	618.0000
8		3.0000	.2000		48.4000	65.7000		238.0000	318.0000		422.0000	384.0000		864.0000	760.0000
10		5.7000	19.5000		36.0000o	1.0000		228.0000	213.0000		487.0000	727.0000		727.0000	1040.0000
15		4.2000	2.7000		32.0000	42.0000		185.0000	242.0000		494.0000	568.0000		749.0000	820.0000
16	o	60.0000o	60.0000	o	167.0000	66.0000	o	367.0000	254.0000		722.0000	833.0000		723.0000	888.0000
17		3.0000	3.0000		48.0000	58.0000		261.0000	280.0000		560.0000	620.0000		840.0000	880.0000
20	r	26.0000r	20.0000	r	67.0000r	67.0000	r	275.0000r	320.0000	r	664.0000r	657.0000	r	896.0000r	969.0000
21		3.0000	2.7000		44.5000	55.0000		220.0000	269.0000		532.0000	578.0000		791.0000	835.0000
22		14.0000	16.5000		51.9000	66.2000		269.0000	311.0000		491.0000	562.0000		848.0000	793.0000
24		6.0000	6.2000		47.1000	55.0000		152.0000	168.0000		318.0000	718.0000		919.0000	1167.0000
25		3.2000	3.2000		42.9000	56.1000		240.0000	267.0000		594.0000	535.0000		861.0000	939.0000
26		-6.0000	10.0000		54.0000	55.0000		251.0000	313.0000		603.0000	677.0000		831.0000	924.0000
27	r	-20.0000r	-30.0000	r	20.0000r	30.0000	r	190.0000r	240.0000	r	530.0000r	530.0000	r	770.0000r	770.0000

as-9.daf

```

As 9 5 14.0000 13.0000 58.0000 70.0000 254.0000 313.0000 614.0000 677.0000 907.0000 974.0000
As 9 6 -4.0000 -3.0000 48.0000 48.0000 219.0000 255.0000 561.0000 611.0000 799.0000 929.0000
As 9 8 3.0000 .2000 48.4000 65.7000 238.0000 318.0000 422.0000 384.0000 864.0000 760.0000
As 9 10 5.7000 19.5000 36.0000o 1.0000 228.0000 213.0000 487.0000 727.0000 727.0000 1040.0000
As 9 15 4.2000 2.7000 32.0000 42.0000 185.0000 242.0000 494.0000 568.0000 749.0000 820.0000
As 9 16 o 66.0000o 254.0000 722.0000 833.0000 723.0000 888.0000
As 9 17 3.0000 3.0000 48.0000 58.0000 261.0000 280.0000 560.0000 620.0000 840.0000 880.0000
As 9 21 3.0000 2.7000 44.5000 55.0000 220.0000 269.0000 532.0000 578.0000 791.0000 835.0000
As 9 22 14.0000 16.5000 51.9000 66.2000 269.0000 311.0000 491.0000 562.0000 848.0000 793.0000
As 9 24 6.0000 6.2000 47.1000 55.0000 152.0000 168.0000 318.0000 718.0000 919.0000 1167.0000
As 9 25 3.2000 3.2000 42.9000 56.1000 240.0000 267.0000 594.0000 535.0000 861.0000 939.0000
As 9 26 -6.0000 10.0000 54.0000 55.0000 251.0000 313.0000 603.0000 677.0000 831.0000 924.0000

```

## STATCALC Input/Output

File Name: as-9  
Data Preparation File (.PRP)

Analyte: As Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc	Lab	Rep	Mean	Result		Ratio
Lev	No	No	Result			
1	16	1	9.4733	60.0000		6.33
2	8	1	10.6173	.2000		.02
2	16	1	10.6173	60.0000		5.65
4	10	1	50.5533	1.0000		.02

Total Number of Questionable Observations: 4

*** Results of Factor of 5 Error Check ***						
*** Questionable Data (All Values) ***						
Conc	Lab	Rep	Mean	Mean	Obs	
Lev	No	No	Result	Result	Dev	Dev Ratio
3	16	1	52.4667	167.0000	18.151	114.533 6.31

Total Number of Questionable Observations: 1

File Name: as-9  
Data Preparation File (.PRP)

Analyte: As Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***		
*** Two-Tailed 5% Significance Level ***		
***		
***	Upper Critical Value:	119.0 ***
***	Lower Critical Value:	40.0 ***

Ranks												
Lab	Rank Sums	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Level 8	Level 9	Level 10	
5	126.5	12.50	11.00	13.00	15.00	11.00	12.50	13.00	11.50	14.00	13.00	
6	65.5	3.00	2.00	8.50	5.00	5.00	7.00	10.00	8.00	7.00	10.00	
7	23.0	4.00	4.00	2.00	2.00	2.00	2.00	3.00	2.00	1.00	1.00	
8	69.0	6.00	3.00	10.00	11.00	8.00	14.00	2.00	1.00	12.00	2.00	
10	73.0	10.00	13.00	4.00	1.00	7.00	3.00	4.00	14.00	3.00	14.00	
15	50.5	9.00	5.50	3.00	4.00	3.00	5.00	6.00	6.00	4.00	5.00	
16	118.0	15.00	15.00	15.00	12.00	15.00	6.00	15.00	15.00	2.00	8.00	
17	87.5	6.00	7.00	8.50	10.00	12.00	10.00	9.00	9.00	9.00	7.00	
20	134.0	14.00	14.00	14.00	14.00	14.00	15.00	14.00	10.00	13.00	12.00	
21	66.5	6.00	5.50	6.00	7.00	6.00	9.00	8.00	7.00	6.00	6.00	
22	96.5	12.50	12.00	11.00	13.00	13.00	11.00	5.00	5.00	10.00	4.00	
24	80.0	11.00	9.00	7.00	7.00	1.00	1.00	1.00	13.00	15.00	15.00	
25	84.0	8.00	8.00	5.00	9.00	9.00	8.00	11.00	4.00	11.00	11.00	
26	94.0	2.00	10.00	12.00	7.00	10.00	12.50	12.00	11.50	8.00	9.00	
27	32.0	1.00	1.00	1.00	3.00	4.00	4.00	7.00	3.00	5.00	3.00	
*** Laboratory 27 Rejected; Rank Sum 32.0 ***												
*** Laboratory 20 Rejected; Rank Sum 134.0 ***												
*** Laboratory 7 Rejected; Rank Sum 23.0 ***												

File Name: as-9  
Data Preparation File (.PRP)

Analyte: As Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Outlier Testing Results ***		
*** Two-Sided 5% Significance Level ***		

- Outlier(s) -											
Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n		
1	1	16	1	60.0000	8.8417	17.1339	2.986	2.412	12		
2	1	16	1	60.0000	11.1667	16.8049	2.906	2.412	12		
3	1	16	1	167.0000	56.4833	35.5321	3.110	2.412	12		
4	1	10	1	1.0000	53.1667	18.3149	2.848	2.412	12		
5	1	16	1	367.0000	240.3333	51.7728	2.447	2.412	12		

File Name: as-9  
Data Preparation File (.PRP)

Analyte: As Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

- Normality Tests -						
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)	
1	11	W	A	.8966	.850	---
2	11	W	A	.9238	.850	---
3	11	W	A	.9537	.850	---
4	11	W	A	.9332	.850	---
5	11	W	A	.9010	.850	---
6	12	W	A	.9106	.859	---
7	12	W	A	.9680	.859	---
8	12	W	A	.9691	.859	---
9	12	W	A	.9459	.859	---
10	12	W	A	.9445	.859	---
- 0 Normality Rejection(s) -						

File Name: as-9  
Data Preparation File (.PRP)

Analyte: As Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

Lev	Mtrx	Points As Received	After Lab Ranking		After Outlier Testing	
			Points	%	Points	%
1	9	15	12	80.0	11	73.3
2	9	15	12	80.0	11	73.3
3	9	15	12	80.0	11	73.3
4	9	15	12	80.0	11	73.3
5	9	15	12	80.0	11	73.3
6	9	15	12	80.0	12	80.0
7	9	15	12	80.0	12	80.0
8	9	15	12	80.0	12	80.0
9	9	15	12	80.0	12	80.0
10	9	15	12	80.0	12	80.0
Totals:		150	120	80.0	115	76.7

## STATCALC Input/Output

File Name: as-9  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: As Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	5.4590	5.4590	50.3590	61.7590	228.7590	281.7590	551.7590	600.7590	799.7590	858.7590
RECOVERY:										
Observations	11	11	11	11	11	12	12	12	12	12
Mean Result	4.1909	6.7273	46.4364	57.9091	228.8182	266.9167	533.1667	624.1667	821.5833	912.4167
Bias	-1.2681	1.2683	-3.9226	-3.8499	.0592	-14.8423	-18.5924	23.4076	21.8243	53.6576
Relative Bias %	-23.2294	23.2327	-7.7893	-6.2338	.0259	-5.2677	-3.3697	3.8963	2.7289	6.2483
Maximum Result	14.0000	19.5000	58.0000	70.0000	269.0000	318.0000	722.0000	833.0000	919.0000	1167.0000
Minimum Result	-6.0000	-3.0000	32.0000	42.0000	152.0000	168.0000	318.0000	384.0000	723.0000	760.0000
SINGLE OPERATOR PRECISION:	Pair 1	Pair 2	Pair 3	Pair 4	Pair 5					
Observations	11	10	11	12	12					
Standard Deviation	4.4393	3.8747	18.7619	86.2481	81.5279					
Correction Factor	1.0253	1.0281	1.0253	1.0230	1.0230					
Corrected Std Dev	4.5515	3.9836	19.2361	88.2279	83.3995					
Relative Std Dev (%)	83.3743	7.6354	7.7348	15.2468	9.6193					
OVERALL PRECISION:										
Observations	11	11	11	11	11	12	12	12	12	12
Standard Deviation	6.1169	7.1062	7.5070	8.4914	34.6145	45.3240	102.8519	114.2349	65.1173	112.6825
Correction Factor	1.0253	1.0253	1.0253	1.0253	1.0253	1.0230	1.0230	1.0230	1.0230	1.0230
Corrected Std Dev	6.2715	7.2858	7.6967	8.7060	35.4893	46.3644	105.2130	116.8572	66.6121	115.2693
Relative Std Dev %	149.6460	108.3025	16.5747	15.0340	15.5098	17.3704	19.7336	18.7221	8.1078	12.6334

File Name: as-9  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: As Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	5.4590	4.1909	-1.2681	-23.23	.689	3.169	NO
2	5.4590	6.7273	1.2683	23.23	.592	3.169	NO
3	50.3590	46.4364	-3.9226	-7.79	1.733	3.169	NO
4	61.7590	57.9091	-3.8499	-6.23	1.504	3.169	NO
5	228.7590	228.8182	.0592	.03	.006	3.169	NO
6	281.7590	266.9167	-14.8423	-5.27	1.134	3.106	NO
7	551.7590	533.1667	-18.5924	-3.37	.626	3.106	NO
8	600.7590	624.1667	23.4076	3.90	.710	3.106	NO
9	799.7590	821.5833	21.8243	2.73	1.161	3.106	NO
10	858.7590	912.4167	53.6576	6.25	1.650	3.106	NO

File Name: as-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: As Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	11	95.68	5.4590	4.5515	4.3619
2	10	3.97	56.0590	3.9836	8.7012
3	11	.26	255.2590	19.2361	25.7840
4	12	.06	576.2590	88.2279	53.3121
5	12	.03	829.2590	83.3995	75.0087

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a:	4.8596	Intercept (a'):	1.5810
b:	1.0040	Slope (b'):	.0040

=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	11	19.60	5.4590	4.5515	4.9672
2	10	17.60	5.4590	3.9836	6.0847
3	11	19.60	50.3590	19.2361	13.5267
4	12	21.60	61.7590	88.2279	49.0099
5	12	21.60	228.7590	83.3995	135.1886

File Name: as-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: As Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	11	34.83	5.4590	6.2715	5.5259
2	11	34.83	5.4590	7.2858	5.5259
3	11	13.57	50.3590	7.6967	11.6558
4	11	11.31	61.7590	8.7060	13.2122
5	11	2.18	228.7590	35.4893	36.0116
6	12	1.73	281.7590	46.3644	43.2473
7	12	.55	551.7590	105.2130	80.1086
8	12	.48	600.7590	116.8572	86.7982
9	12	.28	799.7590	66.6121	113.9663
10	12	.25	858.7590	115.2693	122.0212

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a:	9.2703	Intercept (a'):	2.2268
b:	1.0034	Slope (b'):	.0034

=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	11	9.51	5.4590	6.2715	9.4422
2	11	9.51	5.4590	7.2858	9.4422
3	11	9.51	50.3590	7.6967	10.9827
4	11	9.51	61.7590	8.7060	11.4123
5	11	9.51	228.7590	35.4893	20.0217
6	12	10.49	281.7590	46.3644	23.9319
7	12	10.49	551.7590	105.2130	59.3841
8	12	10.49	600.7590	116.8572	70.0325
9	12	10.49	799.7590	66.6121	136.8368
10	12	10.49	858.7590	115.2693	166.8979

## STATCALC Input/Output

File Name: as-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: As Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): -.7400  
Slope (b): 1.0034

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	11	40.73	5.4590	4.1909	4.7378
2	11	40.73	5.4590	6.7273	4.7378
3	11	9.15	50.3590	46.4364	49.7922
4	11	7.12	61.7590	57.9091	61.2314
5	11	.96	228.7590	228.8182	228.8058
6	12	.73	281.7590	266.9167	281.9881
7	12	.21	551.7590	533.1667	552.9168
8	12	.18	600.7590	624.1667	602.0853
9	12	.10	799.7590	821.5833	801.7698
10	12	.09	858.7590	912.4167	860.9727

File Name: as-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: As Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): 4.6312  
Slope (f): .0855

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 4.8740  
(f): 1.0040

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): 5.5181  
Slope (f): .1361

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 9.2933  
(f): 1.0034



as-10.dat

```

As 10 1 3.9000 5.7000 65.7000 98.2000 316.0000 387.0000 660.0000 684.0000 510.0000 670.0000
As 10 2 -0.5000 -1.1000 58.0000 66.0000 300.0000 37.7000 712.0000 816.0000 993.0000 1089.0000
As 10 5 12.0000 19.0000 82.0000 108.0000 341.0000 424.0000 731.0000 802.0000 917.0000 984.0000
As 10 6 5.0000 5.0000 81.0000 119.0000 367.0000 481.0000 811.0000 879.0000 965.0000 1026.0000
As 10 7 -4.4200 5.4800 57.0000 83.0000 321.0000 403.0000 697.0000 772.0000 841.0000 938.0000
As 10 8 0.0000 0.0000 18.3000 20.7000 45.4000 40.8000 836.0000 944.0000 928.0000 992.0000
As 10 10 36.0000 6.0000 45.0000 58.0000 217.0000 474.0000 739.0000 668.0000 790.0000 917.0000
As 10 15 4.7000 3.0000 62.0000 81.0000 288.0000 348.0000 736.0000 595.0000 775.0000 931.0000
As 10 16 52.2000 9.0000 175.0000 122.0000 422.0000 589.0000 800.0000 770.0000 988.0000 112.0000
As 10 17 6.0000 57.0000 100.0000 140.0000 400.0000 490.0000 220.0000 930.0000 1080.0000 770.0000
As 10 20 13.0000 18.0000 94.0000 118.0000 364.0000 448.0000 779.0000 855.0000 952.0000 1062.0000
As 10 21 37.0000 37.9000 59.0000 87.0000 310.0000 389.0000 633.0000 675.0000 765.0000 819.0000
As 10 24 21.4000 21.5000 96.6000 158.0000 375.0000 680.0000 779.0000 950.0000 1090.0000 1156.0000
As 10 25 0.0000 0.0000 52.8000 294.0000 380.0000 384.0000 648.0000 713.0000 818.0000 889.0000
As 10 26 -1.0000 -1.0000 64.0000 84.0000 323.0000 394.0000 725.0000 737.0000 904.0000 973.0000
As 10 27 -20.0000 -10.0000 60.0000 90.0000 350.0000 430.0000 670.0000 810.0000 840.0000 960.0000

```

File Name: as-10  
Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte: As      Matrix: Acid Mine Drainage
Project: AMQ-TC   Matrix ID: 10
Date: 12/13/1995 Method: GFAAS
Pairs: 5
Units: ug/L

```

Level	1	2	3	4	5	6	7	8	9	10
Spike	8.3055	.0000	63.8000	30.4000	229.0000	82.0000	288.0000	70.0000	101.0000	70.0000
Spike Increment	.0000	.0000	63.8000	94.2000	323.2000	405.2000	693.2000	763.2000	864.2000	934.2000

Final Concentration										
Lab ID	8.3055	8.3055	72.1055	102.5055	331.5055	413.5055	701.5055	771.5055	872.5055	942.5055
1	3.9000	5.7000	65.7000	98.2000	316.0000	387.0000	660.0000	684.0000	510.0000	670.0000
2	-.5000	-1.1000	58.0000	66.0000	300.0000	37.7000	712.0000	816.0000	993.0000	1089.0000
5	12.0000	19.0000	82.0000	108.0000	341.0000	424.0000	731.0000	802.0000	917.0000	984.0000
6	5.0000	5.0000	81.0000	119.0000	367.0000	481.0000	811.0000	879.0000	965.0000	1026.0000
7	-4.4200	5.4800	57.0000	83.0000	321.0000	403.0000	697.0000	772.0000	841.0000	938.0000
8	.0000	.0000	18.3000	20.7000	45.4000	40.8000	836.0000	944.0000	928.0000	992.0000
10	36.0000	6.0000	45.0000	58.0000	217.0000	474.0000	739.0000	668.0000	790.0000	917.0000
15	4.7000	3.0000	62.0000	81.0000	288.0000	348.0000	736.0000	595.0000	775.0000	931.0000
16	52.2000	9.0000	175.0000	122.0000	422.0000	589.0000	800.0000	770.0000	988.0000	112.0000
17	6.0000	57.0000	100.0000	140.0000	400.0000	490.0000	220.0000	930.0000	1080.0000	770.0000
20	13.0000	18.0000	94.0000	118.0000	364.0000	448.0000	779.0000	855.0000	952.0000	1062.0000
21	37.0000	37.9000	59.0000	87.0000	310.0000	389.0000	633.0000	675.0000	765.0000	819.0000
24	21.4000	21.5000	96.6000	158.0000	375.0000	680.0000	779.0000	950.0000	1090.0000	1156.0000
25	.0000	.0000	52.8000	294.0000	380.0000	384.0000	648.0000	713.0000	818.0000	889.0000
26	-1.0000	-1.0000	64.0000	84.0000	323.0000	394.0000	725.0000	737.0000	904.0000	973.0000
27	-20.0000	-10.0000	60.0000	90.0000	350.0000	430.0000	670.0000	810.0000	840.0000	960.0000

as-5.daf

```

As 10 1 3.9000 5.7000 65.7000 98.2000 316.0000 387.0000 660.0000 684.0000 510.0000 670.0000
As 10 2 -.5000 -1.1000 58.0000 66.0000 300.0000 37.7000 712.0000 816.0000 993.0000 1089.0000
As 10 5 12.0000 19.0000 82.0000 108.0000 341.0000 424.0000 731.0000 802.0000 917.0000 984.0000
As 10 6 5.0000 5.0000 81.0000 119.0000 367.0000 481.0000 811.0000 879.0000 965.0000 1026.0000
As 10 7 -4.4200 5.4800 57.0000 83.0000 321.0000 403.0000 697.0000 772.0000 841.0000 938.0000
As 10 8 .0000 .0000 18.3000 20.7000 45.4000 40.8000 836.0000 944.0000 928.0000 992.0000
As 10 10 36.0000 6.0000 45.0000 58.0000 217.0000 474.0000 739.0000 668.0000 790.0000 917.0000
As 10 15 4.7000 3.0000 62.0000 81.0000 288.0000 348.0000 736.0000 595.0000 775.0000 931.0000
As 10 16 52.2000 9.0000 175.0000 122.0000 422.0000 589.0000 800.0000 770.0000 988.0000 112.0000
As 10 17 6.0000 57.0000 100.0000 140.0000 400.0000 490.0000 220.0000 930.0000 1080.0000 770.0000
As 10 20 13.0000 18.0000 94.0000 118.0000 364.0000 448.0000 779.0000 855.0000 952.0000 1062.0000
As 10 21 37.0000 37.9000 59.0000 87.0000 310.0000 389.0000 633.0000 675.0000 765.0000 819.0000
As 10 25 .0000 .0000 52.8000 294.0000 380.0000 384.0000 648.0000 713.0000 818.0000 889.0000
As 10 26 -1.0000 -1.0000 64.0000 84.0000 323.0000 394.0000 725.0000 737.0000 904.0000 973.0000
As 10 27 -20.0000 -10.0000 60.0000 90.0000 350.0000 430.0000 670.0000 810.0000 840.0000 960.0000

```

## STATCALC Input/Output

File Name: as-10  
Data Preparation File (.PRP)

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc	Lab	Rep	Mean	Result		Ratio
Lev	No	No	Result			
4	8	1	107.9313	20.7000		.19
5	8	1	319.9625	45.4000		.14
6	2	1	399.9688	37.7000		.09
6	8	1	399.9688	40.8000		.10
10	16	1	893.0000	112.0000		.13

Total Number of Questionable Observations: 5

*** Results of Factor of 5 Error Check ***						
*** Questionable Data (All Values) ***						
Conc	Lab	Rep	Mean	Result	Mean	Obs
Lev	No	No	Result		Dev	Dev
7	17	1	698.5000	220.0000	82.875	478.500
10	16	1	893.0000	112.0000	150.625	781.000

Total Number of Questionable Observations: 2

File Name: as-10  
Data Preparation File (.PRP)

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***		
*** Two-Tailed 5% Significance Level ***		
***	Upper Critical Value:	127.0
***	Lower Critical Value:	42.0

Ranks											
Lab	Rank Sums	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Level 8	Level 9	Level 10
1	57.0	7.00	9.00	10.00	9.00	6.00	5.00	4.00	4.00	1.00	2.00
2	66.0	4.00	2.00	5.00	5.00	3.00	4.00	1.00	7.00	11.00	15.00
5	102.0	11.00	13.00	12.00	10.00	9.00	9.00	9.00	9.00	9.00	11.00
6	117.0	9.00	7.00	11.00	12.00	12.00	13.00	15.00	13.00	12.00	13.00
7	63.0	2.00	8.00	4.00	5.00	7.00	8.00	6.00	8.00	7.00	8.00
8	68.0	5.50	4.50	1.00	1.00	1.00	2.00	16.00	15.00	10.00	12.00
10	65.0	14.00	10.00	2.00	2.00	2.00	12.00	11.00	2.00	4.00	6.00
15	53.0	8.00	6.00	8.00	4.00	3.00	3.00	10.00	1.00	3.00	7.00
16	122.0	16.00	11.00	16.00	13.00	16.00	15.00	14.00	7.00	13.00	1.00
17	117.0	10.00	16.00	15.00	14.00	15.00	14.00	1.00	14.00	15.00	3.00
20	119.5	12.00	12.00	13.00	11.00	11.00	11.00	12.50	12.00	11.00	14.00
21	65.0	15.00	15.00	6.00	7.00	5.00	6.00	2.00	3.00	2.00	4.00
24	145.5	13.00	14.00	14.00	15.00	13.00	16.00	12.50	16.00	16.00	16.00
25	65.0	5.50	4.50	3.00	16.00	14.00	4.00	3.00	5.00	5.00	5.00
26	68.0	3.00	3.00	9.00	6.00	8.00	7.00	8.00	6.00	8.00	10.00
27	67.0	1.00	1.00	7.00	8.00	10.00	10.00	5.00	10.00	6.00	9.00

\*\*\* Laboratory 24 Rejected; Rank Sum 145.5 \*\*\*

File Name: as-10  
Data Preparation File (.PRP)

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Outlier Testing Results ***		
*** Two-Sided 5% Significance Level ***		

- Outlier(s) -										
Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n	
2	1	17	1	57.0000	10.2653	17.1245	2.729	2.549	15	
3	1	16	1	175.0000	71.5867	34.8204	2.970	2.549	15	
4	1	25	1	294.0000	104.5933	60.0828	3.152	2.549	15	
5	1	8	1	45.4000	316.2933	89.9398	3.012	2.549	15	
7	1	17	1	220.0000	693.1334	144.1724	3.282	2.549	15	
9	1	1	1	510.0000	871.0667	135.2534	2.670	2.549	15	
*	1	16	1	112.0000	875.4667	238.0549	3.207	2.549	15	

File Name: as-10  
Data Preparation File (.PRP)

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

- Normality Tests -						
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)	
1	15	W	R	.8684	.881	---
2	14	W	R	.8646	.874	---
3	14	W	A	.9406	.874	---
4	14	W	A	.9601	.874	---
5	14	W	A	.9699	.874	---
6	15	W	R	.7727	.881	---
7	14	W	A	.9622	.874	---
8	15	W	A	.9778	.881	---
9	14	W	A	.9551	.874	---
10	14	W	A	.9393	.874	---

- 3 Normality Rejection(s) -

File Name: as-10  
Data Preparation File (.PRP)

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

Lev	Mtrx	Points As Received	After Lab Ranking		After Outlier Testing	
			Points	%	Points	%
1	10	16	15	93.8	15	93.8
2	10	16	15	93.8	14	87.5
3	10	16	15	93.8	14	87.5
4	10	16	15	93.8	14	87.5
5	10	16	15	93.8	14	87.5
6	10	16	15	93.8	15	93.8
7	10	16	15	93.8	14	87.5
8	10	16	15	93.8	15	93.8
9	10	16	15	93.8	14	87.5
10	10	16	15	93.8	14	87.5
Totals:		160	150	93.8	143	89.4

## STATCALC Input/Output

File Name: as-10  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	8.3055	8.3055	72.1055	102.5055	331.5055	413.5055	701.5055	771.5055	872.5055	942.5055
RECOVERY:										
Observations	15	14	14	14	14	15	14	15	14	14
Mean Result	9.5920	6.9271	64.2000	91.0643	335.6429	381.3000	726.9286	776.6667	896.8571	930.0000
Bias	1.2865	-1.3784	-7.9055	-11.4412	4.1374	-32.2055	25.4231	5.1612	24.3517	-12.5055
Relative Bias %	15.4897	-16.5957	-10.9638	-11.1616	1.2481	-7.7884	3.6241	.6690	2.7910	-1.3268
Maximum Result	52.2000	37.9000	100.0000	140.0000	422.0000	589.0000	836.0000	944.0000	1080.0000	1089.0000
Minimum Result	-20.0000	-10.0000	18.3000	20.7000	217.0000	37.7000	633.0000	595.0000	765.0000	670.0000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4		Pair 5	
Observations	14		13		14		14		13	
Standard Deviation	10.6085		7.8177		79.0047		53.5711		81.5664	
Correction Factor	1.0194		1.0210		1.0194		1.0194		1.0210	
Corrected Std Dev	10.8143		7.9821		80.5372		54.6102		83.2815	
Relative Std Dev (%)	130.2064		10.2820		22.4176		7.2557		9.1175	
OVERALL PRECISION:										
Observations	15	14	14	14	14	15	14	15	14	14
Standard Deviation	18.5969	11.6531	20.5992	30.5109	51.6074	150.7063	62.7295	100.3022	94.6360	113.9723
Correction Factor	1.0180	1.0194	1.0194	1.0194	1.0194	1.0180	1.0194	1.0180	1.0194	1.0194
Corrected Std Dev	18.9317	11.8792	20.9988	31.1027	52.6085	153.4194	63.9463	102.1078	96.4717	116.1831
Relative Std Dev %	197.3696	171.4876	32.7084	34.1547	15.6739	40.2359	8.7968	13.1469	10.7566	12.4928

File Name: as-10  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	8.3055	9.5920	1.2865	15.49	.268	2.977	NO
2	8.3055	6.9271	-1.3784	-16.60	.443	3.012	NO
3	72.1055	64.2000	-7.9055	-10.96	1.436	3.012	NO
4	102.5055	91.0643	-11.4412	-11.16	1.403	3.012	NO
5	331.5055	335.6429	4.1374	1.25	.300	3.012	NO
6	413.5055	381.3000	-32.2055	-7.79	.828	2.977	NO
7	701.5055	726.9286	25.4231	3.62	1.516	3.012	NO
8	771.5055	776.6667	5.1612	.67	.199	2.977	NO
9	872.5055	896.8571	24.3517	2.79	.963	3.012	NO
10	942.5055	930.0000	-12.5055	-1.33	.411	3.012	NO

File Name: as-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): 8.6122  
Slope (b): .0977  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	14	57.04	8.3055	10.8143	9.4237
2	13	29.05	87.3055	7.9821	17.1421
3	14	8.49	372.5055	80.5372	45.0068
4	14	3.26	736.5055	54.6102	80.5703
5	13	2.16	907.5055	83.2815	97.2774

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

a: 11.5809 Intercept (a'): 2.4494  
b: 1.0024 Slope (b'): .0024  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	14	20.65	8.3055	10.8143	11.8148
2	13	19.03	8.3055	7.9821	14.2896
3	14	20.65	72.1055	80.5372	28.3919
4	14	20.65	102.5055	54.6102	68.1950
5	13	19.03	331.5055	83.2815	102.9276

File Name: as-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): 16.6175  
Slope (b): .1264  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	15	27.17	8.3055	18.9317	17.6675
2	14	25.20	8.3055	11.8792	17.6675
3	14	16.70	72.1055	20.9988	25.7334
4	14	14.10	102.5055	31.1027	29.5768
5	14	5.42	331.5055	52.6085	58.5282
6	15	4.53	413.5055	153.4194	68.8951
7	14	2.08	701.5055	63.9463	105.3056
8	15	1.95	771.5055	102.1078	114.1554
9	14	1.51	872.5055	96.4717	126.9243
10	14	1.34	942.5055	116.1831	135.7741

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

a: 21.4233 Intercept (a'): 3.0645  
b: 1.0020 Slope (b'): .0020  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	15	10.54	8.3055	18.9317	21.7817
2	14	9.77	8.3055	11.8792	21.7817
3	14	9.77	72.1055	20.9988	24.7419
4	14	9.77	102.5055	31.1027	26.2908
5	14	9.77	331.5055	52.6085	41.5378
6	15	10.54	413.5055	153.4194	48.9297
7	14	9.77	701.5055	63.9463	86.9744
8	15	10.54	771.5055	102.1078	100.0257
9	14	9.77	872.5055	96.4717	122.3831
10	14	9.77	942.5055	116.1831	140.7478

## STATCALC Input/Output

File Name: as-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): -2.6439  
Slope (b): .9988

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	15	34.00	8.3055	9.5920	5.6517
2	14	31.73	8.3055	6.9271	5.6517
3	14	14.96	72.1055	64.2000	69.3759
4	14	11.32	102.5055	91.0643	99.7397
5	14	2.89	331.5055	335.6429	328.4675
6	15	2.24	413.5055	381.3000	410.3700
7	14	.89	701.5055	726.9286	698.0276
8	15	.81	771.5055	776.6667	767.9445
9	14	.61	872.5055	896.8571	868.8244
10	14	.54	942.5055	930.0000	938.7411

File Name: as-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: As Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): 11.2593  
Slope (f): .0978

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 11.6549  
(f): 1.0024

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): 19.2645  
Slope (f): .1266

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 21.5369  
(f): 1.0020

cd-5.dat

Cd	5	1	0.0200	-0.0200	0.5700	1.0000	2.1800	3.0800	4.7100	5.8500	8.1100	9.7000
Cd	5	2	0.0000	0.0000	0.7000	1.3000	4.1000	3.9000	6.4000	7.8000	8.4000	9.6000
Cd	5	6	-0.1000	-0.1000	0.5000	1.1000	2.5000	3.3000	5.2000	6.7000	8.5000	9.7000
Cd	5	7	-0.0175	-0.0646	0.5020	0.9860	2.3000	3.2400	5.0900	6.4100	7.1000	8.8000
Cd	5	8	0.2000	0.1000	0.8000	1.6000	3.0000	3.9000	5.3000	6.4000	8.2000	9.4000
Cd	5	10	0.0000	-0.1000	0.4500	1.1000	2.2000	2.6000	4.8000	5.5000	7.2000	7.3000
Cd	5	11	0.0000	1.0000	0.7000	1.7000	2.4000	3.3000	4.6000	5.8000	8.5000	9.9000
Cd	5	15	0.1000	0.0000	0.6000	1.1000	2.2000	3.0000	4.9000	6.2000	9.0000	10.2000
Cd	5	16	-0.0010	-0.0010	-0.0010	1.1000	0.0000	1.1000	2.2000	3.3000	4.4000	5.5000
Cd	5	17	0.1000	0.0000	0.4000	26.7000	2.1000	3.5000	17.6000	6.5000	9.6000	18.6000
Cd	5	20	0.0000	0.0000	0.5000	1.1000	2.4000	3.2000	4.8000	6.1000	8.7000	10.0000
Cd	5	21	0.1000	0.1000	0.6000	1.1000	2.4000	3.2000	4.8000	6.1000	8.7000	9.5000
Cd	5	22	-0.0800	-0.1100	0.6200	1.0700	2.8000	3.4000	4.8000	6.0500	8.7000	10.0000
Cd	5	24	0.2500	0.2400	0.8100	1.3400	3.2200	3.6900	6.0900	6.2200	9.0800	10.8000
Cd	5	25	0.1000	0.1000	0.6000	1.1000	2.4000	3.1000	4.7000	6.5000	8.6000	9.9000
Cd	5	26	-0.2000	-0.2000	0.6000	1.3000	2.6000	3.4000	4.9000	6.5000	9.0000	11.0000
Cd	5	27	0.1000	0.1000	0.6000	1.1000	2.0000	2.7000	4.0000	4.2000	8.3000	9.3000

File Name: cd-5

Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte:  Cd      Matrix:  Reagent Grade Water
Project:  AMQ-TC   Matrix ID: 5
Date:    12/13/1995 Method:  GFAAS
Pairs:   5
Units:   ug/L

```

Level	1	2	3	4	5	6	7	8	9	10
Spike	.0084	.0000	.5000	.6000	1.2000	.8000	1.6000	1.2000	2.4000	1.2000
Spike Increment	.0000	.0000	.5000	1.1000	2.3000	3.1000	4.7000	5.9000	8.3000	9.5000

Final Concentration											
Lab ID	.0084	.0084	.5084	1.1084	2.3084	3.1084	4.7084	5.9084	8.3084	9.5084	
1	.0200	-.0200	.5700	1.0000	2.1800	3.0800	4.7100	5.8500	8.1100	9.7000	
2	.0000	.0000	.7000	1.3000	4.1000	3.9000	6.4000?	7.8000	8.4000	9.6000	
6	-.1000	-.1000	.5000	1.1000	2.5000	3.3000	5.2000	6.7000	8.5000	9.7000	
7	-.0175	-.0646	.5020	.9860	2.3000	3.2400	5.0900	6.4100	7.1000	8.8000	
8	.2000	.1000	.8000	1.6000	3.0000	3.9000	5.3000	6.4000	8.2000	9.4000	
10	r .0000r	-.1000 r	.4500r	1.1000 r	2.2000r	2.6000 r	4.8000r	5.5000 r	7.2000r	7.3000	
11	.0000o	1.0000	.7000	1.7000	2.4000	3.3000	4.6000	5.8000	8.5000	9.9000	
15	.1000	.0000	.6000	1.1000	2.2000	3.0000	4.9000	6.2000	9.0000	10.2000	
16	r -.0010r	-.0010 r	-.0010r	1.1000 r	.0000r	1.1000 r	2.2000r	3.3000 r	4.4000r	5.5000	
17	.1000	.0000	.4000o	26.7000	2.1000	3.5000	o 17.6000	6.5000	9.6000o	18.6000	
20	.0000	.0000	.5000	1.1000	2.4000	3.2000	4.8000	6.1000	8.7000	10.0000	
21	.1000	.1000	.6000	1.1000	2.4000	3.2000	4.8000	6.1000	8.7000	9.5000	
22	-.0800	-.1100	.6200	1.0700	2.8000	3.4000	4.8000	6.0500	8.7000	10.0000	
24	r .2500r	.2400 r	.8100r	1.3400 r	3.2200r	3.6900 r	6.0900r	6.2200 r	9.0800r	10.8000	
25	.1000	.1000	.6000	1.1000	2.4000	3.1000	4.7000	6.5000	8.6000	9.9000	
26	-.2000	-.2000	.6000	1.3000	2.6000	3.4000	4.9000	6.5000	9.0000	11.0000	
27	.1000	.1000	.6000	1.1000	2.0000	2.7000	4.0000o	4.2000	8.3000	9.3000	

cd-5.daf

Cd	5	1	.0200	-.0200	.5700	1.0000	2.1800	3.0800	4.7100	5.8500	8.1100	9.7000
Cd	5	2	.0000	.0000	.7000	1.3000o	4.1000	3.9000	6.4000	7.8000	8.4000	9.6000
Cd	5	6	-.1000	-.1000	.5000	1.1000	2.5000	3.3000	5.2000	6.7000	8.5000	9.7000
Cd	5	7	-.0175	-.0646	.5020	.9860	2.3000	3.2400	5.0900	6.4100o		8.8000
Cd	5	8	.2000	.1000	.8000	1.6000	3.0000	3.9000	5.3000	6.4000	8.2000	9.4000
Cd	5	11	.0000o		.7000	1.7000	2.4000	3.3000	4.6000	5.8000	8.5000	9.9000
Cd	5	15	.1000	.0000	.6000	1.1000	2.2000	3.0000	4.9000	6.2000	9.0000	10.2000
Cd	5	17	.1000	.0000	.4000o		2.1000	3.5000o		6.5000	9.6000o	
Cd	5	20	.0000	.0000	.5000	1.1000	2.4000	3.2000	4.8000	6.1000	8.7000	10.0000
Cd	5	21	.1000	.1000	.6000	1.1000	2.4000	3.2000	4.8000	6.1000	8.7000	9.5000
Cd	5	22	-.0800	-.1100	.6200	1.0700	2.8000	3.4000	4.8000	6.0500	8.7000	10.0000
Cd	5	25	.1000	.1000	.6000	1.1000	2.4000	3.1000	4.7000	6.5000	8.6000	9.9000
Cd	5	26	-.2000	-.2000	.6000	1.3000	2.6000	3.4000	4.9000	6.5000	9.0000	11.0000
Cd	5	27	.1000	.1000	.6000	1.1000	2.0000	2.7000	4.0000o		8.3000	9.3000

## STATCALC Input/Output

File Name: cd-5  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***					
*** Questionable Data (Positive Values) ***					
Conc Lev	Lab No	Rep No	Mean Result	Result	Ratio
2	11	1	.0965	1.0000	10.37
4	17	1	2.6939	26.7000	9.91

Total Number of Questionable Observations: 2

*** Results of Factor of 5 Error Check ***							
*** Questionable Data (All Values) ***							
Conc Lev	Lab No	Rep No	Mean Result	Result	Mean Dev	Obs Dev	Ratio
2	11	1	.0614	1.0000	.150	.939	6.27
4	17	1	2.6939	26.7000	2.824	24.006	8.50
5	16	1	2.4000	.0000	.449	2.400	5.34
6	16	1	3.1535	1.1000	.393	2.054	5.22
7	17	1	5.5818	17.6000	1.570	12.018	7.66
9	16	1	8.2406	4.4000	.729	3.841	5.27
10	17	1	9.9529	18.6000	1.280	8.647	6.75

Total Number of Questionable Observations: 7

File Name: cd-5  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***		
*** Two-Tailed 5% Significance Level ***		
***		
***	Upper Critical Value:	135.0 ***
***	Lower Critical Value:	45.0 ***

Ranks											
Lab	Rank Sums	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Level 8	Level 9	Level 10
1	56.5	10.00	6.00	7.00	2.00	4.00	5.00	5.00	5.00	4.00	8.50
2	124.5	7.50	9.50	14.50	12.50	17.00	16.50	16.00	17.00	7.00	7.00
6	86.0	2.00	3.50	4.50	7.50	12.00	10.50	13.00	16.00	8.50	8.50
7	61.0	4.00	5.00	6.00	1.00	7.00	9.00	12.00	12.00	2.00	3.00
8	127.0	16.00	13.50	16.00	15.00	15.00	16.50	14.00	11.00	5.00	5.00
10	44.5	7.50	3.50	3.00	7.50	5.50	2.00	7.50	3.00	3.00	2.00
11	101.0	7.50	17.00	14.50	16.00	9.50	10.50	3.00	4.00	8.50	10.50
15	97.5	13.00	9.50	10.00	7.50	5.50	4.00	10.50	9.00	14.50	14.00
16	26.5	5.00	7.00	1.00	7.50	1.00	1.00	1.00	1.00	1.00	1.00
17	123.5	13.00	9.50	2.00	17.00	3.00	14.00	17.00	14.00	17.00	17.00
20	85.5	7.50	9.50	4.50	7.50	9.50	7.50	7.50	7.50	12.00	12.50
21	94.0	13.00	13.50	10.00	7.50	9.50	7.50	7.50	7.50	12.00	6.00
22	85.5	3.00	2.00	13.00	3.00	14.00	12.50	7.50	6.00	12.00	12.50
24	151.0	17.00	16.00	17.00	14.00	16.00	15.00	15.00	10.00	16.00	15.00
25	98.0	13.00	13.50	10.00	7.50	9.50	6.00	4.00	14.00	10.00	10.50
26	105.0	1.00	1.00	10.00	12.50	13.00	12.50	10.50	14.00	14.50	16.00
27	63.0	13.00	13.50	10.00	7.50	2.00	3.00	2.00	2.00	6.00	4.00
*** Laboratory 10 Rejected; Rank Sum 44.5 ***											
*** Laboratory 16 Rejected; Rank Sum 26.5 ***											
*** Laboratory 24 Rejected; Rank Sum 151.0 ***											

File Name: cd-5  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Outlier Testing Results ***		
*** Two-Sided 5% Significance Level ***		

- Outlier(s) -										
Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n	
2	1	11	1	1.0000	.0647	.2839	3.294	2.507	14	
4	1	17	1	26.7000	3.0183	6.8194	3.473	2.507	14	
5	1	2	1	4.1000	2.5271	.5249	2.996	2.507	14	
7	1	17	1	17.6000	5.8429	3.4237	3.434	2.507	14	
8	1	27	1	4.2000	6.2221	.7587	2.665	2.507	14	
9	1	7	1	7.1000	8.5293	.5602	2.551	2.507	14	
*	1	17	1	18.6000	10.4000	2.4125	3.399	2.507	14	



File Name: cd-5  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

- Normality Tests -						
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)	
1	14	W	A	.9382	.874	---
2	13	W	A	.9017	.866	---
3	14	W	A	.9449	.874	---
4	13	W	R	.7615	.866	---
5	13	W	A	.9466	.866	---
6	14	W	A	.9341	.874	---
7	13	W	R	.8405	.866	---
8	13	W	R	.8176	.866	---
9	13	W	A	.9230	.866	---
10	13	W	A	.9452	.866	---
- 3 Normality Rejection(s) -						

File Name: cd-5  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

Lev	Mtrx	Points As Received	After Lab Ranking		After Outlier Testing	
			Points	%	Points	%
1	5	17	14	82.4	14	82.4
2	5	17	14	82.4	13	76.5
3	5	17	14	82.4	14	82.4
4	5	17	14	82.4	13	76.5
5	5	17	14	82.4	13	76.5
6	5	17	14	82.4	14	82.4
7	5	17	14	82.4	13	76.5
8	5	17	14	82.4	13	76.5
9	5	17	14	82.4	13	76.5
10	5	17	14	82.4	13	76.5
Totals:		170	140	82.4	133	78.2

## STATCALC Input/Output

File Name: cd-5  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	.0084	.0084	.5084	1.1084	2.3084	3.1084	4.7084	5.9084	8.3084	9.5084
RECOVERY:										
Observations	14	13	14	13	13	14	13	13	13	13
Mean Result	.0230	-.0073	.5923	1.1966	2.4062	3.3014	4.9385	6.3777	8.6392	9.7692
Bias	.0146	-.0157	.0839	.0882	.0978	.1930	.2301	.4693	.3308	.2608
Relative Bias %	174.2347	-186.6300	16.4999	7.9588	4.2347	6.2099	4.8862	7.9428	3.9819	2.7432
Maximum Result	.2000	.1000	.8000	1.7000	3.0000	3.9000	6.4000	7.8000	9.6000	11.0000
Minimum Result	-.2000	-.2000	.4000	.9860	2.0000	2.7000	4.0000	5.8000	8.1100	8.8000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4		Pair 5	
Observations	13		13		13		12		12	
Standard Deviation	.0298		.1143		.1351		.1410		.2092	
Correction Factor	1.0210		1.0210		1.0210		1.0230		1.0230	
Corrected Std Dev	.0304		.1167		.1379		.1443		.2140	
Relative Std Dev (%)	360.6674		13.2104		4.8059		2.5496		2.3254	
OVERALL PRECISION:										
Observations	14	13	14	13	13	14	13	13	13	13
Standard Deviation	.1037	.0940	.1000	.2222	.2766	.3213	.5418	.5065	.3958	.5202
Correction Factor	1.0194	1.0210	1.0194	1.0210	1.0210	1.0194	1.0210	1.0210	1.0210	1.0210
Corrected Std Dev	.1057	.0960	.1020	.2269	.2824	.3275	.5532	.5172	.4042	.5312
Relative Std Dev %	458.7046	*****	17.2160	18.9606	11.7362	9.9206	11.2025	8.1090	4.6783	5.4371

File Name: cd-5  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	.0084	.0230	.0146	174.23	.529	3.012	NO
2	.0084	-.0073	-.0157	*****	.601	3.055	NO
3	.5084	.5923	.0839	16.50	3.138	3.012	YES
4	1.1084	1.1966	.0882	7.96	1.431	3.055	NO
5	2.3084	2.4062	.0978	4.23	1.274	3.055	NO
6	3.1084	3.3014	.1930	6.21	2.248	3.012	NO
7	4.7084	4.9385	.2301	4.89	1.531	3.055	NO
8	5.9084	6.3777	.4693	7.94	3.341	3.055	YES
9	8.3084	8.6392	.3308	3.98	3.013	3.055	NO
10	9.5084	9.7692	.2608	2.74	1.808	3.055	NO

File Name: cd-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .0604  
Slope (b): .0202  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	42.10	.0084	.0304	.0606
2	13	30.00	.8084	.1167	.0768
3	13	15.98	2.7084	.1379	.1152
4	12	7.80	5.3084	.1443	.1677
5	12	4.13	8.9084	.2140	.2405

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

a: .0621 Intercept (a'): -2.7784  
b: 1.1715 Slope (b'): .1582  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	20.70	.0084	.0304	.0622
2	13	20.70	.0084	.1167	.0706
3	13	20.70	.5084	.1379	.0954
4	12	18.95	1.1084	.1443	.1439
5	12	18.95	2.3084	.2140	.2544

File Name: cd-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .1112  
Slope (b): .0600  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	14	23.85	.0084	.1057	.1117
2	13	21.98	.0084	.0960	.1117
3	14	17.99	.5084	.1020	.1417
4	13	12.37	1.1084	.2269	.1777
5	13	7.64	2.3084	.2824	.2497
6	14	6.35	3.1084	.3275	.2977
7	13	3.75	4.7084	.5532	.3938
8	13	2.83	5.9084	.5172	.4658
9	13	1.78	8.3084	.4042	.6099
10	13	1.46	9.5084	.5312	.6819

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

a: .1386 Intercept (a'): -1.9761  
b: 1.1910 Slope (b'): .1748  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	14	10.58	.0084	.1057	.1388
2	13	9.75	.0084	.0960	.1388
3	14	10.58	.5084	.1020	.1515
4	13	9.75	1.1084	.2269	.1682
5	13	9.75	2.3084	.2824	.2075
6	14	10.58	3.1084	.3275	.2387
7	13	9.75	4.7084	.5532	.3157
8	13	9.75	5.9084	.5172	.3893
9	13	9.75	8.3084	.4042	.5923
10	13	9.75	9.5084	.5312	.7305

## STATCALC Input/Output

File Name: cd-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): .0166  
Slope (b): 1.0477

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	14	29.18	.0084	.0230	.0254
2	13	27.10	.0084	-.0073	.0254
3	14	18.13	.5084	.5923	.5493
4	13	10.70	1.1084	1.1966	1.1779
5	13	5.42	2.3084	2.4062	2.4351
6	14	4.10	3.1084	3.3014	3.2733
7	13	2.18	4.7084	4.9385	4.9496
8	13	1.56	5.9084	6.3777	6.2068
9	13	.91	8.3084	8.6392	8.7213
10	13	.73	9.5084	9.7692	9.9786

File Name: cd-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: Cd Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .0446  
Slope (f): .0193

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): .0620  
(f): 1.1630

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .0953  
Slope (f): .0573

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): .1382  
(f): 1.1816

cd8.dat

Cd	8	1	0.4200	0.3900	1.0300	2.1800	5.1900	5.5100	8.7400	11.5800	15.7400	18.1600
Cd	8	2	0.0000	0.0000	0.6000	1.4000	3.8000	5.2000	7.1000	8.8000	8.5000	11.6000
Cd	8	6	0.1000	0.3000	0.9000	2.2000	4.5000	5.9000	7.3000	9.4000	12.3000	11.3000
Cd	8	7	-0.2100	-0.1420	-0.0120	1.1300	2.8000	3.6400	5.3900	7.0700	7.8000	9.2000
Cd	8	8	0.3000	-0.1000	0.4000	1.1000	2.8000	3.5000	4.8000	6.0000	7.7000	8.0000
Cd	8	10	-0.1000	-0.1000	0.4000	1.5500	3.4000	3.7500	6.4000	7.8500	8.2500	11.6500
Cd	8	11	0.1000	0.1000	0.4000	1.1000	3.2000	3.8000	5.3000	7.4000	8.8000	10.2000
Cd	8	15	0.1000	0.1000	0.5000	1.2000	3.2000	4.0000	5.8000	6.2000	7.7000	10.5000
Cd	8	16	-0.0010	-0.0020	-0.0040	-0.0020	-0.0020	0.0000	1.7000	3.9000	5.0000	5.6000
Cd	8	17	2.1000	0.5000	127.0000	4.3000	5.4000	4.4000	5.7000	8.3000	11.1000	12.3000
Cd	8	20	0.0000	0.0000	0.6000	1.5000	3.9000	5.2000	7.4000	9.9000	12.1000	14.0000
Cd	8	21	-0.1000	-0.1500	0.3000	1.1000	3.2000	4.0000	5.8000	7.4000	9.1000	12.0000
Cd	8	22	0.0000	0.0800	0.5100	1.0900	3.2000	4.0000	5.3000	6.9500	8.4000	10.2000
Cd	8	24	0.2600	0.7800	0.6900	1.5100	4.0700	5.2200	7.3900	9.6600	10.0000	16.2000
Cd	8	25	0.1000	0.1000	0.5000	1.2000	3.5000	4.2000	5.1000	8.0000	8.8000	8.8000
Cd	8	26	-0.1000	-0.1000	0.4000	1.4000	3.7000	4.4000	6.0000	8.0000	9.0000	12.0000
Cd	8	27	0.3000	0.1000	0.5000	1.0000	2.7000	3.5000	4.9000	7.1000	8.8000	10.6000

File Name: cd-8

Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte:  Cd      Matrix:  Freshwater
Project:  AMQ-TC   Matrix ID:  8
Date:    12/13/1995 Method:  GFAAS
Pairs:   5
Units:   ug/L

```

Level	1	2	3	4	5	6	7	8	9	10
Spike	.0436	.0000	.4000	.7000	1.9000	.8000	1.6000	1.6000	1.6000	1.7000
Increment	.0000	.0000	.4000	1.1000	3.0000	3.8000	5.4000	7.0000	8.6000	10.3000

		Final Concentration										
Lab ID		.0436	.0436	.4436	1.1436	3.0436	3.8436	5.4436	7.0436	8.6436	10.3436	
1	r	.4200r	.3900 r	1.0300r	2.1800 r	5.1900r	5.5100 r	8.7400r	11.5800 r	15.7400r	18.1600	
2		.0000	.0000	.6000	1.4000	3.8000	5.2000	7.1000	8.8000	8.5000	11.6000	
6	!	.1000!	.3000 !	.9000?	2.2000 !	4.5000!	5.9000 !	7.3000!	9.4000 !	12.3000!	11.3000	
7	!	-.2100!	-.1420 !	-.0120!	1.1300 !	2.8000!	3.6400 !	5.3900!	7.0700 !	7.8000!	9.2000	
8	!	.3000!	-.1000 !	.4000!	1.1000 !	2.8000!	3.5000 !	4.8000!	6.0000 !	7.7000!	8.0000	
10		-.1000	-.1000	.4000	1.5500	3.4000	3.7500	6.4000	7.8500	8.2500	11.6500	
11		.1000	.1000	.4000	1.1000	3.2000	3.8000	5.3000	7.4000	8.8000	10.2000	
15		.1000	.1000	.5000	1.2000	3.2000	4.0000	5.8000	6.2000	7.7000	10.5000	
16	r	-.0010r	-.0020 r	-.0040r	-.0020 r	-.0020r	.0000 r	1.7000r	3.9000 r	5.0000r	5.6000	
17	o	2.1000!	.5000 o	127.0000o	4.3000 o	5.4000!	4.4000 !	5.7000!	8.3000 !	11.1000!	12.3000	
20		.0000	.0000	.6000	1.5000	3.9000	5.2000	7.4000	9.9000	12.1000	14.0000	
21		-.1000	-.1500	.3000	1.1000	3.2000	4.0000	5.8000	7.4000	9.1000	12.0000	
22		.0000	.0800	.5100	1.0900	3.2000	4.0000	5.3000	6.9500	8.4000	10.2000	
24	r	.2600r	.7800 r	.6900r	1.5100 r	4.0700r	5.2200 r	7.3900r	9.6600 r	10.0000r	16.2000	
25		.1000	.1000	.5000	1.2000	3.5000	4.2000	5.1000	8.0000	8.8000	8.8000	
26		-.1000	-.1000	.4000	1.4000	3.7000	4.4000	6.0000	8.0000	9.0000	12.0000	
27		.3000	.1000	.5000	1.0000	2.7000	3.5000	4.9000	7.1000	8.8000	10.6000	

cd-8.daf

Cd	8	2	.0000	.0000	.6000	1.4000	3.8000	5.2000	7.1000	8.8000	8.5000	11.6000
Cd	8	6	.1000	.3000	.9000	2.2000	4.5000	5.9000	7.3000	9.4000	12.3000	11.3000
Cd	8	7	-.2100	-.1420	-.0120	1.1300	2.8000	3.6400	5.3900	7.0700	7.8000	9.2000
Cd	8	8	.3000	-.1000	.4000	1.1000	2.8000	3.5000	4.8000	6.0000	7.7000	8.0000
Cd	8	10	-.1000	-.1000	.4000	1.5500	3.4000	3.7500	6.4000	7.8500	8.2500	11.6500
Cd	8	11	.1000	.1000	.4000	1.1000	3.2000	3.8000	5.3000	7.4000	8.8000	10.2000
Cd	8	15	.1000	.1000	.5000	1.2000	3.2000	4.0000	5.8000	6.2000	7.7000	10.5000
Cd	8	17	o	.5000o	o	o	4.4000	5.7000	8.3000	11.1000	12.3000	
Cd	8	20	.0000	.0000	.6000	1.5000	3.9000	5.2000	7.4000	9.9000	12.1000	14.0000
Cd	8	21	-.1000	-.1500	.3000	1.1000	3.2000	4.0000	5.8000	7.4000	9.1000	12.0000
Cd	8	22	.0000	.0800	.5100	1.0900	3.2000	4.0000	5.3000	6.9500	8.4000	10.2000
Cd	8	25	.1000	.1000	.5000	1.2000	3.5000	4.2000	5.1000	8.0000	8.8000	8.8000
Cd	8	26	-.1000	-.1000	.4000	1.4000	3.7000	4.4000	6.0000	8.0000	9.0000	12.0000
Cd	8	27	.3000	.1000	.5000	1.0000	2.7000	3.5000	4.9000	7.1000	8.8000	10.6000

## STATCALC Input/Output

File Name: cd-8  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc Lev	Lab No	Rep No	Mean Result	Result		Ratio
1	17	1	.2224	2.1000		9.44
2	24	1	.1441	.7800		5.41
3	1	1	7.9253	1.0300		.13
3	2	1	7.9253	.6000		.08
3	6	1	7.9253	.9000		.11
3	8	1	7.9253	.4000		.05
3	10	1	7.9253	.4000		.05
3	11	1	7.9253	.4000		.05
3	15	1	7.9253	.5000		.06
3	17	1	7.9253	127.0000		16.02
3	20	1	7.9253	.6000		.08
3	21	1	7.9253	.3000		.04
3	22	1	7.9253	.5100		.06
3	24	1	7.9253	.6900		.09
3	25	1	7.9253	.5000		.06
3	26	1	7.9253	.4000		.05
3	27	1	7.9253	.5000		.06

Total Number of Questionable Observations: 17

*** Results of Factor of 5 Error Check ***							
*** Questionable Data (All Values) ***							
Conc Lev	Lab No	Rep No	Mean Result	Result	Mean Dev	Obs Dev	Ratio
1	17	1	.1923	2.1000	.285	1.908	6.70
3	17	1	7.9244	127.0000	14.009	119.076	8.50
4	17	1	1.4681	4.3000	.521	2.832	5.43
6	16	1	4.1306	.0000	.822	4.131	5.03

Total Number of Questionable Observations: 4

File Name: cd-8  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***		
*** Two-Tailed 5% Significance Level ***		
***		
***	Upper Critical Value:	135.0
***	Lower Critical Value:	45.0
***		

Ranks											
Lab	Rank Sums	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Level 8	Level 9	Level 10
1	162.0	16.00	15.00	16.00	15.00	16.00	16.00	17.00	17.00	17.00	17.00
2	106.0	7.00	7.50	12.50	10.50	12.00	13.50	13.00	13.00	7.00	10.00
6	140.5	10.50	14.00	15.00	16.00	15.00	17.00	14.00	14.00	16.00	9.00
7	38.5	1.00	2.00	1.00	7.00	3.50	4.00	7.00	5.00	4.00	4.00
8	43.5	14.50	4.00	5.50	5.00	3.50	2.50	2.00	2.00	2.50	2.00
10	77.5	3.00	4.00	5.50	14.00	9.00	5.00	12.00	9.00	5.00	11.00
11	72.5	10.50	11.50	5.50	5.00	6.50	6.00	5.50	7.50	9.00	5.50
15	76.0	10.50	11.50	9.00	8.50	6.50	8.00	9.50	3.00	2.50	7.00
16	20.0	5.00	6.00	2.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
17	143.5	17.00	16.00	17.00	17.00	17.00	11.50	8.00	12.00	14.00	14.00
20	127.5	7.00	7.50	12.50	12.00	13.00	13.50	16.00	16.00	15.00	15.00
21	68.0	3.00	1.00	3.00	5.00	6.50	8.00	9.50	7.50	12.00	12.50
22	65.5	7.00	9.00	11.00	3.00	6.50	8.00	5.50	4.00	6.00	5.50
24	145.0	13.00	17.00	14.00	13.00	14.00	15.00	15.00	15.00	13.00	16.00
25	86.0	10.50	11.50	9.00	8.50	10.00	10.00	4.00	10.50	9.00	3.00
26	90.5	3.00	4.00	5.50	10.50	11.00	11.50	11.00	10.50	11.00	12.50
27	67.5	14.50	11.50	9.00	2.00	2.00	2.50	3.00	6.00	9.00	8.00
*** Laboratory	24 Rejected; Rank Sum	145.0	***								
*** Laboratory	16 Rejected; Rank Sum	20.0	***								
*** Laboratory	1 Rejected; Rank Sum	162.0	***								

File Name: cd-8  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Outlier Testing Results \*\*\*  
\*\*\* Two-Sided 5% Significance Level \*\*\*

-----										
- Outlier(s) -										
Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n	
1	1	17	1	2.1000	.1850	.5701	3.359	2.507	14	
3	1	17	1	127.0000	9.4999	33.8194	3.474	2.507	14	
4	1	17	1	4.3000	1.5193	.8576	3.242	2.507	14	
5	1	17	1	5.4000	3.5214	.7277	2.582	2.507	14	

File Name: cd-8  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

-----										
- Normality Tests -										
Level	n	Test Type	Test Normality Accept/Reject	Test Statistic	Critical Value(s)					
1	13	W	A	.9255	.866	---				
2	14	W	R	.8670	.874	---				
3	13	W	A	.8977	.866	---				
4	13	W	R	.7783	.866	---				
5	13	W	A	.9381	.866	---				
6	14	W	R	.8683	.874	---				
7	14	W	A	.9012	.874	---				
8	14	W	A	.9692	.874	---				
9	14	W	R	.7954	.874	---				
10	14	W	A	.9764	.874	---				

- 4 Normality Rejection(s) -

File Name: cd-8  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

-----						
Points As						
Lev	Mtrrx	Received	After Lab Ranking Points	%	After Outlier Testing Points	%
1	8	17	14	82.4	13	76.5
2	8	17	14	82.4	14	82.4
3	8	17	14	82.4	13	76.5
4	8	17	14	82.4	13	76.5
5	8	17	14	82.4	13	76.5
6	8	17	14	82.4	14	82.4
7	8	17	14	82.4	14	82.4
8	8	17	14	82.4	14	82.4
9	8	17	14	82.4	14	82.4
10	8	17	14	82.4	14	82.4
-----						
Totals:		170	140	82.4	136	80.0

## STATCALC Input/Output

File Name: cd-8  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	.0436	.0436	.4436	1.1436	3.0436	3.8436	5.4436	7.0436	8.6436	10.3436
RECOVERY:										
Observations	13	14	13	13	13	14	14	14	14	14
Mean Result	.0377	.0491	.4614	1.3054	3.3769	4.2493	5.8779	7.7407	9.1679	10.8821
Bias	-.0059	.0055	.0178	.1618	.3333	.4057	.4343	.6971	.5243	.5385
Relative Bias %	-13.5497	12.7130	4.0092	14.1470	10.9516	10.5548	7.9774	9.8971	6.0653	5.2065
Maximum Result	.3000	.5000	.9000	2.2000	4.5000	5.9000	7.4000	9.9000	12.3000	14.0000
Minimum Result	-.2100	-.1500	-.0120	1.0000	2.7000	3.5000	4.8000	6.0000	7.7000	8.0000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4		Pair 5	
Observations	13		13		13		14		14	
Standard Deviation	.1013		.1699		.2232		.4470		.9160	
Correction Factor	1.0210		1.0210		1.0210		1.0194		1.0194	
Corrected Std Dev	.1035		.1735		.2279		.4556		.9338	
Relative Std Dev (%)	237.1734		19.6360		5.9525		6.6913		9.3148	
OVERALL PRECISION:										
Observations	13	14	13	13	13	14	14	14	14	14
Standard Deviation	.1516	.1809	.2047	.3208	.5069	.7185	.8679	1.1135	1.5352	1.5723
Correction Factor	1.0210	1.0194	1.0210	1.0210	1.0210	1.0194	1.0194	1.0194	1.0194	1.0194
Corrected Std Dev	.1547	.1844	.2090	.3276	.5175	.7325	.8848	1.1351	1.5650	1.6028
Relative Std Dev %	410.5423	375.1765	45.3009	25.0936	15.3255	17.2379	15.0528	14.6642	17.0701	14.7288

File Name: cd-8  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	.0436	.0377	-.0059	-13.55	.140	3.055	NO
2	.0436	.0491	.0055	12.71	.115	3.012	NO
3	.4436	.4614	.0178	4.01	.313	3.055	NO
4	1.1436	1.3054	.1618	14.15	1.818	3.055	NO
5	3.0436	3.3769	.3333	10.95	2.371	3.055	NO
6	3.8436	4.2493	.4057	10.55	2.113	3.012	NO
7	5.4436	5.8779	.4343	7.98	1.872	3.012	NO
8	7.0436	7.7407	.6971	9.90	2.342	3.012	NO
9	8.6436	9.1679	.5243	6.07	1.278	3.012	NO
10	10.3436	10.8821	.5385	5.21	1.282	3.012	NO



File Name: cd-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .1025  
Slope (b): .0654  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	80.47	.0436	.1035	.1054
2	13	16.55	.7936	.1735	.1544
3	13	1.93	3.4436	.2279	.3276
4	14	.73	6.2436	.4556	.5106
5	14	.33	9.4936	.9338	.7230

- Curvilinear Model -  $s = a \cdot (b \cdot T)$  (  $\ln s = b' \cdot T + a'$  )

=====

a: .1180 Intercept (a'): -2.1371  
b: 1.2417 Slope (b'): .2165  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	19.34	.0436	.1035	.1191
2	13	19.34	.0436	.1735	.1401
3	13	19.34	.4436	.2279	.2487
4	14	20.99	1.1436	.4556	.4559
5	14	20.99	3.0436	.9338	.9212

File Name: cd-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .1601  
Slope (b): .1410  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	13	33.12	.0436	.1547	.1662
2	14	35.94	.0436	.1844	.1662
3	13	17.18	.4436	.2090	.2226
4	13	7.74	1.1436	.3276	.3214
5	13	2.16	3.0436	.5175	.5893
6	14	1.63	3.8436	.7325	.7021
7	14	.92	5.4436	.8848	.9278
8	14	.59	7.0436	1.1351	1.1534
9	14	.41	8.6436	1.5650	1.3791
10	14	.30	10.3436	1.6028	1.6188

- Curvilinear Model -  $s = a \cdot (b \cdot T)$  (  $\ln s = b' \cdot T + a'$  )

=====

a: .2147 Intercept (a'): -1.5386  
b: 1.2555 Slope (b'): .2276  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	13	9.52	.0436	.1547	.2168
2	14	10.32	.0436	.1844	.2168
3	13	9.52	.4436	.2090	.2375
4	13	9.52	1.1436	.3276	.2785
5	13	9.52	3.0436	.5175	.4291
6	14	10.32	3.8436	.7325	.5148
7	14	10.32	5.4436	.8848	.7409
8	14	10.32	7.0436	1.1351	1.0664
9	14	10.32	8.6436	1.5650	1.5348
10	14	10.32	10.3436	1.6028	2.2597

## STATCALC Input/Output

File Name: cd-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): .0020  
Slope (b): 1.0834

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	13	31.99	.0436	.0377	.0492
2	14	34.45	.0436	.0491	.0492
3	13	17.83	.4436	.4614	.4825
4	13	8.56	1.1436	1.3054	1.2409
5	13	2.55	3.0436	3.3769	3.2993
6	14	1.93	3.8436	4.2493	4.1660
7	14	1.11	5.4436	5.8779	5.8994
8	14	.72	7.0436	7.7407	7.6328
9	14	.50	8.6436	9.1679	9.3662
10	14	.36	10.3436	10.8821	11.2079

File Name: cd-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: Cd Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .1007  
Slope (f): .0603

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): .1179  
(f): 1.2212

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .1583  
Slope (f): .1302

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): .2146  
(f): 1.2337

cd-9.dat

Cd	9	6	2.0000	2.0000	14.0000	24.0000	43.0000	53.0000	69.0000	82.0000	86.0000	94.0000
Cd	9	7	-0.5090	-0.3070	8.7100	13.1000	27.6000	37.8000	43.9000	59.0000	83.4000	92.2000
Cd	9	8	2.3000	2.5000	10.4000	13.3000	31.0000	31.7000	41.5000	52.3000	71.6000	79.9000
Cd	9	10	0.0000	0.0000	2.0000	5.5000	2.4500	12.0000	15.0000	35.0000	32.6000	95.5000
Cd	9	15	0.1000	0.1000	9.0000	15.0000	30.0000	41.0000	51.0000	62.0000	91.0000	104.0000
Cd	9	16	-0.0020	-0.0020	1.0000	0.0000	22.2000	22.2000	44.4000	44.4000	128.0000	88.8000
Cd	9	17	0.1000	0.3000	6.4000	10.6000	33.2000	33.0000	43.0000	59.0000	77.0000	91.0000
Cd	9	20	0.0000	0.0000	11.0000	19.0000	34.0000	45.0000	58.0000	74.0000	107.0000	121.0000
Cd	9	21	-0.3000	0.0000	8.9000	16.9000	33.0000	44.8000	65.7000	65.0000	91.8000	103.8000
Cd	9	22	0.0600	0.0600	9.3000	14.2000	29.0000	36.4000	45.6000	57.2000	81.2000	92.0000
Cd	9	24	0.9000	1.1000	10.7000	19.1000	39.8000	53.5000	69.0000	69.2000	149.0000	105.0000
Cd	9	25	0.0000	0.0000	8.5000	16.4000	28.7000	38.5000	54.5000	65.7000	87.9000	113.0000
Cd	9	26	-0.1000	-1.0000	11.0000	19.0000	36.0000	45.0000	55.0000	70.0000	90.0000	110.0000
Cd	9	27	0.0000	3.0000	4.0000	4.0000	9.0000	14.0000	16.0000	23.0000	34.0000	42.0000

File Name: cd-9

Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte:  Cd      Matrix:  Estuarine
Project:  AMQ-TC   Matrix ID:  9
Date:    12/13/1995  Method:  GFAAS
Pairs:    5
Units:   ug/L

```

Level	1	2	3	4	5	6	7	8	9	10
Spike	.1739	.0000	9.2000	6.0000	14.7000	9.5000	9.6000	12.3000	24.6000	11.0000
Spike Increment	.0000	.0000	9.2000	15.2000	29.9000	39.4000	49.0000	61.3000	85.9000	96.9000

Final Concentration															
Lab ID		.1739	.1739	9.3739	15.3739	30.0739	39.5739	49.1739	61.4739	86.0739	97.0739				
6	r	2.0000r	2.0000	r	14.0000r	24.0000	r	43.0000r	53.0000	r	69.0000r	82.0000	r	86.0000r	94.0000
7	?	-.5090	-.3070		8.7100	13.1000		27.6000	37.8000		43.9000	59.0000		83.4000	92.2000
8	o	2.3000	2.5000		10.4000	13.3000		31.0000	31.7000		41.5000	52.3000		71.6000	79.9000
10	!	.0000!	.0000	!	2.0000!	5.5000	!	2.4500!	12.0000	!	15.0000!	35.0000	!	32.6000!	95.5000
15		.1000	.1000		9.0000	15.0000		30.0000	41.0000		51.0000	62.0000		91.0000	104.0000
16		-.0020	-.0020		1.0000	.0000		22.2000	22.2000		44.4000	44.4000		128.0000	88.8000
17		.1000	.3000		6.4000	10.6000		33.2000	33.0000		43.0000	59.0000		77.0000	91.0000
20		.0000	.0000		11.0000	19.0000		34.0000	45.0000		58.0000	74.0000		107.0000	121.0000
21		-.3000	.0000		8.9000	16.9000		33.0000	44.8000		65.7000	65.0000		91.8000	103.8000
22		.0600	.0600		9.3000	14.2000		29.0000	36.4000		45.6000	57.2000		81.2000	92.0000
24	r	.9000r	1.1000	r	10.7000r	19.1000	r	39.8000r	53.5000	r	69.0000r	69.2000	r	149.0000r	105.0000
25		.0000	.0000		8.5000	16.4000		28.7000	38.5000		54.5000	65.7000		87.9000	113.0000
26		-.1000	-1.0000		11.0000	19.0000		36.0000	45.0000		55.0000	70.0000		90.0000	110.0000
27	!	.0000!	3.0000	!	4.0000!	4.0000	!	9.0000!	14.0000	!	16.0000!	23.0000	!	34.0000o	42.0000

cd-9.daf

Cd	9	7	-.5090	-.3070	8.7100	13.1000	27.6000	37.8000	43.9000	59.0000	83.4000	92.2000
Cd	9	8 o		2.5000	10.4000	13.3000	31.0000	31.7000	41.5000	52.3000	71.6000	79.9000
Cd	9	10	.0000	.0000	2.0000	5.5000	2.4500	12.0000	15.0000	35.0000	32.6000	95.5000
Cd	9	15	.1000	.1000	9.0000	15.0000	30.0000	41.0000	51.0000	62.0000	91.0000	104.0000
Cd	9	16	-.0020	-.0020	1.0000	.0000	22.2000	22.2000	44.4000	44.4000	128.0000	88.8000
Cd	9	17	.1000	.3000	6.4000	10.6000	33.2000	33.0000	43.0000	59.0000	77.0000	91.0000
Cd	9	20	.0000	.0000	11.0000	19.0000	34.0000	45.0000	58.0000	74.0000	107.0000	121.0000
Cd	9	21	-.3000	.0000	8.9000	16.9000	33.0000	44.8000	65.7000	65.0000	91.8000	103.8000
Cd	9	22	.0600	.0600	9.3000	14.2000	29.0000	36.4000	45.6000	57.2000	81.2000	92.0000
Cd	9	25	.0000	.0000	8.5000	16.4000	28.7000	38.5000	54.5000	65.7000	87.9000	113.0000
Cd	9	26	-.1000	-1.0000	11.0000	19.0000	36.0000	45.0000	55.0000	70.0000	90.0000	110.0000
Cd	9	27	.0000	3.0000	4.0000	4.0000	9.0000	14.0000	16.0000	23.0000	34.0000o	

## STATCALC Input/Output

File Name: cd-9  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc	Lab	Rep	Mean	Result		Ratio
Lev	No	No				
1	6	1	.3900	2.0000		5.13
1	8	1	.3900	2.3000		5.90
1	22	1	.3900	.0600		.15
2	15	1	.6471	.1000		.15
2	22	1	.6471	.0600		.09
3	16	1	8.2079	1.0000		.12
5	10	1	28.4964	2.4500		.09

Total Number of Questionable Observations: 7

*** Results of Factor of 5 Error Check ***						
*** Questionable Data (All Values) ***						
Total Number of Questionable Observations: 0						

File Name: cd-9  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***		
*** Two-Tailed 5% Significance Level ***		
***		
***	Upper Critical Value:	112.0 ***
***	Lower Critical Value:	38.0 ***

Ranks											
Lab	Rank Sums	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Level 8	Level 9	Level 10
6	121.5	13.00	12.00	14.00	14.00	14.00	13.00	13.50	14.00	7.00	7.00
7	48.5	1.00	2.00	6.00	5.00	4.00	7.00	5.00	6.50	6.00	6.00
8	67.0	14.00	13.00	10.00	6.00	8.00	4.00	3.00	4.00	3.00	2.00
10	31.0	6.50	5.50	2.00	3.00	1.00	1.00	1.00	2.00	1.00	8.00
15	87.5	10.50	9.00	8.00	8.00	7.00	9.00	8.00	8.00	10.00	10.00
16	40.0	4.00	3.00	1.00	1.00	3.00	3.00	6.00	3.00	13.00	3.00
17	62.0	10.50	10.00	4.00	4.00	10.00	5.00	4.00	6.50	4.00	4.00
20	108.5	6.50	5.50	12.50	11.50	11.00	11.50	11.00	13.00	12.00	14.00
21	84.5	2.00	5.50	7.00	10.00	9.00	10.00	12.00	9.00	11.00	9.00
22	67.0	9.00	8.00	9.00	7.00	6.00	6.00	7.00	5.00	5.00	5.00
24	123.5	12.00	11.00	11.00	13.00	13.00	14.00	13.50	11.00	14.00	11.00
25	79.0	6.50	5.50	5.00	9.00	5.00	8.00	9.00	10.00	8.00	13.00
26	94.5	3.00	1.00	12.50	11.50	12.00	11.50	10.00	12.00	9.00	12.00
27	35.5	6.50	14.00	3.00	2.00	2.00	2.00	2.00	1.00	2.00	1.00
*** Laboratory 6 Rejected; Rank Sum 121.5 ***											
*** Laboratory 24 Rejected; Rank Sum 123.5 ***											

File Name: cd-9  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Outlier Testing Results ***		
*** Two-Sided 5% Significance Level ***		

- Outlier(s) -										
Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n	
1	1	8	1	2.3000	.1374	.7036	3.073	2.412	12	
*	1	27	1	42.0000	94.4333	20.1993	2.596	2.412	12	

File Name: cd-9  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

- Normality Tests -						
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)	
1	11	W	R	.7562	.850	---
2	12	W	R	.7060	.859	---
3	12	W	R	.8531	.859	---
4	12	W	A	.8989	.859	---
5	12	W	R	.7804	.859	---
6	12	W	A	.8648	.859	---
7	12	W	A	.8712	.859	---
8	12	W	A	.9110	.859	---
9	12	W	A	.9030	.859	---
10	11	W	A	.9626	.850	---
- 4 Normality Rejection(s) -						

File Name: cd-9  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

Lev	Mtrx	Points As Received		After Lab Ranking		After Outlier Testing	
				Points	%	Points	%
1	9	14	12	85.7	11	78.6	
2	9	14	12	85.7	12	85.7	
3	9	14	12	85.7	12	85.7	
4	9	14	12	85.7	12	85.7	
5	9	14	12	85.7	12	85.7	
6	9	14	12	85.7	12	85.7	
7	9	14	12	85.7	12	85.7	
8	9	14	12	85.7	12	85.7	
9	9	14	12	85.7	12	85.7	
10	9	14	12	85.7	11	78.6	
Totals:		140	120	85.7	118	84.3	

## STATCALC Input/Output

File Name: cd-9  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	.1739	.1739	9.3739	15.3739	30.0739	39.5739	49.1739	61.4739	86.0739	97.0739
RECOVERY:										
Observations	11	12	12	12	12	12	12	12	12	11
Mean Result	-.0592	.3876	7.5175	12.2500	26.3458	33.4500	44.4667	55.5500	81.2917	99.2000
Bias	-.2331	.2137	-1.8564	-3.1239	-3.7281	-6.1239	-4.7072	-5.9239	-4.7822	2.1261
Relative Bias %	-134.0321	122.8771	-19.8039	-20.3195	-12.3963	-15.4746	-9.5726	-9.6364	-5.5560	2.1902
Maximum Result	.1000	3.0000	11.0000	19.0000	36.0000	45.0000	65.7000	74.0000	128.0000	121.0000
Minimum Result	-.5090	-1.0000	1.0000	.0000	2.4500	12.0000	15.0000	23.0000	32.6000	79.9000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4		Pair 5	
Observations	11		12		12		12		11	
Standard Deviation	.6807		2.1767		3.2205		4.4622		16.5133	
Correction Factor	1.0253		1.0230		1.0230		1.0230		1.0253	
Corrected Std Dev	.6979		2.2266		3.2945		4.5647		16.9306	
Relative Std Dev (%)	401.2945		22.5282		11.0191		9.1278		18.8418	
OVERALL PRECISION:										
Observations	11	12	12	12	12	12	12	12	12	11
Standard Deviation	.1855	1.1539	3.4216	6.1019	10.3630	11.5758	15.3134	14.8518	26.7836	12.2023
Correction Factor	1.0253	1.0230	1.0230	1.0230	1.0230	1.0230	1.0230	1.0230	1.0230	1.0253
Corrected Std Dev	.1902	1.1803	3.5001	6.2420	10.6008	11.8415	15.6650	15.1928	27.3984	12.5107
Relative Std Dev %	-321.3881	304.5391	46.5599	50.9552	40.2373	35.4007	35.2285	27.3497	33.7038	12.6115

File Name: cd-9  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	.1739	-.0592	-.2331	*****	4.166	3.169	YES
2	.1739	.3876	.2137	122.88	.642	3.106	NO
3	9.3739	7.5175	-1.8564	-19.80	1.879	3.106	NO
4	15.3739	12.2500	-3.1239	-20.32	1.773	3.106	NO
5	30.0739	26.3458	-3.7281	-12.40	1.246	3.106	NO
6	39.5739	33.4500	-6.1239	-15.47	1.833	3.106	NO
7	49.1739	44.4667	-4.7072	-9.57	1.065	3.106	NO
8	61.4739	55.5500	-5.9239	-9.64	1.382	3.106	NO
9	86.0739	81.2917	-4.7822	-5.56	.619	3.106	NO
10	97.0739	99.2000	2.1261	2.19	.578	3.169	NO

File Name: cd-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .7771  
Slope (b): .0888  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	11	58.88	.1739	.6979	.7925
2	12	30.82	12.3739	2.2266	1.8759
3	12	7.83	34.8239	3.2945	3.8695
4	12	2.24	55.3239	4.5647	5.6899
5	11	.22	91.5739	16.9306	8.9089

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a: 1.0176 Intercept (a'): .0174  
b: 1.0310 Slope (b'): .0305  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	11	18.84	.1739	.6979	1.0230
2	12	20.77	.1739	2.2266	1.4843
3	12	20.77	9.3739	3.2945	2.9444
4	12	20.77	15.3739	4.5647	5.5034
5	11	18.84	30.0739	16.9306	16.6323

File Name: cd-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .8957  
Slope (b): .2629  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	11	33.25	.1739	.1902	.9415
2	12	36.65	.1739	1.1803	.9415
3	12	12.66	9.3739	3.5001	3.3597
4	12	7.86	15.3739	6.2420	4.9369
5	12	3.41	30.0739	10.6008	8.8009
6	12	2.28	39.5739	11.8415	11.2980
7	12	1.63	49.1739	15.6650	13.8214
8	12	1.14	61.4739	15.1928	17.0546
9	12	.64	86.0739	27.3984	23.5209
10	11	.47	97.0739	12.5107	26.4123

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a: 1.7061 Intercept (a'): .5342  
b: 1.0332 Slope (b'): .0327  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	11	9.24	.1739	.1902	1.7158
2	12	10.19	.1739	1.1803	1.7158
3	12	10.19	9.3739	3.5001	2.3180
4	12	10.19	15.3739	6.2420	2.8204
5	12	10.19	30.0739	10.6008	4.5608
6	12	10.19	39.5739	11.8415	6.2221
7	12	10.19	49.1739	15.6650	8.5163
8	12	10.19	61.4739	15.1928	12.7322
9	12	10.19	86.0739	27.3984	28.4584
10	11	9.24	97.0739	12.5107	40.7760

## STATCALC Input/Output

File Name: cd-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): -.0421  
Slope (b): .8961

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	11	44.49	.1739	-.0592	.1137
2	12	48.53	.1739	.3876	.1137
3	12	3.81	9.3739	7.5175	8.3576
4	12	1.77	15.3739	12.2500	13.7341
5	12	.56	30.0739	26.3458	26.9064
6	12	.34	39.5739	33.4500	35.4191
7	12	.23	49.1739	44.4667	44.0215
8	12	.15	61.4739	55.5500	55.0432
9	12	.08	86.0739	81.2917	77.0867
10	11	.06	97.0739	99.2000	86.9436

File Name: cd-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: Cd Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .8241  
Slope (f): .0991

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 1.0191  
(f): 1.0346

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .9428  
Slope (f): .2933

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 1.7087  
(f): 1.0372



cd-10.dat

Cd	10	1	7.0000	7.0000	31.5000	46.4000	67.3000	75.1000	97.8000	106.4000	145.0000	158.2000
Cd	10	2	5.1000	3.9000	19.8000	29.1000	42.6000	51.6000	69.2000	78.3000	81.0000	88.0000
Cd	10	6	6.0000	7.0000	30.0000	39.0000	60.0000	73.0000	87.0000	94.0000	84.0000	87.0000
Cd	10	7	3.6700	2.9800	-10.6000	-11.3000	-6.7500	-10.9000	-5.2100	-9.4300	0.8220	-6.3600
Cd	10	8	3.1000	2.7000	18.0000	24.1000	32.5000	39.5000	48.4000	55.3000	66.7000	73.9000
Cd	10	10	2.0000	2.0000	24.0000	31.0000	50.5000	58.5000	71.0000	87.0000	92.0000	104.5000
Cd	10	11	3.7000	3.7000	20.7000	28.0000	39.7000	47.7000	63.5000	69.0000	84.0000	90.5000
Cd	10	15	3.0000	3.0000	20.0000	29.0000	40.0000	48.0000	59.0000	61.0000	80.0000	97.0000
Cd	10	16	0.0000	0.0000	22.2000	15.6000	22.2000	37.8000	44.4000	60.0000	33.3000	73.0000
Cd	10	17	4.3000	4.0000	26.0000	26.0000	43.0000	46.0000	64.0000	70.0000	78.0000	122.0000
Cd	10	20	5.0000	4.0000	23.0000	32.0000	46.0000	57.0000	77.0000	86.0000	106.0000	115.0000
Cd	10	21	3.4000	3.7000	21.3000	45.7000	45.2000	61.7000	77.1000	79.8000	87.5000	96.0000
Cd	10	24	3.7000	3.5000	21.1000	29.4000	43.9000	54.2000	75.5000	79.9000	103.0000	112.0000
Cd	10	25	3.6000	2.6000	20.6000	29.5000	41.8000	48.0000	63.6000	77.8000	87.9000	97.0000
Cd	10	26	4.0000	5.0000	26.0000	33.0000	44.0000	49.0000	70.0000	80.0000	90.0000	100.0000
Cd	10	27	0.0000	0.0000	2.0000	0.0000	4.0000	20.0000	5.0000	4.0000	10.0000	6.0000

File Name: cd-10  
Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte:  Cd      Matrix:  Acid Mine Drainage
Project:  AMQ-TC   Matrix ID: 10
Date:    12/13/1995  Method:  GFAAS
Pairs:    5
Units:   ug/L

```

Level	1	2	3	4	5	6	7	8	9	10
Spike	3.5385	.0000	16.0000	8.5000	11.8000	8.1000	14.3000	8.7000	13.8000	8.1000
Spike Increment	.0000	.0000	16.0000	24.5000	36.3000	44.4000	58.7000	67.4000	81.2000	89.3000

Final Concentration															
Lab ID		3.5385	3.5385	19.5385	28.0385	39.8385	47.9385	62.2385	70.9385	84.7385	92.8385				
1	r	7.0000r	7.0000	r	31.5000r	46.4000	r	67.3000r	75.1000	r	97.8000r	106.4000	r	145.0000r	158.2000
2		5.1000	3.9000		19.8000	29.1000		42.6000	51.6000		69.2000	78.3000		81.0000	88.0000
6	!	6.0000!	7.0000	!	30.0000!	39.0000	!	60.0000!	73.0000	!	87.0000!	94.0000	!	84.0000!	87.0000
7	r	3.6700r	2.9800	r	-10.6000r	-11.3000	r	-6.7500r	-10.9000	r	-5.2100r	-9.4300	r	.8220r	-6.3600
8	!	3.1000!	2.7000	!	18.0000!	24.1000	!	32.5000!	39.5000	!	48.4000!	55.3000	!	66.7000!	73.9000
10		2.0000	2.0000		24.0000	31.0000		50.5000	58.5000		71.0000	87.0000		92.0000	104.5000
11		3.7000	3.7000		20.7000	28.0000		39.7000	47.7000		63.5000	69.0000		84.0000	90.5000
15		3.0000	3.0000		20.0000	29.0000		40.0000	48.0000		59.0000	61.0000		80.0000	97.0000
16	!	.0000!	.0000	!	22.2000!	15.6000	!	22.2000!	37.8000	!	44.4000!	60.0000	o	33.3000!	73.0000
17		4.3000	4.0000		26.0000	26.0000		43.0000	46.0000		64.0000	70.0000		78.0000	122.0000
20	!	5.0000!	4.0000	!	23.0000!	32.0000	!	46.0000!	57.0000	!	77.0000!	86.0000	!	106.0000!	115.0000
21		3.4000	3.7000		21.3000	45.7000		45.2000	61.7000		77.1000	79.8000		87.5000	96.0000
24		3.7000	3.5000		21.1000	29.4000		43.9000	54.2000		75.5000	79.9000		103.0000	112.0000
25		3.6000	2.6000		20.6000	29.5000		41.8000	48.0000		63.6000	77.8000		87.9000	97.0000
26		4.0000	5.0000		26.0000	33.0000		44.0000	49.0000		70.0000	80.0000		90.0000	100.0000
27	r	.0000r	.0000	r	2.0000r	.0000	r	4.0000r	20.0000	r	5.0000r	4.0000	r	10.0000r	6.0000

cd-10.daf

Cd	10	2	5.1000	3.9000	19.8000	29.1000	42.6000	51.6000	69.2000	78.3000	81.0000	88.0000
Cd	10	6	6.0000	7.0000	30.0000	39.0000	60.0000	73.0000	87.0000	94.0000	84.0000	87.0000
Cd	10	8	3.1000	2.7000	18.0000	24.1000	32.5000	39.5000	48.4000	55.3000	66.7000	73.9000
Cd	10	10	2.0000	2.0000	24.0000	31.0000	50.5000	58.5000	71.0000	87.0000	92.0000	104.5000
Cd	10	11	3.7000	3.7000	20.7000	28.0000	39.7000	47.7000	63.5000	69.0000	84.0000	90.5000
Cd	10	15	3.0000	3.0000	20.0000	29.0000	40.0000	48.0000	59.0000	61.0000	80.0000	97.0000
Cd	10	16	.0000	.0000	22.2000	15.6000	22.2000	37.8000	44.4000	60.0000o		73.0000
Cd	10	17	4.3000	4.0000	26.0000	26.0000	43.0000	46.0000	64.0000	70.0000	78.0000	122.0000
Cd	10	20	5.0000	4.0000	23.0000	32.0000	46.0000	57.0000	77.0000	86.0000	106.0000	115.0000
Cd	10	21	3.4000	3.7000	21.3000	45.7000	45.2000	61.7000	77.1000	79.8000	87.5000	96.0000
Cd	10	24	3.7000	3.5000	21.1000	29.4000	43.9000	54.2000	75.5000	79.9000	103.0000	112.0000
Cd	10	25	3.6000	2.6000	20.6000	29.5000	41.8000	48.0000	63.6000	77.8000	87.9000	97.0000
Cd	10	26	4.0000	5.0000	26.0000	33.0000	44.0000	49.0000	70.0000	80.0000	90.0000	100.0000

## STATCALC Input/Output

File Name: cd-10  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc	Lab	Rep	Mean	Result		Ratio
Lev	No	No				
3	27	1	20.3875	2.0000		.10
5	27	1	38.9188	4.0000		.10
7	27	1	60.7812	5.0000		.08
8	27	1	68.0313	4.0000		.06
9	7	1	76.8264	.8220		.01
9	27	1	76.8264	10.0000		.13
10	27	1	88.7562	6.0000		.07

Total Number of Questionable Observations: 7

*** Results of Factor of 5 Error Check ***						
*** Questionable Data (All Values) ***						
Total Number of Questionable Observations: 0						

File Name: cd-10  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***		
*** Two-Tailed 5% Significance Level ***		
***		
***	Upper Critical Value:	127.0 ***
***	Lower Critical Value:	42.0 ***

Ranks												
Lab	Rank Sums	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Level 8	Level 9	Level 10	
1	159.5	16.00	15.50	16.00	16.00	16.00	16.00	16.00	16.00	16.00	16.00	16.00
2	86.0	14.00	11.00	4.00	8.00	8.00	10.00	9.00	9.00	7.00	6.00	
6	133.0	15.00	15.50	15.00	14.00	15.00	15.00	15.00	15.00	8.50	5.00	
7	22.0	8.00	6.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
8	40.0	5.00	5.00	3.00	4.00	4.00	4.00	4.00	3.00	4.00	4.00	
10	106.0	3.00	3.00	12.00	11.00	14.00	13.00	11.00	14.00	13.00	12.00	
11	70.5	9.50	9.50	7.00	6.00	5.00	6.00	6.00	6.00	8.50	7.00	
15	62.0	4.00	7.00	5.00	7.00	6.00	7.50	5.00	5.00	6.00	9.50	
16	35.0	1.50	1.50	10.00	3.00	3.00	3.00	3.00	4.00	3.00	3.00	
17	92.0	12.00	12.50	13.50	5.00	9.00	5.00	8.00	7.00	5.00	15.00	
20	128.5	13.00	12.50	11.00	12.00	13.00	12.00	13.00	13.00	15.00	14.00	
21	107.5	6.00	9.50	9.00	15.00	12.00	14.00	14.00	10.00	10.00	8.00	
24	105.5	9.50	8.00	8.00	9.00	10.00	11.00	12.00	11.00	14.00	13.00	
25	77.0	7.00	4.00	6.00	10.00	7.00	7.50	7.00	8.00	11.00	9.50	
26	116.5	11.00	14.00	13.50	13.00	11.00	9.00	10.00	12.00	12.00	11.00	
27	19.0	1.50	1.50	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00	
*** Laboratory 7 Rejected; Rank Sum 22.0 ***												
*** Laboratory 27 Rejected; Rank Sum 19.0 ***												
*** Laboratory 1 Rejected; Rank Sum 159.5 ***												

File Name: cd-10  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Outlier Testing Results ***		
*** Two-Sided 5% Significance Level ***		

- Outlier(s) -											
Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n		
9	1	16	1	33.3000	82.5692	17.9737	2.741	2.462	13		

File Name: cd-10  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

- Normality Tests -						
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)	
1	13	W	A	.9343	.866	---
2	13	W	A	.9341	.866	---
3	13	W	A	.9211	.866	---
4	13	W	A	.9268	.866	---
5	13	W	A	.9108	.866	---
6	13	W	A	.9498	.866	---
7	13	W	A	.9604	.866	---
8	13	W	A	.9501	.866	---
9	12	W	A	.9567	.859	---
10	13	W	A	.9673	.866	---
- 0 Normality Rejection(s) -						

File Name: cd-10  
Data Preparation File (.PRP)

Analyte: Cd Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

Lev	Mtrx	Points As Received	After Lab Ranking		After Outlier Testing	
			Points	%	Points	%
1	10	16	13	81.3	13	81.3
2	10	16	13	81.3	13	81.3
3	10	16	13	81.3	13	81.3
4	10	16	13	81.3	13	81.3
5	10	16	13	81.3	13	81.3
6	10	16	13	81.3	13	81.3
7	10	16	13	81.3	13	81.3
8	10	16	13	81.3	13	81.3
9	10	16	13	81.3	12	75.0
10	10	16	13	81.3	13	81.3
Totals:		160	130	81.3	129	80.6

## STATCALC Input/Output

File Name: cd-10  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: Cd Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	3.5385	3.5385	19.5385	28.0385	39.8385	47.9385	62.2385	70.9385	84.7385	92.8385
RECOVERY:										
Observations	13	13	13	13	13	13	13	13	12	13
Mean Result	3.6077	3.4692	22.5154	30.1077	42.4154	51.6923	66.9000	75.2385	86.6750	96.6077
Bias	.0692	-.0693	2.9769	2.0692	2.5769	3.7538	4.6615	4.3000	1.9365	3.7692
Relative Bias %	1.9554	-1.9576	15.2360	7.3798	6.4683	7.8305	7.4897	6.0615	2.2853	4.0599
Maximum Result	6.0000	7.0000	30.0000	45.7000	60.0000	73.0000	87.0000	94.0000	106.0000	122.0000
Minimum Result	.0000	.0000	18.0000	15.6000	22.2000	37.8000	44.4000	55.3000	66.7000	73.0000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4		Pair 5	
Observations	13		13		13		13		12	
Standard Deviation	.4818		4.8117		2.7939		3.2560		7.5410	
Correction Factor	1.0210		1.0210		1.0210		1.0210		1.0230	
Corrected Std Dev	.4919		4.9128		2.8527		3.3244		7.7141	
Relative Std Dev (%)	13.9019		18.6718		6.0626		4.6777		8.3996	
OVERALL PRECISION:										
Observations	13	13	13	13	13	13	13	13	12	13
Standard Deviation	1.4947	1.6183	3.2580	7.1059	8.7599	9.3963	11.7527	11.4969	10.6467	14.6376
Correction Factor	1.0210	1.0210	1.0210	1.0210	1.0210	1.0210	1.0210	1.0210	1.0230	1.0210
Corrected Std Dev	1.5261	1.6524	3.3265	7.2553	8.9441	9.5939	11.9998	11.7386	10.8911	14.9454
Relative Std Dev %	42.3018	47.6288	14.7745	24.0980	21.0870	18.5596	17.9369	15.6019	12.5654	15.4702

File Name: cd-10  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: Cd Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	3.5385	3.6077	.0692	1.96	.166	3.055	NO
2	3.5385	3.4692	-.0693	-1.96	.154	3.055	NO
3	19.5385	22.5154	2.9769	15.24	3.294	3.055	YES
4	28.0385	30.1077	2.0692	7.38	1.050	3.055	NO
5	39.8385	42.4154	2.5769	6.47	1.061	3.055	NO
6	47.9385	51.6923	3.7538	7.83	1.440	3.055	NO
7	62.2385	66.9000	4.6615	7.49	1.430	3.055	NO
8	70.9385	75.2385	4.3000	6.06	1.349	3.055	NO
9	84.7385	86.6750	1.9365	2.29	.630	3.106	NO
10	92.8385	96.6077	3.7692	4.06	.928	3.055	NO

File Name: cd-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: Cd Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .6454  
Slope (b): .0745  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	65.79	3.5385	.4919	.9092
2	13	18.39	23.7885	4.9128	2.4185
3	13	8.54	43.8885	2.8527	3.9167
4	13	4.62	66.5885	3.3244	5.6087
5	12	2.67	88.7885	7.7141	7.2634

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )  
=====

a: .9581 Intercept (a'): -.0428  
b: 1.0241 Slope (b'): .0238  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	20.35	3.5385	.4919	1.0423
2	13	20.35	3.5385	4.9128	1.6874
3	13	20.35	19.5385	2.8527	2.7222
4	13	20.35	28.0385	3.3244	4.6717
5	12	18.62	39.8385	7.7141	7.9225

File Name: cd-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: Cd Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): 1.0781  
Slope (b): .1615  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	13	36.07	3.5385	1.5261	1.6495
2	13	36.07	3.5385	1.6524	1.6495
3	13	9.74	19.5385	3.3265	4.2336
4	13	6.18	28.0385	7.2553	5.6064
5	13	3.76	39.8385	8.9441	7.5121
6	13	2.84	47.9385	9.5939	8.8202
7	13	1.87	62.2385	11.9998	11.1297
8	13	1.51	70.9385	11.7386	12.5348
9	12	1.02	84.7385	10.8911	14.7635
10	13	.95	92.8385	14.9454	16.0717

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )  
=====

a: 2.2015 Intercept (a'): .7891  
b: 1.0240 Slope (b'): .0237  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	13	10.09	3.5385	1.5261	2.3942
2	13	10.09	3.5385	1.6524	2.3942
3	13	10.09	19.5385	3.3265	3.4986
4	13	10.09	28.0385	7.2553	4.2797
5	13	10.09	39.8385	8.9441	5.6613
6	13	10.09	47.9385	9.5939	6.8598
7	13	10.09	62.2385	11.9998	9.6283
8	13	10.09	70.9385	11.7386	11.8339
9	12	9.23	84.7385	10.8911	16.4141
10	13	10.09	92.8385	14.9454	19.8892

## STATCALC Input/Output

File Name: cd-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: Cd                      Matrix: Acid Mine Drainage  
Project: AMQ-TC                Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): -.1210  
Slope (b): 1.0686

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	13	41.97	3.5385	3.6077	3.6601
2	13	41.97	3.5385	3.4692	3.6601
3	13	6.37	19.5385	22.5154	20.7572
4	13	3.63	28.0385	30.1077	29.8400
5	13	2.02	39.8385	42.4154	42.4490
6	13	1.47	47.9385	51.6923	51.1044
7	13	.92	62.2385	66.9000	66.3849
8	13	.73	70.9385	75.2385	75.6814
9	12	.48	84.7385	86.6750	90.4276
10	13	.44	92.8385	96.6077	99.0830

File Name: cd-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: Cd                      Matrix: Acid Mine Drainage  
Project: AMQ-TC                Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .7586  
Slope (f): .0698

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): .9607  
(f): 1.0225

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): 1.1913  
Slope (f): .1511

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 2.2074  
(f): 1.0224

cr-5.dat

Cr	5	1	0.0000	-0.0200	6.1100	8.5100	15.3000	21.1000	49.9000	56.9000	84.8000	101.8000
Cr	5	2	-0.2000	-0.3000	5.1000	8.4000	15.4000	21.3000	38.3000	42.4000	65.6000	80.6000
Cr	5	5	0.5000	0.2000	5.3000	8.7000	15.2000	21.5000	47.1000	55.2000	85.3000	101.3000
Cr	5	6	-0.7000	-0.9000	4.3000	7.6000	15.4000	22.0000	49.2000	55.0000	85.9000	96.3000
Cr	5	7	-0.4930	-0.6500	6.0800	8.1400	16.1000	23.2000	49.8000	56.1000	81.9000	92.6000
Cr	5	8	2.5000	-1.2000	5.0000	10.1000	13.3000	22.0000	50.2000	46.1000	84.1000	89.9000
Cr	5	10	0.7000	0.8000	6.1000	7.5000	15.7000	22.3000	45.1000	57.1000	82.7000	87.0000
Cr	5	11	-0.1000	-0.1000	5.6000	8.1000	15.8000	21.9000	47.2000	53.7000	84.7000	88.2000
Cr	5	15	0.6000	1.1000	5.9000	8.5000	16.2000	22.0000	49.9000	51.6000	82.7000	80.6000
Cr	5	16	2.2000	7.8000	10.6000	11.1000	22.8000	28.3000	36.7000	67.8000	67.8000	88.3000
Cr	5	17	1.0000	0.0000	6.0000	9.0000	16.0000	23.0000	52.0000	59.0000	89.0000	119.7000
Cr	5	20	1.5000	0.7000	5.1000	7.2000	16.8000	22.7000	45.0000	52.6000	81.2000	90.4000
Cr	5	21	4.8000	0.1000	6.8000	10.0000	17.4000	22.9000	48.7000	54.1000	80.0000	95.7000
Cr	5	24	0.0000	0.9800	5.5000	11.1000	19.8000	29.2000	70.5000	66.3000	62.8000	97.6000
Cr	5	25	0.3000	0.0000	7.1000	8.4000	18.6000	18.4000	41.6000	57.6000	88.0000	92.4000
Cr	5	26	0.2000	0.2000	5.8000	8.1000	15.8000	21.8000	49.2000	56.0000	86.0000	99.0000
Cr	5	27	0.0000	1.0000	6.0000	10.0000	15.0000	16.0000	43.0000	45.0000	88.0000	78.0000

File Name: cr-5  
Data Validation File (.DA~)

\*\*\*\*\*  
\*\*\* Parameter and Data Validation File \*\*\*  
\*\*\*\*\*  
Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC Matrix ID: 5  
Date: 12/13/1995 Method: GFAAS  
Pairs: 5  
Units: ug/L

Level	1	2	3	4	5	6	7	8	9	10
Spike	.3472	.0000	5.2000	2.7000	7.1000	6.1000	24.4000	6.4000	27.4000	11.8000
Increment	.0000	.0000	5.2000	7.9000	15.0000	21.1000	45.5000	51.9000	79.3000	91.1000

Final Concentration										
Lab ID	.3472	.3472	5.5472	8.2472	15.3472	21.4472	45.8472	52.2472	79.6472	91.4472
1	.0000	-.0200	6.1100	8.5100	15.3000	21.1000	49.9000	56.9000	84.8000	101.8000
2	r -.2000r	-.3000	r 5.1000r	8.4000	r 15.4000r	21.3000	r 38.3000r	42.4000	r 65.6000r	80.6000
5	.5000	.2000	5.3000	8.7000	15.2000	21.5000	47.1000	55.2000	85.3000	101.3000
6	-.7000	-.9000	4.3000	7.6000	15.4000	22.0000	49.2000	55.0000	85.9000	96.3000
7	-.4930	-.6500	6.0800	8.1400	16.1000	23.2000	49.8000	56.1000	81.9000	92.6000
8	2.5000	-1.2000	5.0000	10.1000	13.3000	22.0000	50.2000	46.1000	84.1000	89.9000
10	.7000	.8000	6.1000	7.5000	15.7000	22.3000	45.1000	57.1000	82.7000	87.0000
11	-.1000	-.1000	5.6000	8.1000	15.8000	21.9000	47.2000	53.7000	84.7000	88.2000
15	.6000	1.1000	5.9000	8.5000	16.2000	22.0000	49.9000	51.6000	82.7000	80.6000
16	2.2000o	7.8000	o 10.6000	11.1000	o 22.8000	28.3000	36.7000	67.8000	? 67.8000	88.3000
17	1.0000	.0000	6.0000	9.0000	16.0000	23.0000	52.0000	59.0000	89.0000o	119.7000
20	1.5000	.7000	5.1000	7.2000	16.8000	22.7000	45.0000	52.6000	81.2000	90.4000
21	o 4.8000	.1000	6.8000	10.0000	17.4000	22.9000	48.7000	54.1000	80.0000	95.7000
24	.0000	.9800	5.5000	11.1000	19.8000	29.2000	o 70.5000	66.3000	o 62.8000	97.6000
25	.3000	.0000	7.1000	8.4000	18.6000	18.4000	41.6000	57.6000	88.0000	92.4000
26	.2000	.2000	5.8000	8.1000	15.8000	21.8000	49.2000	56.0000	86.0000	99.0000
27	.0000	1.0000	6.0000	10.0000	15.0000	16.0000	43.0000	45.0000	88.0000	78.0000

cr-5.daf

Cr	5	1	.0000	-.0200	6.1100	8.5100	15.3000	21.1000	49.9000	56.9000	84.8000	101.8000
Cr	5	5	.5000	.2000	5.3000	8.7000	15.2000	21.5000	47.1000	55.2000	85.3000	101.3000
Cr	5	6	-.7000	-.9000	4.3000	7.6000	15.4000	22.0000	49.2000	55.0000	85.9000	96.3000
Cr	5	7	-.4930	-.6500	6.0800	8.1400	16.1000	23.2000	49.8000	56.1000	81.9000	92.6000
Cr	5	8	2.5000	-1.2000	5.0000	10.1000	13.3000	22.0000	50.2000	46.1000	84.1000	89.9000
Cr	5	10	.7000	.8000	6.1000	7.5000	15.7000	22.3000	45.1000	57.1000	82.7000	87.0000
Cr	5	11	-.1000	-.1000	5.6000	8.1000	15.8000	21.9000	47.2000	53.7000	84.7000	88.2000
Cr	5	15	.6000	1.1000	5.9000	8.5000	16.2000	22.0000	49.9000	51.6000	82.7000	80.6000
Cr	5	16	2.2000o	7.8000	o 10.6000	11.1000o	22.8000	28.3000	36.7000	67.8000	67.8000	88.3000
Cr	5	17	1.0000	.0000	6.0000	9.0000	16.0000	23.0000	52.0000	59.0000	89.0000o	119.7000
Cr	5	20	1.5000	.7000	5.1000	7.2000	16.8000	22.7000	45.0000	52.6000	81.2000	90.4000
Cr	5	21	o 4.8000	.1000	6.8000	10.0000	17.4000	22.9000	48.7000	54.1000	80.0000	95.7000
Cr	5	24	.0000	.9800	5.5000	11.1000	19.8000	29.2000o	70.5000	66.3000o	62.8000	97.6000
Cr	5	25	.3000	.0000	7.1000	8.4000	18.6000	18.4000	41.6000	57.6000	88.0000	92.4000
Cr	5	26	.2000	.2000	5.8000	8.1000	15.8000	21.8000	49.2000	56.0000	86.0000	99.0000
Cr	5	27	.0000	1.0000	6.0000	10.0000	15.0000	16.0000	43.0000	45.0000	88.0000	78.0000

## STATCALC Input/Output

File Name: cr-5  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc	Lab	Rep	Mean	Result		Ratio
Lev	No	No	Result			
1	21	1	.8412	4.8000		5.71
2	16	1	.7576	7.8000		10.30
2	21	1	.7576	.1000		.13

Total Number of Questionable Observations: 3

*** Results of Factor of 5 Error Check ***							
*** Questionable Data (All Values) ***							
Conc	Lab	Rep	Mean	Result	Mean	Obs	Ratio
Lev	No	No	Result		Dev	Dev	
2	16	1	.5712	7.8000	1.053	7.229	6.86
3	16	1	6.0229	10.6000	.783	4.577	5.85

Total Number of Questionable Observations: 2

File Name: cr-5  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***		
*** Two-Tailed 5% Significance Level ***		
***	Upper Critical Value:	135.0
***	Lower Critical Value:	45.0

Ranks												
Lab	Rank Sums	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Level 8	Level 9	Level 10	
1	95.5	6.00	6.00	14.00	10.00	4.00	3.00	13.50	12.00	11.00	16.00	
2	35.0	3.00	4.00	3.50	7.50	5.50	4.00	2.00	1.00	2.00	2.50	
5	87.5	10.00	10.50	5.00	11.00	3.00	5.00	7.00	9.00	12.00	15.00	
6	65.0	1.00	2.00	1.00	3.00	5.50	9.00	10.50	8.00	13.00	12.00	
7	88.0	2.00	3.00	12.00	6.00	11.00	15.00	12.00	11.00	6.00	10.00	
8	78.0	16.00	1.00	2.00	15.00	1.00	9.00	15.00	3.00	9.00	7.00	
10	88.5	12.00	13.00	13.00	2.00	7.00	11.00	6.00	13.00	7.50	4.00	
11	65.0	4.00	5.00	7.00	4.50	8.50	7.00	8.00	6.00	10.00	5.00	
15	93.5	11.00	16.00	9.00	9.00	12.00	9.00	13.50	4.00	7.50	2.50	
16	125.5	15.00	17.00	17.00	16.50	17.00	16.00	1.00	17.00	3.00	6.00	
17	132.0	13.00	7.50	10.50	12.00	10.00	14.00	16.00	15.00	17.00	17.00	
20	78.5	14.00	12.00	3.50	1.00	13.00	12.00	5.00	5.00	5.00	8.00	
21	112.5	17.00	9.00	15.00	13.50	14.00	13.00	9.00	7.00	4.00	11.00	
24	122.5	6.00	14.00	6.00	16.50	16.00	17.00	17.00	16.00	1.00	13.00	
25	98.5	9.00	7.50	16.00	7.50	15.00	2.00	3.00	14.00	15.50	9.00	
26	94.0	8.00	10.50	8.00	4.50	8.50	6.00	10.50	10.00	14.00	14.00	
27	70.5	6.00	15.00	10.50	13.50	2.00	1.00	4.00	2.00	15.50	1.00	

\*\*\* Laboratory 2 Rejected; Rank Sum 35.0 \*\*\*

File Name: cr-5  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Outlier Testing Results ***		
*** Two-Sided 5% Significance Level ***		

-----  
- Outlier(s) -  
-----

Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n
1	1	21	1	4.8000	.8129	1.3851	2.878	2.585	16
2	1	16	1	7.8000	.6256	2.0273	3.539	2.585	16
3	1	16	1	10.6000	6.0806	1.3804	3.274	2.585	16
5	1	16	1	22.8000	16.5750	2.2323	2.789	2.585	16
7	1	24	1	70.5000	48.4437	7.0724	3.119	2.585	16
9	1	24	1	62.8000	82.1813	7.1088	2.726	2.585	16
*	1	17	1	119.7000	93.6750	9.6749	2.690	2.585	16



File Name: cr-5  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

- Normality Tests -						
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)	
1	15	W	A	.9132	.881	---
2	15	W	A	.9352	.881	---
3	15	W	A	.9653	.881	---
4	16	W	A	.9124	.887	---
5	15	W	A	.9120	.881	---
6	16	W	R	.8478	.887	---
7	15	W	R	.8803	.881	---
8	16	W	A	.9302	.887	---
9	15	W	R	.7824	.881	---
10	15	W	A	.9576	.881	---
- 3 Normality Rejection(s) -						

File Name: cr-5  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

Lev	Mtrx	Points As Received	After Lab Ranking		After Outlier Testing	
			Points	%	Points	%
1	5	17	16	94.1	15	88.2
2	5	17	16	94.1	15	88.2
3	5	17	16	94.1	15	88.2
4	5	17	16	94.1	16	94.1
5	5	17	16	94.1	15	88.2
6	5	17	16	94.1	16	94.1
7	5	17	16	94.1	15	88.2
8	5	17	16	94.1	16	94.1
9	5	17	16	94.1	15	88.2
10	5	17	16	94.1	15	88.2
Totals:		170	160	94.1	153	90.0

## STATCALC Input/Output

File Name: cr-5  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	.3472	.3472	5.5472	8.2472	15.3472	21.4472	45.8472	52.2472	79.6472	91.4472
RECOVERY:										
Observations	15	15	15	16	15	16	15	16	15	15
Mean Result	.5471	.1473	5.7793	8.8781	16.1600	22.3937	46.9733	55.6312	83.4733	91.9400
Bias	.1999	-.1999	.2321	.6309	.8128	.9465	1.1261	3.3840	3.8261	.4928
Relative Bias %	57.5845	-57.5653	4.1847	7.6502	5.2961	4.4134	2.4563	6.4770	4.8039	.5389
Maximum Result	2.5000	1.1000	7.1000	11.1000	19.8000	29.2000	52.0000	67.8000	89.0000	101.8000
Minimum Result	-.7000	-1.2000	4.3000	7.2000	13.3000	16.0000	36.7000	45.0000	67.8000	78.0000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4		Pair 5	
Observations	14		15		15		15		14	
Standard Deviation	.8017		.8625		1.7452		5.5292		5.8007	
Correction Factor	1.0194		1.0180		1.0180		1.0180		1.0194	
Corrected Std Dev	.8172		.8780		1.7766		5.6287		5.9132	
Relative Std Dev (%)	235.3601		11.8988		9.1683		10.9419		6.7421	
OVERALL PRECISION:										
Observations	15	15	15	16	15	16	15	16	15	15
Standard Deviation	.9190	.6942	.6968	1.2259	1.5449	3.0871	4.0653	5.8721	5.0521	6.9774
Correction Factor	1.0180	1.0180	1.0180	1.0168	1.0180	1.0168	1.0180	1.0168	1.0180	1.0180
Corrected Std Dev	.9355	.7067	.7094	1.2465	1.5727	3.1389	4.1385	5.9707	5.1430	7.1030
Relative Std Dev %	170.9820	479.6907	12.2745	14.0398	9.7323	14.0169	8.8103	10.7326	6.1613	7.7257

File Name: cr-5  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	.3472	.5471	.1999	57.58	.841	2.977	NO
2	.3472	.1473	-.1999	-57.57	1.115	2.977	NO
3	5.5472	5.7793	.2321	4.18	1.290	2.977	NO
4	8.2472	8.8781	.6309	7.65	2.059	2.947	NO
5	15.3472	16.1600	.8128	5.30	2.038	2.977	NO
6	21.4472	22.3937	.9465	4.41	1.226	2.947	NO
7	45.8472	46.9733	1.1261	2.46	1.073	2.977	NO
8	52.2472	55.6312	3.3840	6.48	2.305	2.947	NO
9	79.6472	83.4733	3.8261	4.80	2.933	2.977	NO
10	91.4472	91.9400	.4928	.54	.274	2.977	NO

File Name: cr-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .6649  
Slope (b): .0729  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	14	59.43	.3472	.8172	.6902
2	15	26.88	6.8972	.8780	1.1677
3	15	10.26	18.3972	1.7766	2.0061
4	15	2.52	49.0472	5.6287	4.2405
5	14	.91	85.5472	5.9132	6.9014

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a: .9387 Intercept (a'): -.0632  
b: 1.0259 Slope (b'): .0256  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	14	19.10	.3472	.8172	.9471
2	15	20.60	.3472	.8780	1.1199
3	15	20.60	5.5472	1.7766	1.5031
4	15	20.60	8.2472	5.6287	3.2928
5	14	19.10	15.3472	5.9132	8.3784

File Name: cr-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .7091  
Slope (b): .0755  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	15	28.82	.3472	.9355	.7353
2	15	28.82	.3472	.7067	.7353
3	15	15.01	5.5472	.7094	1.1279
4	16	12.29	8.2472	1.2465	1.3317
5	15	6.46	15.3472	1.5727	1.8678
6	16	4.70	21.4472	3.1389	2.3283
7	15	1.51	45.8472	4.1385	4.1705
8	16	1.31	52.2472	5.9707	4.6537
9	15	.61	79.6472	5.1430	6.7224
10	15	.48	91.4472	7.1030	7.6133

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a: 1.0060 Intercept (a'): .0060  
b: 1.0249 Slope (b'): .0246  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	15	9.79	.3472	.9355	1.0146
2	15	9.79	.3472	.7067	1.0146
3	15	9.79	5.5472	.7094	1.1531
4	16	10.50	8.2472	1.2465	1.2324
5	15	9.79	15.3472	1.5727	1.4676
6	16	10.50	21.4472	3.1389	1.7054
7	15	9.79	45.8472	4.1385	3.1088
8	16	10.50	52.2472	5.9707	3.6391
9	15	9.79	79.6472	5.1430	7.1422
10	15	9.79	91.4472	7.1030	9.5487

## STATCALC Input/Output

File Name: cr-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): .0386  
Slope (b): 1.0391

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	15	32.36	.3472	.5471	.3993
2	15	32.36	.3472	.1473	.3993
3	15	13.75	5.5472	5.7793	5.8026
4	16	10.52	8.2472	8.8781	8.6081
5	15	5.01	15.3472	16.1600	15.9855
6	16	3.44	21.4472	22.3937	22.3239
7	15	1.01	45.8472	46.9733	47.6775
8	16	.86	52.2472	55.6312	54.3276
9	15	.39	79.6472	83.4733	82.7984
10	15	.30	91.4472	91.9400	95.0595

File Name: cr-5  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: Cr Matrix: Reagent Grade Water  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .6278  
Slope (f): .0702

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): .9378  
(f): 1.0249

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .6719  
Slope (f): .0727

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 1.0051  
(f): 1.0240

cr-8.dat

Cr	8	1	0.0900	0.1300	8.4800	6.0500	14.8000	21.6000	42.5000	45.9000	83.5000	92.2000
Cr	8	2	-0.1000	-0.5000	4.4000	7.5000	17.6000	21.5000	45.1000	48.0000	97.0000	106.0000
Cr	8	5	0.6000	0.5000	4.7000	7.4000	19.5000	22.7000	50.3000	58.9000	80.9000	93.3000
Cr	8	6	-0.1000	1.6000	3.3000	6.4000	15.4000	19.1000	44.3000	49.6000	75.9000	90.7000
Cr	8	7	0.1410	-0.4470	4.4700	8.7400	20.4000	26.8000	55.4000	64.8000	86.2000	110.0000
Cr	8	8	0.0000	1.4000	5.4000	9.4000	23.4000	23.1000	57.6000	56.9000	103.0000	109.0000
Cr	8	10	0.8000	1.0000	3.9000	6.1000	15.9000	21.3000	53.1000	59.1000	78.5000	84.9000
Cr	8	11	0.2000	-0.1000	4.9000	8.3000	20.0000	25.1000	54.7000	64.3000	86.1000	104.0000
Cr	8	15	1.1000	0.9000	4.4000	7.5000	18.1000	23.3000	48.2000	54.1000	92.3000	98.9000
Cr	8	16	7.2000	6.1000	11.1000	16.7000	32.8000	38.9000	75.6000	90.0000	125.6000	143.9000
Cr	8	17	6.0000	5.0000	5.0000	9.0000	28.0000	28.0000	75.0000	70.0000	100.0000	30.0000
Cr	8	20	1.0000	0.6000	266.0000	10.1000	20.5000	25.7000	54.1000	67.6000	90.7000	96.4000
Cr	8	21	4.1000	2.1000	7.1000	8.6000	18.7000	25.6000	50.6000	59.7000	82.2000	97.4000
Cr	8	24	0.2700	0.0000	4.0100	11.7000	29.1000	31.3000	54.5000	83.8000	87.2000	87.6000
Cr	8	25	0.4000	0.0000	5.0000	8.9000	21.8000	16.8000	49.6000	51.7000	77.7000	101.2000
Cr	8	26	0.0000	-0.1000	5.0000	7.7000	19.3000	23.8000	53.0000	73.5000	92.0000	103.0000
Cr	8	27	-1.0000	0.0000	6.0000	9.0000	20.0000	24.0000	48.0000	64.0000	86.0000	99.0000

File Name: cr-8

Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte:  Cr           Matrix:  Freshwater
Project:  AMQ-TC       Matrix ID: 8
Date:     12/13/1995   Method:  GFAAS
Pairs:    5
Units:    ug/L

```

Level	1	2	3	4	5	6	7	8	9	10
Spike	.4673	.0000	4.8000	3.0000	11.7000	5.0000	30.0000	8.0000	24.7000	12.5000
Increment	.0000	.0000	4.8000	7.8000	19.5000	24.5000	54.5000	62.5000	87.2000	99.7000

Final Concentration											
Lab ID	.4673	.4673	5.2673	8.2673	19.9673	24.9673	54.9673	62.9673	87.6673	100.1673	
1	.0900	.1300	?	8.4800	6.0500	14.8000	21.6000	42.5000	45.9000	83.5000	92.2000
2	-.1000	-.5000		4.4000	7.5000	17.6000	21.5000	45.1000	48.0000	97.0000	106.0000
5	.6000	.5000		4.7000	7.4000	19.5000	22.7000	50.3000	58.9000	80.9000	93.3000
6	r -.1000r	1.6000	r	3.3000r	6.4000	r	15.4000r	19.1000	r	44.3000r	49.6000
7	.1410	-.4470		4.4700	8.7400		20.4000	26.8000		55.4000	64.8000
8	.0000	1.4000		5.4000	9.4000		23.4000	23.1000		57.6000	56.9000
10	.8000	1.0000		3.9000	6.1000		15.9000	21.3000		53.1000	59.1000
11	.2000	-.1000		4.9000	8.3000		20.0000	25.1000		54.7000	64.3000
15	1.1000	.9000		4.4000	7.5000		18.1000	23.3000		48.2000	54.1000
16	r 7.2000r	6.1000	r	11.1000r	16.7000	r	32.8000r	38.9000	r	75.6000r	90.0000
17	o 6.0000o	5.0000		5.0000	9.0000		28.0000	28.0000	o	75.0000	70.0000
20	1.0000	.6000	o	266.0000	10.1000		20.5000	25.7000		54.1000	67.6000
21	? 4.1000	2.1000		7.1000	8.6000		18.7000	25.6000		50.6000	59.7000
24	.2700	.0000		4.0100	11.7000		29.1000	31.3000		54.5000	83.8000
25	.4000	.0000		5.0000	8.9000		21.8000	16.8000		49.6000	51.7000
26	.0000	-.1000		5.0000	7.7000		19.3000	23.8000		53.0000	73.5000
27	-1.0000	.0000		6.0000	9.0000		20.0000	24.0000		48.0000	64.0000

cr-8.daf

Cr	8	1	.0900	.1300	8.4800	6.0500	14.8000	21.6000	42.5000	45.9000	83.5000	92.2000
Cr	8	2	-.1000	-.5000	4.4000	7.5000	17.6000	21.5000	45.1000	48.0000	97.0000	106.0000
Cr	8	5	.6000	.5000	4.7000	7.4000	19.5000	22.7000	50.3000	58.9000	80.9000	93.3000
Cr	8	7	.1410	-.4470	4.4700	8.7400	20.4000	26.8000	55.4000	64.8000	86.2000	110.0000
Cr	8	8	.0000	1.4000	5.4000	9.4000	23.4000	23.1000	57.6000	56.9000	103.0000	109.0000
Cr	8	10	.8000	1.0000	3.9000	6.1000	15.9000	21.3000	53.1000	59.1000	78.5000	84.9000
Cr	8	11	.2000	-.1000	4.9000	8.3000	20.0000	25.1000	54.7000	64.3000	86.1000	104.0000
Cr	8	15	1.1000	.9000	4.4000	7.5000	18.1000	23.3000	48.2000	54.1000	92.3000	98.9000
Cr	8	17	o	o	5.0000	9.0000	28.0000	28.0000o		70.0000	100.0000o	
Cr	8	20	1.0000	.6000o		10.1000	20.5000	25.7000	54.1000	67.6000	90.7000	96.4000
Cr	8	21	4.1000	2.1000	7.1000	8.6000	18.7000	25.6000	50.6000	59.7000	82.2000	97.4000
Cr	8	24	.2700	.0000	4.0100	11.7000	29.1000	31.3000	54.5000	83.8000	87.2000	87.6000
Cr	8	25	.4000	.0000	5.0000	8.9000	21.8000	16.8000	49.6000	51.7000	77.7000	101.2000
Cr	8	26	.0000	-.1000	5.0000	7.7000	19.3000	23.8000	53.0000	73.5000	92.0000	103.0000
Cr	8	27	-1.0000	.0000	6.0000	9.0000	20.0000	24.0000	48.0000	64.0000	86.0000	99.0000

## STATCALC Input/Output

File Name: cr-8  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc	Lab	Rep	Mean			
Lev	No	No	Result	Result		Ratio
1	1	1	1.2883	.0900		.07
1	7	1	1.2883	.1410		.11
1	11	1	1.2883	.2000		.16
1	16	1	1.2883	7.2000		5.59
2	1	1	1.1371	.1300		.11
2	16	1	1.1371	6.1000		5.36
3	6	1	20.7741	3.3000		.16
3	10	1	20.7741	3.9000		.19
3	20	1	20.7741	266.0000		12.80
3	24	1	20.7741	4.0100		.19

Total Number of Questionable Observations: 10

*** Results of Factor of 5 Error Check ***							
*** Questionable Data (All Values) ***							
Conc	Lab	Rep	Mean		Mean	Obs	
Lev	No	No	Result	Result	Dev	Dev	Ratio
3	20	1	20.7741	266.0000	28.850	245.226	8.50
4	16	1	8.7700	16.7000	1.578	7.930	5.03
10	17	1	96.9118	30.0000	12.151	66.912	5.51

Total Number of Questionable Observations: 3

File Name: cr-8  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***		
*** Two-Tailed 5% Significance Level ***		
***	Upper Critical Value:	135.0
***	Lower Critical Value:	45.0

Ranks											
Lab	Rank Sums	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Level 8	Level 9	Level 10
1	49.0	6.00	8.00	15.00	1.00	1.00	5.00	1.00	1.00	6.00	5.00
2	54.5	2.50	1.00	4.50	5.50	4.00	4.00	3.00	2.00	14.00	14.00
5	69.0	11.00	9.00	7.00	4.00	8.00	6.00	7.00	7.00	4.00	6.00
6	34.5	2.50	14.00	1.00	3.00	2.00	2.00	2.00	3.00	1.00	4.00
7	101.0	7.00	2.00	6.00	10.00	11.00	14.00	14.00	12.00	9.00	16.00
8	116.5	4.50	13.00	12.00	14.00	14.00	7.00	15.00	6.00	16.00	15.00
10	57.0	12.00	12.00	2.00	2.00	3.00	3.00	10.00	8.00	3.00	2.00
11	93.0	8.00	3.50	8.00	8.00	9.50	11.00	13.00	11.00	8.00	13.00
15	80.0	14.00	11.00	4.50	5.50	5.00	8.00	5.00	5.00	13.00	9.00
16	169.0	17.00	17.00	16.00	17.00	17.00	17.00	17.00	17.00	17.00	17.00
17	130.5	16.00	16.00	10.00	12.50	15.00	15.00	16.00	14.00	15.00	1.00
20	122.0	13.00	10.00	17.00	15.00	12.00	13.00	11.00	13.00	11.00	7.00
21	101.0	15.00	15.00	14.00	9.00	6.00	12.00	8.00	9.00	5.00	8.00
24	107.0	9.00	6.00	3.00	16.00	16.00	16.00	12.00	16.00	10.00	3.00
25	74.0	10.00	6.00	10.00	11.00	13.00	1.00	6.00	4.00	2.00	11.00
26	89.0	4.50	3.50	10.00	7.00	7.00	9.00	9.00	15.00	12.00	12.00
27	83.0	1.00	6.00	13.00	12.50	9.50	10.00	4.00	10.00	7.00	10.00
*** Laboratory 6 Rejected; Rank Sum 34.5 ***											
*** Laboratory 16 Rejected; Rank Sum 169.0 ***											

File Name: cr-8  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Outlier Testing Results \*\*\*  
\*\*\* Two-Sided 5% Significance Level \*\*\*

-----										
- Outlier(s) -										
Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n	
1	1	17	1	6.0000	.9067	1.7928	2.841	2.549	15	
2	1	17	1	5.0000	.6989	1.3875	3.100	2.549	15	
3	1	20	1	266.0000	22.5840	67.3498	3.614	2.549	15	
7	1	17	1	75.0000	52.7800	7.3769	3.012	2.549	15	
*	1	17	1	30.0000	94.1933	19.1742	3.348	2.549	15	

File Name: cr-8  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

-----										
- Normality Tests -										
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)					
1	14	W	R	.7326	.874	---				
2	14	W	A	.9069	.874	---				
3	14	W	R	.8205	.874	---				
4	15	W	A	.9558	.881	---				
5	15	W	A	.8975	.881	---				
6	15	W	A	.9694	.881	---				
7	14	W	A	.9597	.874	---				
8	15	W	A	.9753	.881	---				
9	15	W	A	.9527	.881	---				
10	14	W	A	.9740	.874	---				

-----  
- 2 Normality Rejection(s) -  
-----

File Name: cr-8  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

-----										
Lev	Mtrx	Points As Received	After Lab Ranking		After Outlier Testing					
			Points	%	Points	%				
1	8	17	15	88.2	14	82.4				
2	8	17	15	88.2	14	82.4				
3	8	17	15	88.2	14	82.4				
4	8	17	15	88.2	15	88.2				
5	8	17	15	88.2	15	88.2				
6	8	17	15	88.2	15	88.2				
7	8	17	15	88.2	14	82.4				
8	8	17	15	88.2	15	88.2				
9	8	17	15	88.2	15	88.2				
10	8	17	15	88.2	14	82.4				
Totals:		170	150	88.2	145	85.3				

## STATCALC Input/Output

File Name: cr-8  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	.4673	.4673	5.2673	8.2673	19.9673	24.9673	54.9673	62.9673	87.6673	100.1673
RECOVERY:										
Observations	14	14	14	15	15	15	14	15	15	14
Mean Result	.5429	.3916	5.1971	8.3993	20.4733	24.0400	51.1929	61.4867	88.2200	98.7786
Bias	.0756	-.0757	-.0702	.1320	.5060	-.9273	-3.7744	-1.4806	.5527	-1.3887
Relative Bias %	16.1842	-16.1903	-1.3319	1.5971	2.5343	-3.7141	-6.8667	-2.3514	.6304	-1.3864
Maximum Result	4.1000	2.1000	8.4800	11.7000	29.1000	31.3000	57.6000	83.8000	103.0000	110.0000
Minimum Result	-1.0000	-.5000	3.9000	6.0500	14.8000	16.8000	42.5000	45.9000	77.7000	84.9000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4		Pair 5	
Observations	14		14		15		14		14	
Standard Deviation	.5453		1.5072		2.2747		5.6724		4.8211	
Correction Factor	1.0194		1.0194		1.0180		1.0194		1.0194	
Corrected Std Dev	.5558		1.5364		2.3156		5.7824		4.9146	
Relative Std Dev (%)	118.9486		22.4184		10.4041		10.2313		5.2666	
OVERALL PRECISION:										
Observations	14	14	14	15	15	15	14	15	15	14
Standard Deviation	1.1504	.7405	1.2535	1.4599	3.9125	3.3588	4.2324	9.9609	7.5743	7.5038
Correction Factor	1.0194	1.0194	1.0194	1.0180	1.0180	1.0180	1.0194	1.0180	1.0180	1.0194
Corrected Std Dev	1.1727	.7549	1.2778	1.4862	3.9830	3.4192	4.3145	10.1402	7.7107	7.6493
Relative Std Dev %	215.9957	192.7552	24.5874	17.6940	19.4543	14.2230	8.4278	16.4917	8.7403	7.7439

File Name: cr-8  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	.4673	.5429	.0756	16.18	.245	3.012	NO
2	.4673	.3916	-.0757	-16.19	.382	3.012	NO
3	5.2673	5.1971	-.0702	-1.33	.209	3.012	NO
4	8.2673	8.3993	.1320	1.60	.350	2.977	NO
5	19.9673	20.4733	.5060	2.53	.501	2.977	NO
6	24.9673	24.0400	-.9273	-3.71	1.069	2.977	NO
7	54.9673	51.1929	-3.7744	-6.87	3.337	3.012	YES
8	62.9673	61.4867	-1.4806	-2.35	.576	2.977	NO
9	87.6673	88.2200	.5527	.63	.283	2.977	NO
10	100.1673	98.7786	-1.3887	-1.39	.692	3.012	NO



File Name: cr-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .7690  
Slope (b): .0651  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	14	49.22	.4673	.5558	.7995
2	14	30.60	6.7673	1.5364	1.2098
3	15	14.15	22.4673	2.3156	2.2325
4	14	4.04	58.9673	5.7824	4.6100
5	14	1.99	93.9173	4.9146	6.8865

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a: 1.0620 Intercept (a'): .0602  
b: 1.0208 Slope (b'): .0206  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	14	19.69	.4673	.5558	1.0723
2	14	19.69	.4673	1.5364	1.2205
3	15	21.23	5.2673	2.3156	1.6853
4	14	19.69	8.2673	5.7824	3.5686
5	14	19.69	19.9673	4.9146	7.3193

File Name: cr-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): .9477  
Slope (b): .0934  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	14	26.66	.4673	1.1727	.9914
2	14	26.66	.4673	.7549	.9914
3	14	16.57	5.2673	1.2778	1.4398
4	15	13.93	8.2673	1.4862	1.7200
5	15	6.57	19.9673	3.9830	2.8130
6	15	5.11	24.9673	3.4192	3.2801
7	14	1.63	54.9673	4.3145	6.0825
8	15	1.42	62.9673	10.1402	6.8299
9	15	.83	87.6673	7.7107	9.1372
10	14	.62	100.1673	7.6493	10.3049

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

=====

a: 1.3754 Intercept (a'): .3187  
b: 1.0219 Slope (b'): .0217  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	14	9.62	.4673	1.1727	1.3893
2	14	9.62	.4673	.7549	1.3893
3	14	9.62	5.2673	1.2778	1.5415
4	15	10.38	8.2673	1.4862	1.6449
5	15	10.38	19.9673	3.9830	2.1191
6	15	10.38	24.9673	3.4192	2.3614
7	14	9.62	54.9673	4.3145	4.5211
8	15	10.38	62.9673	10.1402	5.3761
9	15	10.38	87.6673	7.7107	9.1771
10	14	9.62	100.1673	7.6493	12.0292

## STATCALC Input/Output

File Name: cr-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): .0534  
Slope (b): .9807

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	14	31.93	.4673	.5429	.5116
2	14	31.93	.4673	.3916	.5116
3	14	15.14	5.2673	5.1971	5.2190
4	15	11.36	8.2673	8.3993	8.1611
5	15	4.25	19.9673	20.4733	19.6352
6	15	3.13	24.9673	24.0400	24.5387
7	14	.85	54.9673	51.1929	53.9596
8	15	.72	62.9673	61.4867	61.8051
9	15	.40	87.6673	88.2200	86.0283
10	14	.30	100.1673	98.7786	98.2870

File Name: cr-8  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: Cr Matrix: Freshwater  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .7146  
Slope (f): .0664

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 1.0609  
(f): 1.0212

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): .8933  
Slope (f): .0953

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 1.3737  
(f): 1.0223

cr-9.dat

Cr	9	5	2.0000	0.0000	55.0000	74.0000	283.0000	372.0000	618.0000	697.0000	820.0000	932.0000
Cr	9	6	-7.0000	-10.0000	48.0000	70.0000	282.0000	337.0000	648.0000	732.0000	816.0000	944.0000
Cr	9	7	1.5500	1.7300	45.5000	60.0000	323.0000	407.0000	645.0000	720.0000	797.0000	895.0000
Cr	9	8	2.8000	0.9000	55.3000	75.5000	269.0000	286.0000	534.0000	601.0000	726.0000	818.0000
Cr	9	10	29.5000	4.0000	58.5000	90.5000	372.5000	430.5000	729.5000	764.5000	980.0000	1050.0000
Cr	9	15	1.1000	1.0000	47.0000	67.0000	261.0000	333.0000	532.0000	642.0000	728.0000	878.0000
Cr	9	16	8.0000	84.0000	60.0000	100.0000	378.0000	269.0000	471.0000	582.0000	644.0000	700.0000
Cr	9	17	6.0000	3.0000	66.0000	94.0000	376.0000	420.0000	690.0000	780.0000	910.0000	1249.0000
Cr	9	20	27.0000	23.0000	80.0000	90.0000	329.0000	390.0000	682.0000	735.0000	873.0000	972.0000
Cr	9	21	1.0000	0.5000	61.0000	76.0000	293.0000	378.0000	596.0000	698.0000	823.0000	905.0000
Cr	9	24	7.0000	0.0000	74.2000	67.1000	397.0000	487.0000	717.0000	548.0000	734.0000	801.0000
Cr	9	25	2.4000	0.0000	62.7000	81.4000	321.0000	409.0000	667.0000	768.0000	848.0000	949.0000
Cr	9	26	3.0000	0.0000	60.0000	73.0000	284.0000	335.0000	625.0000	670.0000	800.0000	950.0000
Cr	9	27	10.0000	10.0000	70.0000	80.0000	280.0000	390.0000	550.0000	600.0000	790.0000	810.0000

File Name: cr-9

Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte:  Cr      Matrix:  Estuarine
Project:  AMQ-TC   Matrix ID:  9
Date:    12/13/1995  Method:  GFAAS
Pairs:    5
Units:   ug/L

```

Level	1	2	3	4	5	6	7	8	9	10
Spike	2.6809	.0000	56.1000	19.7000	219.0000	81.0000	269.0000	71.0000	127.0000	110.0000
Spike Increment	.0000	.0000	56.1000	75.8000	294.8000	375.8000	644.8000	715.8000	842.8000	952.8000

Final Concentration											
Lab ID	2.6809	2.6809	58.7809	78.4809	297.4809	378.4809	647.4809	718.4809	845.4809	955.4809	
5	2.0000	.0000	55.0000	74.0000	283.0000	372.0000	618.0000	697.0000	820.0000	932.0000	
6	-7.0000	-10.0000	48.0000	70.0000	282.0000	337.0000	648.0000	732.0000	816.0000	944.0000	
7	1.5500	1.7300	45.5000	60.0000	323.0000	407.0000	645.0000	720.0000	797.0000	895.0000	
8	2.8000	.9000	55.3000	75.5000	269.0000	286.0000	534.0000	601.0000	726.0000	818.0000	
10	r 29.5000r	4.0000 r	58.5000r	90.5000 r	372.5000r	430.5000 r	729.5000r	764.5000 r	980.0000r	1050.0000	
15	! 1.1000!	1.0000 !	47.0000!	67.0000 !	261.0000!	333.0000 !	532.0000!	642.0000 !	728.0000!	878.0000	
16	8.0000o	84.0000	60.0000	100.0000	378.0000	269.0000	471.0000	582.0000	644.0000	700.0000	
17	r 6.0000r	3.0000 r	66.0000r	94.0000 r	376.0000r	420.0000 r	690.0000r	780.0000 r	910.0000r	1249.0000	
20	o 27.0000?	23.0000 !	80.0000!	90.0000 !	329.0000!	390.0000 !	682.0000!	735.0000 !	873.0000!	972.0000	
21	1.0000	.5000	61.0000	76.0000	293.0000	378.0000	596.0000	698.0000	823.0000	905.0000	
24	7.0000	.0000	74.2000	67.1000	397.0000	487.0000	717.0000	548.0000	734.0000	801.0000	
25	2.4000	.0000	62.7000	81.4000	321.0000	409.0000	667.0000	768.0000	848.0000	949.0000	
26	3.0000	.0000	60.0000	73.0000	284.0000	335.0000	625.0000	670.0000	800.0000	950.0000	
27	10.0000	10.0000	70.0000	80.0000	280.0000	390.0000	550.0000	600.0000	790.0000	810.0000	

cr-9.daf

Cr	9	5	2.0000	.0000	55.0000	74.0000	283.0000	372.0000	618.0000	697.0000	820.0000	932.0000
Cr	9	6	-7.0000	-10.0000	48.0000	70.0000	282.0000	337.0000	648.0000	732.0000	816.0000	944.0000
Cr	9	7	1.5500	1.7300	45.5000	60.0000	323.0000	407.0000	645.0000	720.0000	797.0000	895.0000
Cr	9	8	2.8000	.9000	55.3000	75.5000	269.0000	286.0000	534.0000	601.0000	726.0000	818.0000
Cr	9	15	1.1000	1.0000	47.0000	67.0000	261.0000	333.0000	532.0000	642.0000	728.0000	878.0000
Cr	9	16	8.0000o		60.0000	100.0000	378.0000	269.0000	471.0000	582.0000	644.0000	700.0000
Cr	9	20	o 27.0000?	23.0000	80.0000	90.0000	329.0000	390.0000	682.0000	735.0000	873.0000	972.0000
Cr	9	21	1.0000	.5000	61.0000	76.0000	293.0000	378.0000	596.0000	698.0000	823.0000	905.0000
Cr	9	24	7.0000	.0000	74.2000	67.1000	397.0000	487.0000	717.0000	548.0000	734.0000	801.0000
Cr	9	25	2.4000	.0000	62.7000	81.4000	321.0000	409.0000	667.0000	768.0000	848.0000	949.0000
Cr	9	26	3.0000	.0000	60.0000	73.0000	284.0000	335.0000	625.0000	670.0000	800.0000	950.0000
Cr	9	27	10.0000	10.0000	70.0000	80.0000	280.0000	390.0000	550.0000	600.0000	790.0000	810.0000

## STATCALC Input/Output

File Name: cr-9  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc	Lab	Rep	Mean	Result		Ratio
Lev	No	No				
1	15	1	7.2393	1.1000		.15
1	21	1	7.2393	1.0000		.14
2	7	1	9.1521	1.7300		.19
2	8	1	9.1521	.9000		.10
2	15	1	9.1521	1.0000		.11
2	16	1	9.1521	84.0000		9.18
2	21	1	9.1521	.5000		.05

Total Number of Questionable Observations: 7

*** Results of Factor of 5 Error Check ***						
*** Questionable Data (All Values) ***						
Conc	Lab	Rep	Mean	Result	Mean	Obs
Lev	No	No			Dev	Dev
2	16	1	8.4379	84.0000	13.098	75.562
						5.77

Total Number of Questionable Observations: 1

File Name: cr-9  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***			
*** Two-Tailed 5% Significance Level ***			
***	Upper Critical Value:	112.0	***
***	Lower Critical Value:	38.0	***

Ranks											
Lab	Rank	Level	Level	Level	Level	Level	Level	Level	Level	Level	Level
	Sums	1	2	3	4	5	6	7	8	9	10
5	59.5	5.00	3.50	4.00	6.00	5.00	6.00	6.00	7.00	9.00	8.00
6	54.0	1.00	1.00	3.00	4.00	4.00	5.00	9.00	10.00	8.00	9.00
7	63.0	4.00	9.00	1.00	1.00	9.00	10.00	8.00	9.00	6.00	6.00
8	43.0	7.00	7.00	5.00	7.00	2.00	2.00	3.00	4.00	2.00	4.00
10	120.0	14.00	11.00	6.00	12.00	11.00	13.00	14.00	12.00	14.00	13.00
15	34.0	3.00	8.00	2.00	2.00	1.00	3.00	2.00	5.00	3.00	5.00
16	65.5	11.00	14.00	7.50	14.00	13.00	1.00	1.00	2.00	1.00	1.00
17	120.0	9.00	10.00	11.00	13.00	12.00	12.00	12.00	14.00	13.00	14.00
20	115.5	13.00	13.00	14.00	11.00	10.00	8.50	11.00	11.00	12.00	12.00
21	69.0	2.00	6.00	9.00	8.00	7.00	7.00	5.00	8.00	10.00	7.00
24	77.5	10.00	3.50	13.00	3.00	14.00	14.00	13.00	1.00	4.00	2.00
25	92.5	6.00	3.50	10.00	10.00	8.00	11.00	10.00	13.00	11.00	10.00
26	65.0	8.00	3.50	7.50	5.00	6.00	4.00	7.00	6.00	7.00	11.00
27	71.5	12.00	12.00	12.00	9.00	3.00	8.50	4.00	3.00	5.00	3.00
*** Laboratory 10 Rejected; Rank Sum 120.0 ***											
*** Laboratory 17 Rejected; Rank Sum 120.0 ***											

File Name: cr-9  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Outlier Testing Results ***			
*** Two-Sided 5% Significance Level ***			

- Outlier(s) -											
Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n		
1	1	20	1	27.0000	4.9042	8.1665	2.706	2.412	12		
2	1	16	1	84.0000	9.2608	24.7917	3.015	2.412	12		

File Name: cr-9  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

- Normality Tests -						
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)	
1	11	W	A	.8985	.850	---
2	11	W	R	.7518	.850	---
3	12	W	A	.9484	.859	---
4	12	W	A	.9451	.859	---
5	12	W	A	.8659	.859	---
6	12	W	A	.9590	.859	---
7	12	W	A	.9654	.859	---
8	12	W	A	.9455	.859	---
9	12	W	A	.9299	.859	---
10	12	W	A	.8982	.859	---
- 1 Normality Rejection(s) -						

File Name: cr-9  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

Lev	Mtrx	Points As Received	After Lab Ranking		After Outlier Testing	
			Points	%	Points	%
1	9	14	12	85.7	11	78.6
2	9	14	12	85.7	11	78.6
3	9	14	12	85.7	12	85.7
4	9	14	12	85.7	12	85.7
5	9	14	12	85.7	12	85.7
6	9	14	12	85.7	12	85.7
7	9	14	12	85.7	12	85.7
8	9	14	12	85.7	12	85.7
9	9	14	12	85.7	12	85.7
10	9	14	12	85.7	12	85.7
Totals:		140	120	85.7	118	84.3

## STATCALC Input/Output

File Name: cr-9  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	2.6809	2.6809	58.7809	78.4809	297.4809	378.4809	647.4809	718.4809	845.4809	955.4809
RECOVERY:										
Observations	11	11	12	12	12	12	12	12	12	12
Mean Result	2.8955	2.4664	59.8917	76.1667	308.3333	366.0833	607.0833	666.0833	783.2500	879.5000
Bias	.2146	-.2145	1.1108	-2.3142	10.8524	-12.3976	-40.3976	-52.3976	-62.2309	-75.9809
Relative Bias %	8.0031	-8.0024	1.8897	-2.9488	3.6481	-3.2756	-6.2392	-7.2928	-7.3604	-7.9521
Maximum Result	10.0000	23.0000	80.0000	100.0000	397.0000	487.0000	717.0000	768.0000	873.0000	972.0000
Minimum Result	-7.0000	-10.0000	45.5000	60.0000	261.0000	269.0000	471.0000	548.0000	644.0000	700.0000
SINGLE OPERATOR PRECISION:	Pair 1	Pair 2	Pair 3	Pair 4	Pair 5					
Observations	10	12	12	12	12					
Standard Deviation	1.5234	7.6244	40.9136	53.3258	26.6102					
Correction Factor	1.0281	1.0230	1.0230	1.0230	1.0230					
Corrected Std Dev	1.5662	7.7994	41.8528	54.5499	27.2210					
Relative Std Dev (%)	58.4221	11.4648	12.4115	8.5692	3.2742					
OVERALL PRECISION:										
Observations	11	11	12	12	12	12	12	12	12	12
Standard Deviation	4.4832	8.1679	10.7877	10.7969	42.9277	58.9321	72.4349	70.4369	63.8978	81.5537
Correction Factor	1.0253	1.0253	1.0230	1.0230	1.0230	1.0230	1.0230	1.0230	1.0230	1.0230
Corrected Std Dev	4.5965	8.3743	11.0354	11.0447	43.9131	60.2849	74.0977	72.0538	65.3646	83.4258
Relative Std Dev %	158.7495	339.5400	18.4256	14.5007	14.2421	16.4675	12.2055	10.8175	8.3453	9.4856

File Name: cr-9  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	2.6809	2.8955	.2146	8.00	.159	3.169	NO
2	2.6809	2.4664	-.2145	-8.00	.087	3.169	NO
3	58.7809	59.8917	1.1108	1.89	.357	3.106	NO
4	78.4809	76.1667	-2.3142	-2.95	.743	3.106	NO
5	297.4809	308.3333	10.8524	3.65	.876	3.106	NO
6	378.4809	366.0833	-12.3976	-3.28	.729	3.106	NO
7	647.4809	607.0833	-40.3976	-6.24	1.932	3.106	NO
8	718.4809	666.0833	-52.3976	-7.29	2.577	3.106	NO
9	845.4809	783.2500	-62.2309	-7.36	3.374	3.106	YES
10	955.4809	879.5000	-75.9809	-7.95	3.227	3.106	YES

File Name: cr-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): 4.3037  
Slope (b): .0605  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	10	42.58	2.6809	1.5662	4.4659
2	12	35.95	68.6309	7.7994	8.4565
3	12	12.49	337.9809	41.8528	24.7549
4	12	5.36	682.9809	54.5499	45.6308
5	12	3.62	900.4809	27.2210	58.7917

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

a: 5.3611 Intercept (a'): 1.6792  
b: 1.0027 Slope (b'): .0027  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	10	16.92	2.6809	1.5662	5.4000
2	12	20.77	2.6809	7.7994	6.4510
3	12	20.77	58.7809	41.8528	13.3373
4	12	20.77	78.4809	54.5499	33.8145
5	12	20.77	297.4809	27.2210	60.7886

File Name: cr-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): 6.1557  
Slope (b): .0976  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	11	30.07	2.6809	4.5965	6.4173
2	11	30.07	2.6809	8.3743	6.4173
3	12	16.89	58.7809	11.0354	11.8909
4	12	13.95	78.4809	11.0447	13.8130
5	12	3.44	297.4809	43.9131	35.1805
6	12	2.44	378.4809	60.2849	43.0835
7	12	1.05	647.4809	74.0977	69.3294
8	12	.89	718.4809	72.0538	76.2567
9	12	.67	845.4809	65.3646	88.6479
10	12	.54	955.4809	83.4258	99.3805

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

a: 9.9583 Intercept (a'): 2.2984  
b: 1.0027 Slope (b'): .0027  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	11	9.24	2.6809	4.5965	10.0297
2	11	9.24	2.6809	8.3743	10.0297
3	12	10.19	58.7809	11.0354	11.6480
4	12	10.19	78.4809	11.0447	12.2762
5	12	10.19	297.4809	43.9131	22.0118
6	12	10.19	378.4809	60.2849	27.3181
7	12	10.19	647.4809	74.0977	55.9683
8	12	10.19	718.4809	72.0538	67.6328
9	12	10.19	845.4809	65.3646	94.8896
10	12	10.19	955.4809	83.4258	127.2314

## STATCALC Input/Output

File Name: cr-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): .9728  
Slope (b): .9501

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	11	37.86	2.6809	2.8955	3.5200
2	11	37.86	2.6809	2.4664	3.5200
3	12	12.03	58.7809	59.8917	56.8231
4	12	8.92	78.4809	76.1667	75.5409
5	12	1.37	297.4809	308.3333	283.6223
6	12	.92	378.4809	366.0833	360.5840
7	12	.35	647.4809	607.0833	616.1726
8	12	.29	718.4809	666.0833	683.6328
9	12	.22	845.4809	783.2500	804.3010
10	12	.17	955.4809	879.5000	908.8168

File Name: cr-9  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: Cr Matrix: Estuarine  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): 3.2799  
Slope (f): .0637

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 5.3463  
(f): 1.0028

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): 5.1319  
Slope (f): .1027

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 9.9311  
(f): 1.0028



cr-10.dat

Cr	10	1	12.4000	11.4000	40.5000	58.1000	165.1000	214.7000	399.0000	440.0000	1123.0000	1022.0000
Cr	10	2	2.0000	3.0000	47.0000	66.0000	210.0000	279.0000	430.0000	410.0000	744.0000	732.0000
Cr	10	5	3.0000	3.0000	41.0000	59.0000	180.0000	247.0000	378.0000	436.0000	752.0000	817.0000
Cr	10	6	0.0000	-7.0000	39.0000	54.0000	206.0000	290.0000	446.0000	505.0000	863.0000	951.0000
Cr	10	7	5.1200	4.8200	43.4000	62.0000	206.0000	275.0000	418.0000	468.0000	796.0000	822.0000
Cr	10	8	0.9000	0.4000	30.3000	52.2000	172.0000	257.0000	394.0000	479.0000	794.0000	930.0000
Cr	10	10	42.5000	100.0000	100.5000	73.5000	308.0000	343.0000	463.0000	466.0000	971.0000	1072.5000
Cr	10	11	7.1000	8.2000	51.7000	69.8000	215.0000	276.0000	451.0000	505.0000	902.0000	990.0000
Cr	10	15	3.9000	4.1000	40.0000	59.0000	192.0000	247.0000	396.0000	413.0000	718.0000	855.0000
Cr	10	16	22.2000	8.9000	54.4000	111.0000	233.0000	322.0000	478.0000	460.0000	830.0000	910.0000
Cr	10	17	6.0000	4.0000	53.0000	69.0000	223.0000	303.0000	512.0000	580.0000	1020.0000	1211.0000
Cr	10	20	24.0000	18.0000	87.0000	96.0000	266.0000	343.0000	507.0000	563.0000	937.0000	1052.0000
Cr	10	21	2.9000	2.0000	36.0000	53.0000	171.0000	244.0000	376.0000	439.0000	765.0000	869.0000
Cr	10	24	5.2000	0.0000	32.9000	73.4000	230.0000	258.0000	487.0000	496.0000	450.0000	106.0000
Cr	10	25	0.0000	2.4000	58.3000	81.4000	269.0000	295.0000	459.0000	529.0000	1020.0000	949.0000
Cr	10	26	4.0000	4.0000	53.0000	81.0000	206.0000	268.0000	460.0000	490.0000	890.0000	950.0000
Cr	10	27	10.0000	20.0000	40.0000	80.0000	170.0000	220.0000	300.0000	460.0000	780.0000	870.0000

File Name: cr-10  
Data Validation File (.DA~)

```

*****
***      Parameter and Data Validation File      ***
*****
Analyte:  Cr          Matrix:  Acid Mine Drainage
Project:  AMQ-TC      Matrix ID: 10
Date:     12/13/1995  Method:  GFAAS
Pairs:    5
Units:    ug/L

```

Level	1	2	3	4	5	6	7	8	9	10
Spike	4.6978	.0000	45.9000	19.6000	150.0000	70.0000	167.0000	64.0000	391.0000	89.0000
Increment	.0000	.0000	45.9000	65.5000	215.5000	285.5000	452.5000	516.5000	907.5000	996.5000

Final Concentration											
Lab ID	4.6978	4.6978	50.5978	70.1978	220.1978	290.1978	457.1978	521.1978	912.1978	1001.1980	
1	12.4000	11.4000	40.5000	58.1000	165.1000	214.7000	399.0000	440.0000	1123.0000	1022.0000	
2	2.0000	3.0000	47.0000	66.0000	210.0000	279.0000	430.0000	410.0000	744.0000	732.0000	
5	3.0000	3.0000	41.0000	59.0000	180.0000	247.0000	378.0000	436.0000	752.0000	817.0000	
6	.0000	-7.0000	39.0000	54.0000	206.0000	290.0000	446.0000	505.0000	863.0000	951.0000	
7	5.1200	4.8200	43.4000	62.0000	206.0000	275.0000	418.0000	468.0000	796.0000	822.0000	
8	.9000	.4000	30.3000	52.2000	172.0000	257.0000	394.0000	479.0000	794.0000	930.0000	
10	r 42.5000r	100.0000	r 100.5000r	73.5000	r 308.0000r	343.0000	r 463.0000r	466.0000	r 971.0000r	1072.5000	
11	7.1000	8.2000	51.7000	69.8000	215.0000	276.0000	451.0000	505.0000	902.0000	990.0000	
15	3.9000	4.1000	40.0000	59.0000	192.0000	247.0000	396.0000	413.0000	718.0000	855.0000	
16	o 22.2000	8.9000	54.4000o	111.0000	233.0000	322.0000	478.0000	460.0000	830.0000	910.0000	
17	6.0000	4.0000	53.0000	69.0000	223.0000	303.0000	512.0000	580.0000	1020.0000	1211.0000	
20	r 24.0000r	18.0000	r 87.0000r	96.0000	r 266.0000r	343.0000	r 507.0000r	563.0000	r 937.0000r	1052.0000	
21	r 2.9000r	2.0000	r 36.0000r	53.0000	r 171.0000r	244.0000	r 376.0000r	439.0000	r 765.0000r	869.0000	
24	5.2000	.0000	32.9000	73.4000	230.0000	258.0000	487.0000	496.0000	450.0000o	106.0000	
25	.0000	2.4000	58.3000	81.4000	269.0000	295.0000	459.0000	529.0000	1020.0000	949.0000	
26	4.0000	4.0000	53.0000	81.0000	206.0000	268.0000	460.0000	490.0000	890.0000	950.0000	
27	10.0000	20.0000	40.0000	80.0000	170.0000	220.0000	300.0000	460.0000	780.0000	870.0000	

cr-10.daf

Cr	10	1	12.4000	11.4000	40.5000	58.1000	165.1000	214.7000	399.0000	440.0000	1123.0000	1022.0000
Cr	10	2	2.0000	3.0000	47.0000	66.0000	210.0000	279.0000	430.0000	410.0000	744.0000	732.0000
Cr	10	5	3.0000	3.0000	41.0000	59.0000	180.0000	247.0000	378.0000	436.0000	752.0000	817.0000
Cr	10	6	.0000	-7.0000	39.0000	54.0000	206.0000	290.0000	446.0000	505.0000	863.0000	951.0000
Cr	10	7	5.1200	4.8200	43.4000	62.0000	206.0000	275.0000	418.0000	468.0000	796.0000	822.0000
Cr	10	8	.9000	.4000	30.3000	52.2000	172.0000	257.0000	394.0000	479.0000	794.0000	930.0000
Cr	10	11	7.1000	8.2000	51.7000	69.8000	215.0000	276.0000	451.0000	505.0000	902.0000	990.0000
Cr	10	15	3.9000	4.1000	40.0000	59.0000	192.0000	247.0000	396.0000	413.0000	718.0000	855.0000
Cr	10	16	o 22.2000	8.9000	54.4000o	111.0000	233.0000	322.0000	478.0000	460.0000	830.0000	910.0000
Cr	10	17	6.0000	4.0000	53.0000	69.0000	223.0000	303.0000	512.0000	580.0000	1020.0000	1211.0000
Cr	10	24	5.2000	.0000	32.9000	73.4000	230.0000	258.0000	487.0000	496.0000	450.0000o	106.0000
Cr	10	25	.0000	2.4000	58.3000	81.4000	269.0000	295.0000	459.0000	529.0000	1020.0000	949.0000
Cr	10	26	4.0000	4.0000	53.0000	81.0000	206.0000	268.0000	460.0000	490.0000	890.0000	950.0000
Cr	10	27	10.0000	20.0000	40.0000	80.0000	170.0000	220.0000	300.0000	460.0000	780.0000	870.0000

## STATCALC Input/Output

File Name: cr-10  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Results of 5x - 1/5x Mean Error Check ***						
*** Questionable Data (Positive Values) ***						
Conc	Lab	Rep	Mean	Result		Ratio
Lev	No	No	Result			
1	8	1	8.8953	.9000		.10
2	8	1	11.4247	.4000		.04
2	10	1	11.4247	100.0000		8.75
2	21	1	11.4247	2.0000		.18
10	24	1	888.7353	106.0000		.12

Total Number of Questionable Observations: 5

*** Results of Factor of 5 Error Check ***							
*** Questionable Data (All Values) ***							
Conc	Lab	Rep	Mean	Result	Mean	Obs	Ratio
Lev	No	No	Result		Dev	Dev	
2	10	1	11.0129	100.0000	12.394	88.987	7.18
10	24	1	888.7353	106.0000	135.311	782.735	5.78

Total Number of Questionable Observations: 2

File Name: cr-10  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Laboratory Ranking Results ***			
*** Two-Tailed 5% Significance Level ***			
***	Upper Critical Value:	135.0	***
***	Lower Critical Value:	45.0	***

Ranks												
Lab	Rank Sums	Level 1	Level 2	Level 3	Level 4	Level 5	Level 6	Level 7	Level 8	Level 9	Level 10	Level 11
1	83.0	14.00	14.00	7.00	4.00	1.00	1.00	6.00	5.00	17.00	14.00	
2	63.5	4.00	6.50	10.00	8.00	10.00	11.00	8.00	1.00	3.00	2.00	
5	48.5	6.00	6.50	8.00	5.50	5.00	4.50	3.00	3.00	4.00	3.00	
6	74.0	1.50	1.00	4.00	3.00	8.00	12.00	9.00	13.50	10.00	12.00	
7	81.0	9.00	11.00	9.00	7.00	8.00	9.00	7.00	9.00	8.00	4.00	
8	48.0	3.00	3.00	1.00	1.00	4.00	6.00	4.00	10.00	7.00	9.00	
10	147.5	17.00	17.00	17.00	12.00	17.00	16.50	13.00	8.00	14.00	16.00	
11	114.5	12.00	12.00	11.00	10.00	11.00	10.00	10.00	13.50	12.00	13.00	
15	52.5	7.00	10.00	5.50	5.50	6.00	4.50	5.00	2.00	2.00	5.00	
16	125.5	15.00	13.00	14.00	17.00	14.00	15.00	14.00	6.50	9.00	8.00	
17	133.5	11.00	8.50	12.50	9.00	12.00	14.00	17.00	17.00	15.50	17.00	
20	154.5	16.00	15.00	16.00	16.00	15.00	16.50	16.00	16.00	13.00	15.00	
21	37.0	5.00	4.00	3.00	2.00	3.00	3.00	2.00	4.00	5.00	6.00	
24	74.0	10.00	2.00	2.00	11.00	13.00	7.00	15.00	12.00	1.00	1.00	
25	117.0	1.50	5.00	15.00	15.00	16.00	13.00	11.00	15.00	15.50	10.00	
26	104.0	8.00	8.50	12.50	14.00	8.00	8.00	12.00	11.00	11.00	11.00	
27	72.0	13.00	16.00	5.50	13.00	2.00	2.00	1.00	6.50	6.00	7.00	
*** Laboratory	10	Rejected; Rank Sum	147.5	***								
*** Laboratory	20	Rejected; Rank Sum	154.5	***								
*** Laboratory	21	Rejected; Rank Sum	37.0	***								

File Name: cr-10  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

*** Outlier Testing Results ***			
*** Two-Sided 5% Significance Level ***			

- Outlier(s) -										
Lev	Iter	Lab	Rep	Result	Mean	Std Dev	t	Crit t	n	
1	1	16	1	22.2000	5.8443	5.9037	2.770	2.507	14	
4	1	16	1	111.0000	69.7071	15.3918	2.683	2.507	14	
*	1	24	1	106.0000	865.3571	245.8835	3.088	2.507	14	

File Name: cr-10  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Results of Normality Testing \*\*\*

- Normality Tests -						
Level	n	Test Type	Normality Accept/Reject	Test Statistic	Critical Value(s)	
1	13	W	A	.9402	.866	---
2	14	W	A	.9186	.874	---
3	14	W	A	.9451	.874	---
4	13	W	A	.9258	.866	---
5	14	W	A	.9504	.874	---
6	14	W	A	.9790	.874	---
7	14	W	A	.9524	.874	---
8	14	W	A	.9631	.874	---
9	14	W	A	.9405	.874	---
10	13	W	A	.9345	.866	---
- 0 Normality Rejection(s) -						

File Name: cr-10  
Data Preparation File (.PRP)

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC  
Date: 12/13/1995  
Units: ug/L

\*\*\* Data Removal Tracking \*\*\*  
\*\*\* Simple Count of Remaining Data Points \*\*\*  
\*\*\* After Removal Tests \*\*\*

Lev	Mtrx	Points As Received	After Lab Ranking		After Outlier Testing	
			Points	%	Points	%
1	10	17	14	82.4	13	76.5
2	10	17	14	82.4	14	82.4
3	10	17	14	82.4	14	82.4
4	10	17	14	82.4	13	76.5
5	10	17	14	82.4	14	82.4
6	10	17	14	82.4	14	82.4
7	10	17	14	82.4	14	82.4
8	10	17	14	82.4	14	82.4
9	10	17	14	82.4	14	82.4
10	10	17	14	82.4	13	76.5
Totals:		170	140	82.4	137	80.6

## STATCALC Input/Output

File Name: cr-10  
Statistical Analysis File (.STT)

## \*\*\* Summary Performance Statistics \*\*\*

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

LEVEL:	1	2	3	4	5	6	7	8	9	10
YOUDEEN PAIRS:	Pair 1 (Low)	Pair 1 (High)	Pair 2 (Low)	Pair 2 (High)	Pair 3 (Low)	Pair 3 (High)	Pair 4 (Low)	Pair 4 (High)	Pair 5 (Low)	Pair 5 (High)
CONCENTRATION:	4.6978	4.6978	50.5978	70.1978	220.1978	290.1978	457.1978	521.1978	912.1978	1001.1980
RECOVERY:										
Observations	13	14	14	13	14	14	14	14	14	13
Mean Result	4.5862	4.8014	44.6071	66.5308	205.5072	267.9786	429.1429	476.5000	834.4286	923.7692
Bias	-.1116	.1036	-5.9907	-3.6670	-14.6906	-22.2192	-28.0550	-44.6978	-77.7692	-77.4286
Relative Bias %	-2.3766	2.2059	-11.8398	-5.2238	-6.6716	-7.6566	-6.1363	-8.5760	-8.5255	-7.7336
Maximum Result	12.4000	20.0000	58.3000	81.4000	269.0000	322.0000	512.0000	580.0000	1123.0000	1211.0000
Minimum Result	.0000	-7.0000	30.3000	52.2000	165.1000	214.7000	300.0000	410.0000	450.0000	732.0000
SINGLE OPERATOR PRECISION:	Pair 1		Pair 2		Pair 3		Pair 4		Pair 5	
Observations	13		13		14		14		13	
Standard Deviation	2.8082		5.9953		13.8476		32.1578		58.1594	
Correction Factor	1.0210		1.0210		1.0194		1.0194		1.0194	
Corrected Std Dev	2.8672		6.1214		14.1162		32.7816		59.3823	
Relative Std Dev (%)	61.0336		11.0969		5.9627		7.2394		6.7676	
OVERALL PRECISION:										
Observations	13	14	14	13	14	14	14	14	14	13
Standard Deviation	3.7083	6.1932	8.4457	10.1798	28.6267	30.1738	53.9699	46.1648	162.4390	117.2548
Correction Factor	1.0210	1.0194	1.0194	1.0210	1.0194	1.0194	1.0194	1.0194	1.0194	1.0210
Corrected Std Dev	3.7863	6.3133	8.6095	10.3938	29.1820	30.7591	55.0168	47.0603	165.5899	119.7204
Relative Std Dev %	82.5589	131.4881	19.3008	15.6226	14.2000	11.4782	12.8202	9.8762	19.8447	12.9600

File Name: cr-10  
Statistical Analysis File (.STT)

## \*\*\* Results of Bias Testing \*\*\*

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

Conc. Level	Conc	Mean Result	Bias	Rel. Bias (%)	Obs t Value	Crit t Value	Statistically Significant (1% Two-Tail)
1	4.6978	4.5862	-.1116	-2.38	.109	3.055	NO
2	4.6978	4.8014	.1036	2.21	.063	3.012	NO
3	50.5978	44.6071	-5.9907	-11.84	2.654	3.012	NO
4	70.1978	66.5308	-3.6670	-5.22	1.299	3.055	NO
5	220.1978	205.5072	-14.6906	-6.67	1.920	3.012	NO
6	290.1978	267.9786	-22.2192	-7.66	2.755	3.012	NO
7	457.1978	429.1429	-28.0550	-6.14	1.945	3.012	NO
8	521.1978	476.5000	-44.6978	-8.58	3.623	3.012	YES
9	912.1978	834.4286	-77.7692	-8.53	1.791	3.012	NO
10	1001.1980	923.7692	-77.4286	-7.73	2.381	3.055	NO

File Name: cr-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Single Operator Precision \*\*\*

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): 2.5972  
Slope (b): .0561  
=====

Pair	Sample Size	Weights (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	86.18	4.6978	2.8672	2.8606
2	13	12.05	60.3978	6.1214	5.9844
3	14	1.29	255.1978	14.1162	16.9091
4	14	.39	489.1978	32.7816	30.0323
5	13	.10	956.6978	59.3823	56.2505

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

a: 4.8491 Intercept (a'): 1.5788  
b: 1.0030 Slope (b'): .0030  
=====

Pair	Sample Size	Weight (%)	Conc	Single Operator Std Dev	Estimated Std Dev
1	13	19.34	4.6978	2.8672	4.9174
2	13	19.34	4.6978	6.1214	5.8041
3	14	20.99	50.5978	14.1162	10.3647
4	14	20.99	70.1978	32.7816	20.7995
5	13	19.34	220.1978	59.3823	83.6366

File Name: cr-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Overall Precision \*\*\*

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Overall Precision \*\*\*

- Linear Model -  $s = b \cdot T + a$   
=====

Intercept (a): 4.1036  
Slope (b): .1031  
=====

Conc Level	Sample Size	Weights (%)	Conc	Overall Std Dev	Estimated Std Dev
1	13	24.55	4.6978	3.7863	4.5878
2	14	26.64	4.6978	6.3133	4.5878
3	14	19.74	50.5978	8.6095	9.3182
4	13	16.01	70.1978	10.3938	11.3381
5	14	6.52	220.1978	29.1820	26.7969
6	14	4.13	290.1978	30.7591	34.0110
7	14	1.39	457.1978	55.0168	51.2218
8	14	.91	521.1978	47.0603	57.8176
9	14	.07	912.1978	165.5899	98.1135
10	13	.04	1001.1980	119.7204	107.2857

- Curvilinear Model -  $s = a \cdot (b \cdot T)^2$  (  $\ln s = b' \cdot T + a'$  )

a: 7.9953 Intercept (a'): 2.0788  
b: 1.0033 Slope (b'): .0033  
=====

Conc Level	Sample Size	Weight (%)	Conc	Overall Std Dev	Estimated Std Dev
1	13	9.44	4.6978	3.7863	8.1189
2	14	10.24	4.6978	6.3133	8.1189
3	14	10.24	50.5978	8.6095	9.4316
4	13	9.44	70.1978	10.3938	10.0550
5	14	10.24	220.1978	29.1820	16.4095
6	14	10.24	290.1978	30.7591	20.6235
7	14	10.24	457.1978	55.0168	35.5783
8	14	10.24	521.1978	47.0603	43.8473
9	14	10.24	912.1978	165.5899	157.1880
10	13	9.44	1001.1980	119.7204	210.1988

## STATCALC Input/Output

File Name: cr-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\*\*\* Recovery \*\*\*\*\*

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Recovery \*\*\*

- Linear Model -  $X = b \cdot T + a$

Intercept (a): .2353  
Slope (b): .9225

Conc Level	Sample Size	Weights (%)	Conc	Mean Result	Estimated Result
1	13	38.87	4.6978	4.5862	4.5689
2	14	41.86	4.6978	4.8014	4.5689
3	14	10.15	50.5978	44.6071	46.9113
4	13	6.36	70.1978	66.5308	64.9922
5	14	1.23	220.1978	205.5072	203.3660
6	14	.76	290.1978	267.9786	267.9405
7	14	.34	457.1978	429.1429	421.9967
8	14	.26	521.1978	476.5000	481.0362
9	14	.09	912.1978	834.4286	841.7307
10	13	.07	1001.1980	923.7692	923.8325

File Name: cr-10  
Statistical Analysis File (.STT)

\*\*\* Performance Estimation Results \*\*\*  
\*\*\* Precision vs Recovery \*\*\*

Analyte: Cr Matrix: Acid Mine Drainage  
Project: AMQ-TC Method: GFAAS  
Date: 12/13/1995  
Units: ug/L

\*\*\* Single Operator Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): 2.3421  
Slope (f): .0608

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 4.8454  
(f): 1.0032

\*\*\* Overall Precision vs Recovery \*\*\*  
(Obtained by Substitution)

- Linear Model -  $s = f \cdot X + e$

Intercept (e): 3.8486  
Slope (f): .1117

- Curvilinear Model -  $s = e \cdot (f \cdot X)$

Intercept (e): 7.9886  
(f): 1.0035